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ENGINEERING REPORT

K268DE, Baytown, TX, Channel 269D Minor Mod

ENGINEERING STATEMENT

PROTECTION TO KMJQ AND KLOL

All contour non-overlap protection requirements are met with the exception of KMJQ, Houston, TX (271C) and KLOL, Houston, TX (266C), discussed below.

KMJQ (50.8 kilometers at 245 degrees True) and KLOL (52.2 kilometers at 246 degrees True) are second/third adjacent-channel to the proposed channel 269D facility. The 60 dBu F50,50 service contour of each extends well beyond the proposed 269D transmitter site. Using the well-established *Living Way Ministries* Methodology, no actual interference to any population is predicted to exist to KMJQ or KLOL.

Note that a rule waiver of Section 74.1204 for this second/third adjacent-channel protection using the well-established *Living Way Ministries* Methodology is respectfully requested if such a rule waiver is deemed necessary for protection to any station.

The F50,50 signal strength from KMJQ at the proposed 269D transmitter site is at least 75 dBu (the “desired” signal of KMJQ). The F50,50 signal strength from KLOL at the proposed 269D transmitter site is at least 76 dBu (the other “desired” signal of KLOL). The second/third adjacent-channel protection of Section 74.1204 is an undesired-to-desired (“U/D”) dB signal strength ratio of 40:1. Therefore, predicted interference to KMJQ and KLOL from the proposed 269D facility is a signal of greater than or equal to 115 dBu.

Figure EE1 is the vertical plane relative field pattern for the proposed Scala CL-FM(H) single-bay antenna. By adjusting for the vertical plane downward relative field values of the proposed antenna, it is herein demonstrated that the 115 dBu interfering signal (using a free space field determination) does not exist at any point at ground level. (Actually, the study is made to 2 meters above ground level to account for a person’s height.)

Attached as Figure EE2 is a tabulation of various points (at 2 meters above ground level) from the proposed translator tower base. (Column B is the different

distances from the tower base to each studied point.) The actual distance from the antenna to each point is listed in Column C, the hypotenuse of the vertical height (Column A) and the horizontal distance (Column B). Also, the vertical distance from the antenna bottom to the calculated interference signal for each studied point is provided in Column K. Because the calculated distance to the free space interfering signal (Column J) is less than the hypotenuse distance (Column C) and the interfering signal vertical distance (Column K) is less than the vertical distance (Column A) for each studied point, the interfering signal does not reach any studied point. (In other words, the interfering signal does not make it to 2 meters any point.) The clearance is at least 77 meters. Therefore, pursuant to Section 74.1204(d) of the FCC Rules, KMJQ and KLOL are adequately protected by the proposed facility.

FIGURE EE1 (Page 1 of 2)

Antenna: CL-FM

Vertical Polarization (**Vertical Pattern** for H-Pol Antenna)

| Azimuth | Field | Rel.dB | dBd | Pwr Gain |
|---------|-------|--------|-----|----------|
| 0 | 1.000 | 0.0 | 7.0 | 5.012 |
| 1 | 0.998 | -0.0 | 7.0 | 5.012 |
| 2 | 0.997 | -0.0 | 7.0 | 5.012 |
| 3 | 0.996 | -0.0 | 7.0 | 5.012 |
| 4 | 0.995 | -0.0 | 7.0 | 5.012 |
| 5 | 0.993 | -0.1 | 6.9 | 4.898 |
| 6 | 0.991 | -0.1 | 6.9 | 4.898 |
| 7 | 0.988 | -0.1 | 6.9 | 4.898 |
| 8 | 0.985 | -0.1 | 6.9 | 4.898 |
| 9 | 0.982 | -0.2 | 6.8 | 4.786 |
| 10 | 0.980 | -0.2 | 6.8 | 4.786 |
| 11 | 0.975 | -0.2 | 6.8 | 4.786 |
| 12 | 0.969 | -0.3 | 6.7 | 4.677 |
| 13 | 0.964 | -0.3 | 6.7 | 4.677 |
| 14 | 0.958 | -0.4 | 6.6 | 4.571 |
| 15 | 0.952 | -0.4 | 6.6 | 4.571 |
| 16 | 0.946 | -0.5 | 6.5 | 4.467 |
| 17 | 0.938 | -0.6 | 6.4 | 4.365 |
| 18 | 0.931 | -0.6 | 6.4 | 4.365 |
| 19 | 0.923 | -0.7 | 6.3 | 4.266 |
| 20 | 0.916 | -0.8 | 6.2 | 4.169 |
| 21 | 0.908 | -0.8 | 6.2 | 4.169 |
| 22 | 0.899 | -0.9 | 6.1 | 4.074 |
| 23 | 0.890 | -1.0 | 6.0 | 3.981 |
| 24 | 0.882 | -1.1 | 5.9 | 3.890 |
| 25 | 0.873 | -1.2 | 5.8 | 3.802 |
| 26 | 0.862 | -1.3 | 5.7 | 3.715 |
| 27 | 0.851 | -1.4 | 5.6 | 3.631 |
| 28 | 0.840 | -1.5 | 5.5 | 3.548 |
| 29 | 0.829 | -1.6 | 5.4 | 3.467 |
| 30 | 0.817 | -1.8 | 5.2 | 3.311 |
| 31 | 0.806 | -1.9 | 5.1 | 3.236 |
| 32 | 0.793 | -2.0 | 5.0 | 3.162 |
| 33 | 0.781 | -2.2 | 4.8 | 3.020 |
| 34 | 0.767 | -2.3 | 4.7 | 2.951 |
| 35 | 0.756 | -2.4 | 4.6 | 2.884 |
| 36 | 0.742 | -2.6 | 4.4 | 2.754 |
| 37 | 0.729 | -2.7 | 4.3 | 2.692 |
| 38 | 0.716 | -2.9 | 4.1 | 2.570 |
| 39 | 0.704 | -3.1 | 3.9 | 2.455 |
| 40 | 0.690 | -3.2 | 3.8 | 2.399 |
| 41 | 0.675 | -3.4 | 3.6 | 2.291 |
| 42 | 0.661 | -3.6 | 3.4 | 2.188 |
| 43 | 0.646 | -3.8 | 3.2 | 2.089 |
| 44 | 0.632 | -4.0 | 3.0 | 1.995 |
| 45 | 0.618 | -4.2 | 2.8 | 1.905 |

