

ENGINEERING REPORT:

APPLICATION FOR NEW FM BOOSTER STATION
for
KUFX (FM) CHANNEL 253B, 98.5 MHz
SAN JOSE, CA

CITICASTERS LICENSES, INC.

1/2002

Table of Contents

1. Purpose of Report
2. Facilities Proposed
3. Service Area
4. Interference
5. NEIR Study
6. Directional Antenna Data
 - a. Directional Antenna Envelope Pattern Plot
 - b. Directional Antenna Envelope Tabulate Data
 - c. Directional Antenna Vertical Plane Relative Field Pattern
7. Exhibits
 - a. Exhibit 1-A Transmitter Site Map
 - b. Exhibit 6 HAAT Tabulated Data
 - c. Exhibit 11-A KUFX vs. Proposed FM Booster Service Contour Plot
 - d. Exhibit 12-A1 73.207 FM Spacing Study
 - e. Exhibit 12-A1B TV Channel 6 Spacing Study
 - f. Exhibit 12-A2A First Adjacent Channel Study
 - g. Exhibit 12-A2B First Adjacent Channel Contour Plot
 - h. Exhibit 15-A1 Proposed Booster Vertical Plane Relative Field Tabulated Data
 - i. Exhibit 15-A2 KISQ-FM2 Vertical Plane Relative Field Tabulated Data

1. Purpose of Report

This Engineering Report is part of an application for a new FM Booster station for FM Station KUFX San Jose, CA by Citicasters Licenses, Inc.

2. Facilities Proposed

The proposed operation will be an FM Booster Station on FM Channel 253 (98.5 MHz) with a maximum lobe effective radiated power of 2.8 kilowatts (vertical only) and antenna height above average terrain of –63.36 meters. Operation is proposed with a vertically polarized Scala CL-FM/VAM composite antenna side mounted on a 23 meter wooden pole. The proposed FM Booster site location is shown in Exhibit 1-A of this report. Tabulated height above average terrain data is shown in Exhibit 6 of this report.

3. Service Area

The proposed FM Booster station complies with 47 C.F.R. Section 74.1232 (f). The service contour of the proposed FM Booster station falls completely within the protected coverage contour for KUFX. The location of the protected contour for KUFX and the service contour for the proposed FM Booster station are shown in Exhibit 11-A of this report.

4. Interference

The proposed operation complies with the applicable sections of 47 C.F.R. Section 74.1204.

Specifically, the proposed FM Booster station complies with 47 C.F.R. Section 74.1204 (g). The proposed operation meets the required separation distances set out in section 73.207 for stations 53 or 54 channels removed. An FM Spacing Study is included as Exhibit 12-A1 of this report. The proposed FM Booster station was treated as its FM radio station broadcast station equivalent (class A) as determined by 47 C.F.R. Section 73.210 and 73.211. The study reveals no short spacings to any station 53 or 54 channels removed from the proposed FM Booster station. In addition, a TV Channel 6 Spacing Study is included as Exhibit 12-A1B of this report to show compliance with 47 C.F.R. 73.207 (c). The proposed FM Booster station was treated as its FM radio station broadcast station equivalent (class A) as determined by 47 C.F.R. Section 73.210 and 73.211.

Specifically, the proposed FM Booster station complies with 47 C.F.R Section 74.1204 (i). The proposed operation meets the requirement that the signal of any first adjacent station must exceed the signal of the booster station by 6 dB at all points within the protected contour of any first adjacent channel station. A tabulation of all first adjacent stations located within a 200 km radius of the proposed FM Booster station is shown in Exhibit 12-A2A of this report. The protected contours of each first adjacent station and the service contour of the proposed FM Booster station are shown in Exhibit 12-A2B of this report.

The proposed FM Booster station will not operate in the reserved band (channels 201-220) and thus is not required to comply with 47 C.F.R. Section 74.1205.

5. NIER Study

In addition to the proposed FM Booster station, FM Booster station KISQ-FM2 is located on the proposed site. This is a controlled access site.

The power density calculations for this report were made in accordance with the methods outlined in the report "Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields" (OET Bulletin 65 Edition 97-1 August 1997). All calculations are based on vertical plane relative field data supplied by the manufacturer of the antennas and follow the procedure shown in OET Bulletin 65.