FIGURE EE1 (Page 2 of 2)

Antenna: CL-FM

Vertical Polarization (**Vertical Pattern** for H-Pol Antenna)

| Azimuth | Field | Rel.dB | dBd | Pwr Gain |
|---------|-------|--------|-------|----------|
| 46 | 0.602 | -4.4 | 2.6 | 1.820 |
| 47 | 0.588 | -4.6 | 2.4 | 1.738 |
| 48 | 0.573 | -4.8 | 2.2 | 1.660 |
| 49 | 0.558 | -5.1 | 1.9 | 1.549 |
| 50 | 0.544 | -5.3 | 1.7 | 1.479 |
| 51 | 0.528 | -5.5 | 1.5 | 1.413 |
| 52 | 0.513 | -5.8 | 1.2 | 1.318 |
| 53 | 0.498 | -6.1 | 0.9 | 1.230 |
| 54 | 0.483 | -6.3 | 0.7 | 1.175 |
| 55 | 0.467 | -6.6 | 0.4 | 1.096 |
| 56 | 0.452 | -6.9 | 0.1 | 1.023 |
| 57 | 0.436 | -7.2 | -0.2 | 0.955 |
| 58 | 0.421 | -7.5 | -0.5 | 0.891 |
| 59 | 0.405 | -7.8 | -0.8 | 0.832 |
| 60 | 0.390 | -8.2 | -1.2 | 0.759 |
| 61 | 0.372 | -8.6 | -1.6 | 0.692 |
| 62 | 0.354 | -9.0 | -2.0 | 0.631 |
| 63 | 0.336 | -9.5 | -2.5 | 0.562 |
| 64 | 0.318 | -10.0 | -3.0 | 0.501 |
| 65 | 0.300 | -10.5 | -3.5 | 0.447 |
| 66 | 0.278 | -11.1 | -4.1 | 0.389 |
| 67 | 0.256 | -11.8 | -4.8 | 0.331 |
| 68 | 0.234 | -12.6 | -5.6 | 0.275 |
| 69 | 0.212 | -13.5 | -6.5 | 0.224 |
| 70 | 0.190 | -14.4 | -7.4 | 0.182 |
| 71 | 0.174 | -15.2 | -8.2 | 0.151 |
| 72 | 0.158 | -16.0 | -9.0 | 0.126 |
| 73 | 0.142 | -17.0 | -10.0 | 0.100 |
| 74 | 0.126 | -18.0 | -11.0 | 0.079 |
| 75 | 0.110 | -19.2 | -12.2 | 0.060 |
| 76 | 0.098 | -20.2 | -13.2 | 0.048 |
| 77 | 0.086 | -21.3 | -14.3 | 0.037 |
| 78 | 0.074 | -22.6 | -15.6 | 0.028 |
| 79 | 0.062 | -24.2 | -17.2 | 0.019 |
| 80 | 0.050 | -26.0 | -19.0 | 0.013 |
| 81 | 0.046 | -26.7 | -19.7 | 0.011 |
| 82 | 0.042 | -27.5 | -20.5 | 0.009 |
| 83 | 0.038 | -28.4 | -21.4 | 0.007 |
| 84 | 0.034 | -29.4 | -22.4 | 0.006 |
| 85 | 0.030 | -30.5 | -23.5 | 0.004 |
| 86 | 0.030 | -30.5 | -23.5 | 0.004 |
| 87 | 0.030 | -30.5 | -23.5 | 0.004 |
| 88 | 0.030 | -30.5 | -23.5 | 0.004 |
| 89 | 0.030 | -30.5 | -23.5 | 0.004 |
| 90 | 0.030 | -30.5 | -23.5 | 0.004 |