The following equation from OET Bulletin 65 Edition 97-1 was used to calculate the ground level power density from each antenna at incremental distances from the base of the supporting structure out to 500 meters:

Formula (7) from Section II of OET 65:

$$S = (2.56) (EIRP) / (4) (\pi) (R)^2$$

Where:

S = Highest power density (mW/cm^2) at ground level

R = Distance from center antenna to ground in cm,

EIRP = 1.64 times ERP relative to dipole in mW,

Proposed FM Booster Station NIER Analysis

The calculated power density from the proposed FM Booster station utilizes vertical plane relative field data provided by the manufacturer for the Scala CL-FM/VAM antenna array. Tabulated vertical plane relative field data is provided in Exhibit 15-A1. The highest calculated ground level power density occurs 14 meters from the base of the supporting structure. The power density at this point is calculated to be 0.0246 mW/cm². This is 2.5% of 1 mW/cm² which is the ANSI standard for controlled environments such as this one. This is 12.3% of 0.2 mW/cm² which is the ANSI standard for uncontrolled environments.

Station: proposed FM Booster with antenna up 13 meters and ERP 2.8 kW

$$S = \frac{(2.56) (1.64) (1000) (2,800) (0.310)^2}{(4) (3.14) (1,910)^2}$$

Max field 0.31, 54 deg down at 14 meters horizontal.

MAX S = 1.0 mW/cm² for FM station between 88 and 108 mHz

ERP = (horizontal plus vertical times field factor².)

S = 0.0246 mW/cm², 2.5 % of Controlled Exposure allowed.

S = 0.0246 mW/cm², 12.3 % of Uncontrolled Exposure allowed.

KISQ-FM2 NIER Analysis

The calculated power density from the FM Booster station KISQ-FM2 utilizes vertical plane relative field data provided by the manufacturer for the Scala 4CL-FM/CP antenna array. This antenna consists of two cross polarized, horizontal and vertical, antenna arrays. Vertical plane characteristics for each array, horizontal and vertical, were analyzed individually for compliance. Tabulated vertical plane relative field data is provided in Exhibit 15-A2.

The highest calculated ground level power density for the horizontally polarized array occurs 12.0 meters from the base of the supporting structure. The power density at this point is calculated to be 0.0048 mW/cm². This is 0.5% of 1 mW/cm² which is the ANSI standard for controlled environments such as this one. This is 2.4% of 0.2 mW/cm² which is the ANSI standard for uncontrolled environments.

Station: KISQ-FM2 Horizontally polarized array with antenna up 23 meters and ERP 10.0 kW

$$S = \frac{(2.56) (1.64) (1000) (10,000) (0.098)^2}{(4) (3.14) (2,594)^2}$$

Max field 0.10, 65 deg down at 12 meters horizontal.
MAX S = 1.0 mW/cm² for FM station between 88 and 108 mHz
ERP = (horizontal plus vertical times field factor².)

S = 0.0048 mW/cm², 0.5 % of Controlled Exposure allowed.
S = 0.0048 mW/cm², 2.4 % of Uncontrolled Exposure allowed.

The highest calculated ground level power density for the vertically polarized array occurs 29.0 meters from the base of the supporting structure. The power density at this point is calculated to be 0.0052 mW/cm². This is 0.5% of 1 mW/cm² which is the ANSI standard for controlled environments such as this one. This is 2.6% of 0.2 mW/cm² which is the ANSI standard for uncontrolled environments.

Station: KISQ-FM2 Vertically polarized array with antenna up 23 meters and ERP 10.0 kW

$$S = \frac{(2.56) (1.64) (1000) (10,000) (0.146)^2}{(4) (3.14) (3,701)^2}$$

Max field 0.15, 52 deg down at 29 meters horizontal.
MAX S = 1.0 mW/cm² for FM station between 88 and 108 mHz
ERP = (horizontal plus vertical times field factor².)

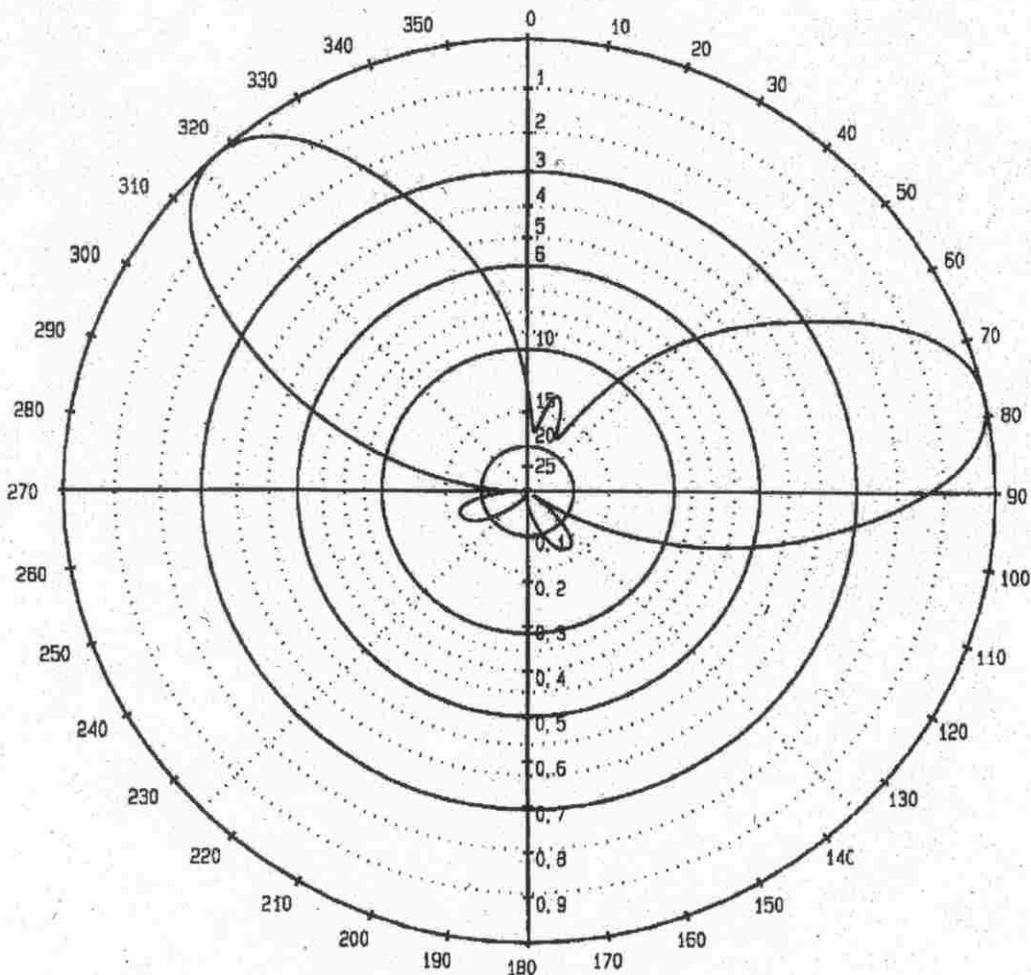
S = 0.0052 mW/cm², 0.5 % of Controlled Exposure allowed.
S = 0.0052 mW/cm², 2.6 % of Uncontrolled Exposure allowed.

Based on the analysis of both the current and proposed operations shown above for this site, the proposed FM booster station complies with 47 C.F.R. Section 1.1306 with regard to maximum permissible radio frequency electromagnetic exposure limits for controlled and uncontrolled environments.

Public access to the site is restricted and the antenna structure is posted with warning signs. Pursuant to OET Bulletin 65, all station personnel and contractors are required to follow appropriate safety procedures before any work is done on the site, including reducing or removing power before any maintenance work begins.

The permittee/licensee, in coordination with other users of the site, must reduce power or cease operation as necessary to protect persons having access to the site, structure or antenna from radio frequency radiation in excess of FCC guidelines.