FIGURE EE2

FREE SPACE FIELD STRENGTH AT A DISTANCE STUDY RESULTS

PROJECT: BAYTOWN, TX, CHANNEL 269D

3-Aug-17

| Pt | Column A Vert Dist From Ant Bottom (meters) | Column B Horiz Dist From Tower Base (meters) | Column C Hypot- enuse Dist fr Ant Bottom (meters) | Column D Down- ward Angle fr Ant Bottom (degrees) | Column E Max ERP (watts) | Column F Max ERP (dBmw) | Column G Pattern Relative Field at Down- ward Angle | Column H Free Space Inter- ferring Signal (dBu) | Column I Adjusted ERP in Down- ward Angle (dBmW) | Column J Interf Distance along Hypot- enuse (meters) | Column K Vert Interf Distance below Antenna (meters) |
|----|---|--|---|---|-----------------------------------|----------------------------------|---|---|--|--|--|
| 1 | 167 | 0.1 | 167.0 | 90.0 | 250 | 53.98 | 0.030 | 115.0 | 23.52 | 5.9 | 5.9 |
| 2 | 167 | 20 | 168.2 | 83.2 | 250 | 53.98 | 0.038 | 115.0 | 25.58 | 7.5 | 7.5 |
| 3 | 167 | 30 | 169.7 | 79.8 | 250 | 53.98 | 0.062 | 115.0 | 29.83 | 12.3 | 12.1 |
| 4 | 167 | 40 | 171.7 | 76.5 | 250 | 53.98 | 0.098 | 115.0 | 33.80 | 19.4 | 18.9 |
| 5 | 167 | 50 | 174.3 | 73.3 | 250 | 53.98 | 0.142 | 115.0 | 37.03 | 28.1 | 26.9 |
| 6 | 167 | 60 | 177.5 | 70.2 | 250 | 53.98 | 0.190 | 115.0 | 39.55 | 37.6 | 35.4 |
| 7 | 167 | 70 | 181.1 | 67.3 | 250 | 53.98 | 0.256 | 115.0 | 42.14 | 50.7 | 46.7 |
| 8 | 167 | 80 | 185.2 | 64.4 | 250 | 53.98 | 0.318 | 115.0 | 44.03 | 62.9 | 56.8 |
| 9 | 167 | 90 | 189.7 | 61.7 | 250 | 53.98 | 0.372 | 115.0 | 45.39 | 73.6 | 64.8 |
| 10 | 167 | 100 | 194.7 | 59.1 | 250 | 53.98 | 0.405 | 115.0 | 46.13 | 80.2 | 68.8 |
| 11 | 167 | 120 | 205.6 | 54.3 | 250 | 53.98 | 0.483 | 115.0 | 47.66 | 95.6 | 77.6 |
| 12 | 167 | 140 | 217.9 | 50.0 | 250 | 53.98 | 0.544 | 115.0 | 48.69 | 107.7 | 82.5 |
| 13 | 167 | 160 | 231.3 | 46.2 | 250 | 53.98 | 0.602 | 115.0 | 49.57 | 119.1 | 86.0 |
| 14 | 167 | 180 | 245.5 | 42.9 | 250 | 53.98 | 0.661 | 115.0 | 50.38 | 130.8 | 89.0 |
| 15 | 167 | 198 | 259.0 | 40.1 | 250 | 53.98 | 0.690 | 115.0 | 50.76 | 136.6 | 88.0 |

NOTE: Study point at 2 meters above ground (or rooftop, see write-up) level.

RESULTS: COLUMN J DISTANCES ARE LESS THAN COLUMN C AND COLUMN K DISTANCES ARE LESS THAN COLUMN A DISTANCES IN ALL INSTANCES; THEREFORE, INTERFERING SIGNAL DOES NOT EXIST AT ANY LOCATION (TWO METERS OR LESS ABOVE GROUND LEVEL)