Proposed FM Booster Station
Directional Antenna Data



frequency in MHz 98.500
 down-tilt in .0
 max / mean in dB 6.24

KSJO / KUFO

SCALA Medford Oregon MB 16.10.11 17:19	2 x 2 CL-FM/VRM Log-Periodic array Frequency: 98.5 Mhz.	Typ Nr. Bl.:

simulation with typical exactness of +/- 8% of max signal

Azimuth Radiation Pattern in % and dB at downtilt: .0

f = 98.500MHz

azimuth	%	dB	azimuth	%	dB
0	23.3	-12.6	180	3.2	-30.0
5	14.1	-17.0	185	2.2	-33.1
10	15.6	-16.2	190	1.2	-38.1
15	21.2	-13.5	195	.8	-41.9
20	21.1	-13.5	200	.8	-41.9
25	15.6	-16.1	205	1.2	-38.2
30	14.1	-17.0	210	2.2	-33.1
35	23.2	-12.7	215	3.2	-29.9
40	35.2	-9.1	220	4.3	-27.2
45	46.4	-6.7	225	6.1	-24.3
50	56.2	-5.0	230	8.3	-21.6
55	65.7	-3.6	235	11.0	-19.2
60	76.3	-2.4	240	13.3	-17.5
65	87.0	-1.2	245	14.8	-16.6
70	95.3	-.4	250	15.4	-16.2
75	99.5	.0	255	14.8	-16.6
80	99.6	.0	260	11.7	-18.7
85	95.2	-.4	265	6.1	-24.3
90	86.1	-1.3	270	2.3	-32.6
95	73.9	-2.6	275	11.4	-18.9
100	60.9	-4.3	280	22.5	-13.0
105	48.0	-6.4	285	35.0	-9.1
110	34.9	-9.1	290	47.9	-6.4
115	22.5	-13.0	295	61.0	-4.3
120	11.4	-18.9	300	73.9	-2.6
125	2.3	-32.6	305	86.1	-1.3
130	6.2	-24.1	310	95.2	-.4
135	11.7	-18.6	315	99.6	.0
140	14.8	-16.6	320	99.5	.0
145	15.4	-16.2	325	95.2	-.4
150	14.7	-16.6	330	87.0	-1.2
155	13.3	-17.5	335	76.3	-2.4
160	11.0	-19.2	340	65.7	-3.6
165	8.3	-21.6	345	56.1	-5.0
170	6.1	-24.3	350	46.4	-6.7
175	4.3	-27.3	355	35.4	-9.0
180	3.2	-30.0	360	23.3	-12.6

maximum fieldstrength was found at:

azimuth 317.
downtilt 0.

KSJO / KUFO

SCALA Medford Oregon	2 x 2 CL-FM/VAM Log-Periodic array	Typ No.
	Frequency: 98.5 Mhz.	Bl.:
MB 16.10.** 17:19		

Dimensions and Feeding of Antenna System

antenna type: K52221. log.-per antenna verti 87.5-108 MHz

operating f in MHz : 98.500 .000 .000 .000 .000
 database f in MHz : 975
 max. azimuth angle 180 max. declination 90 cable design frequency: 98.500 MHz
 compensation in % : .00 .00 .00 .00 .00

bay height	v-feed	power	cab-ph	fix-ph	panel	azipos	azidir	radius	tanoff	radoff	tilt	power	cab-ph	fix-ph
2	3100	1.0	0	0	1	77.0	77.0	254.0	-1000.0	.0	.0	1.0	0	0
					2	77.0	77.0	254.0	1000.0	.0	.0	1.0	0	0
bay height	v-feed	power	cab-ph	fix-ph	panel	azipos	azidir	radius	tanoff	radoff	tilt	power	cab-ph	fix-ph
1	0	1.0	0	0	1	318.0	318.0	254.0	-1000.0	.0	.0	1.0	0	0
					2	318.0	318.0	254.0	1000.0	.0	.0	1.0	0	0

Directivity from HRP and zoomed VRP

operating f in MHz : 98.500 .000 .000 .000 .000
 operating channel : 0 0 0 0 0
 HRP max/mean in dB : 6.24 .00 .00 .00 .00
 VRP omnidir in dB : .90 .00 .00 .00 .00
 directivity in dB : 7.14 .00 .00 .00 .00
 harness losses : .00 .00 .00 .00 .00
 gain in dB : 7.14 .00 .00 .00 .00

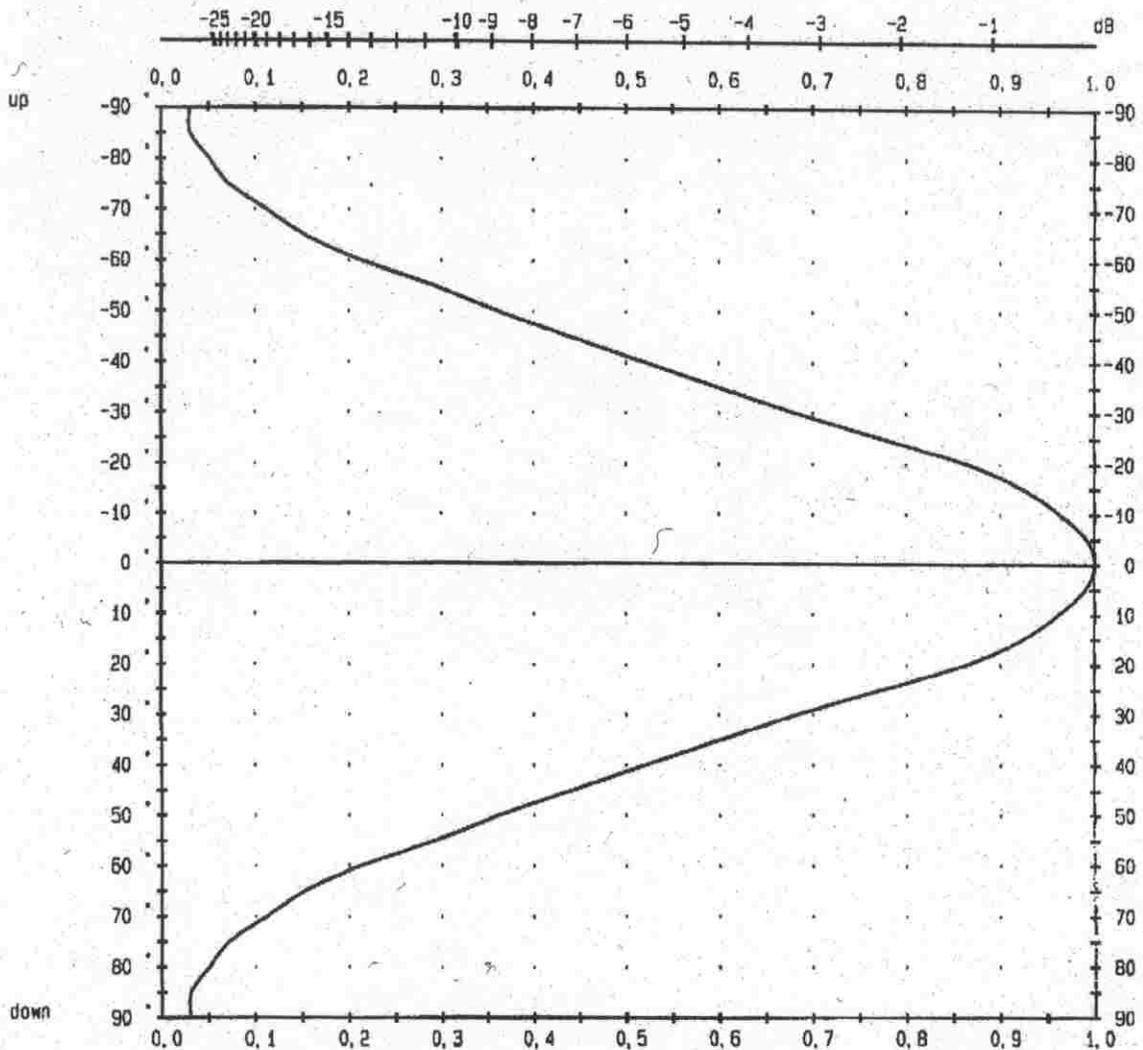
allow +/-0.5 dB tolerance for pattern variations

harness parameters at cable design frequency:

bay feeder : .0 m 4AA034 (a = .00 dB)
 antenna cable: .0 m 4AA034 (a = .00 dB)

KSJO / KUFO

SCALA Medford Oregon	2 x 2 CL-FM/VFM Log-Periodic array	Typ No.
NB 16.10.** 17:19	Frequency: 98.5 Mhz.	B1.

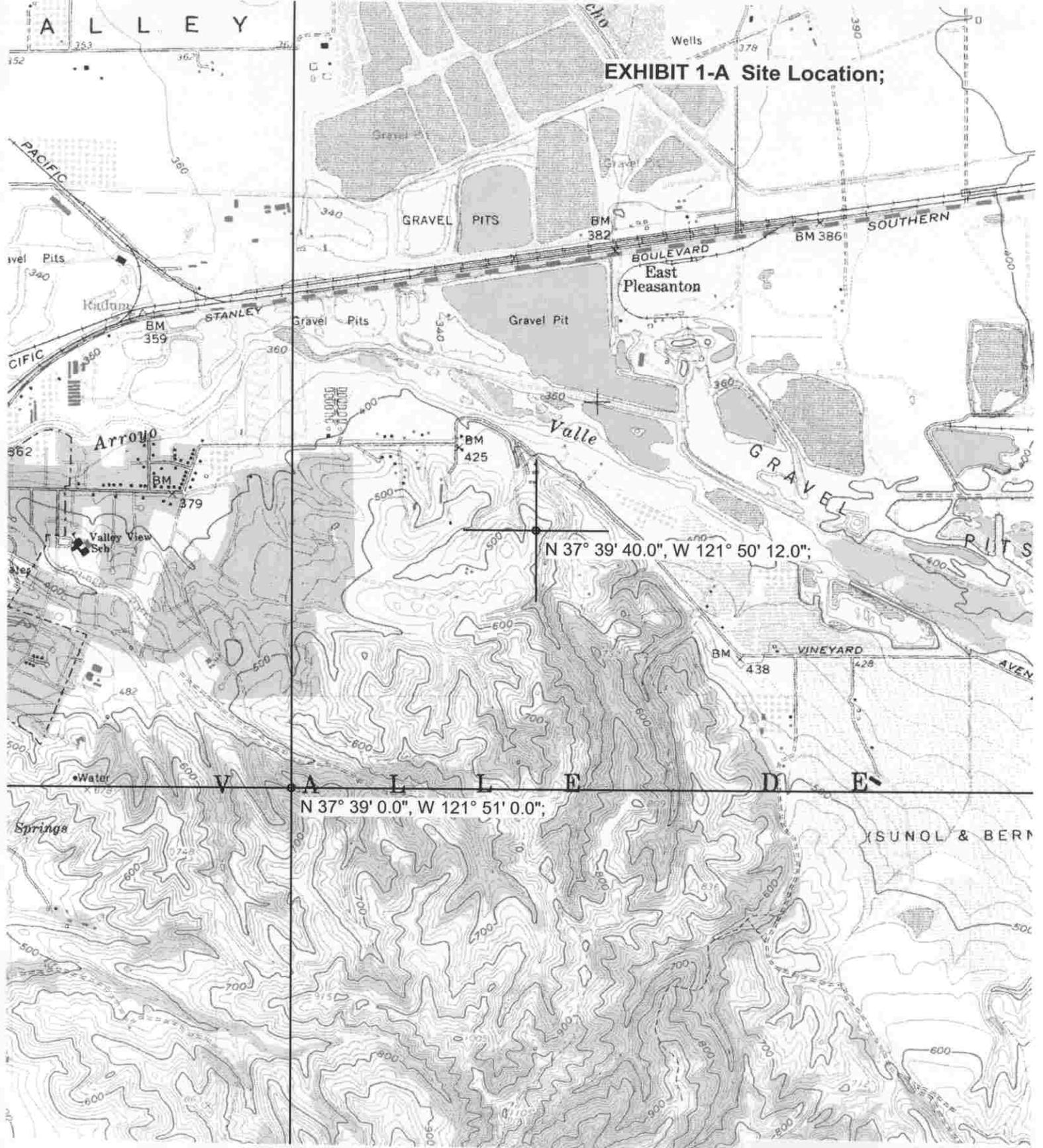


frequency in MHz 98.500
azimut in 78.0
omni-dir in dBd .90

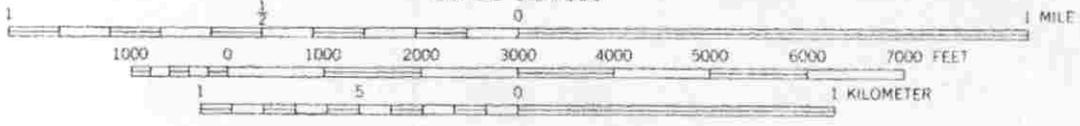
KSJO / KUFO

SCALA Medford Oregon	2 x 2 CL-FM/VAM Log-Periodic array	Typ Nr.
MB 16.10.** 17: 19	Frequency: 98.5 Mhz.	01.:

EXHIBITS



SCALE 1:24000



CONTOUR INTERVAL 20 FEET
 DOTTED LINES REPRESENT 10-FOOT CONTOURS
 NATIONAL GEODETIC VERTICAL DATUM OF 1929

LIVERMORE, CALIF.
 NE/4 LIVERMORE 15' QUADRANGLE
 N3737.5—W12145/7.5

1961
 PHOTOREVISED 1980
 DMA 1659 III NE SERIES V895

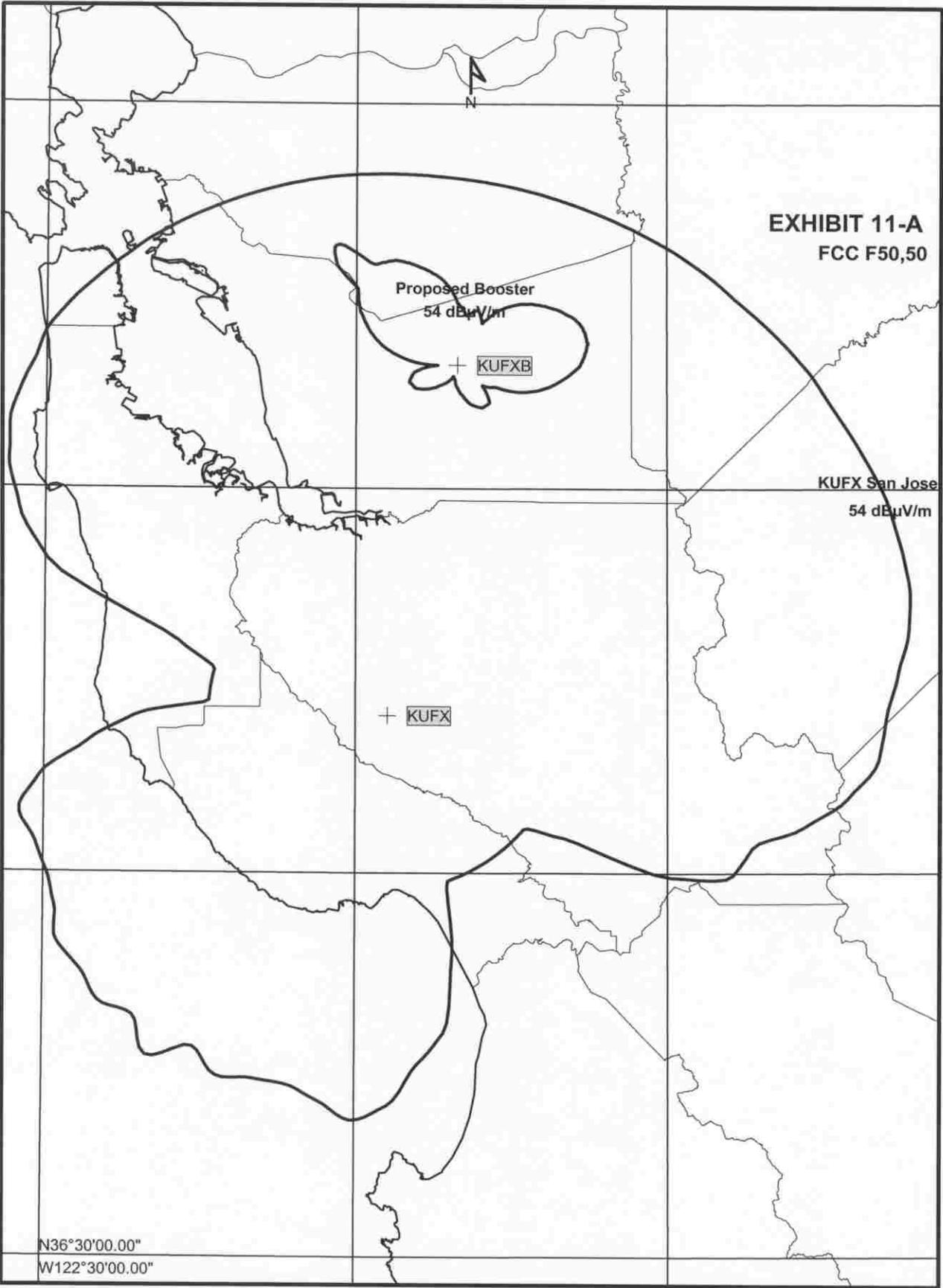


EXHIBIT 11-A
FCC F50,50

Proposed Booster
54 dBuV/m

+ KUFXB

KUFX San Jose
54 dBuV/m

+ KUFX

N36°30'00.00"
W122°30'00.00"

FM Study for: Proposed Booster FCC DB Date: 12/20/2001 37-39-40
 Location: PLEASANTON, CA Channel Class: A 121-50-12
 [*] by HAAT indicates calculated as missing in database.
 [*] by HAAT indicates value taken from 1999 VAX file.
 Call City, State Chan Class Freq kW Latitude Dist. Required
 Status Proponent File Number HAAT Longitude Azm. Clear (km)

 >>>>>>> Study For Channel 253 98.5 MHz <<<<<<<<

KUFX	SAN JOSE, CA	253 B	98.5	10.0	37-12-17	51.6	178	
LIC	Fac. No. 65415	BMLH-20010711AC0	268		121-56-56	191.1	-126.4	SHORT
		Use of 73.215 for short spacing			requires: 143		-91.4	SHORT
KRXQ	SACRAMENTO, CA	253 B	98.5	50.0	38-38-53	127.3	178	
LIC	Fac. No. 20354	BLH-19931005KB	151		121-05-51	30.4	-50.7	SHORT
		Use of 73.215 for short spacing			requires: 143		-15.7	SHORT
KSOL	SAN FRANCISCO, CA	255 B	98.9	6.10	37-45-19	55.2	69	
LIC	Fac. No. 70032	BLH-19990723KF	409		122-27-06	281.1	-13.8	SHORT
		Use of 73.215 for short spacing			requires: 63		-7.8	SHORT
KZOL	SANTA CRUZ, CA	256 B	99.1	1.10+	37-06-39	61.1	69	
LIC	Fac. No. 70033	BLH-19900116KE	796		121-50-37	180.6	-7.9	SHORT
		Use of 73.215 for short spacing			requires: 63		-1.9	SHORT
KISQ	SAN FRANCISCO, CA	251 B	98.1	100.	37-51-04	61.9	69	
LIC	Fac. No. 59964	BLH-19871207KE	293		122-29-49	290.1	-7.1	SHORT
		Use of 73.215 for short spacing			requires: 63		-1.1	SHORT
KISQ	SAN FRANCISCO, CA	251 B	98.1	100.	37-51-04	61.9	69	
LIC	Fac. No. 59964	BMLH-20000830AFM	293		122-29-49	290.1	-7.1	SHORT
		Use of 73.215 for short spacing			requires: 63		-1.1	SHORT
KWNN	TURLOCK, CA	252 A	98.3	2.00	37-34-46	87.9	72	
LIC	Fac. No. 60427	BLH-19871001KC	119		120-50-48	95.6	+15.9	CLEAR

12-22-2001

EXHIBIT 12-A1B

PAGE 1

TV Channel 6 Spacing Study

TV Study for: Proposed Booster FCC DB Date: 12/20/2001 37-39-40

Location: PLEASANTON, CA ZONE: 2 121-50-12

CALL STATUS	LOCATION STATE	CHANNEL ZONE	ERP:KW(DA) HAAT	LATITUDE LONGITUDE	DISTANCE BEARING	REQUIRED CLEAR (km)
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>>>>>>> Study For Channel: 6 <<<<<<<<

KVIQ LIC TV	EUREKA, CA BLCT-1115	6 - ZONE:2	100. 530	40-43-36 123-58-18	387.1 332.2	22.0 +365.1	CLEAR
KSBY LIC TV	SAN LUIS OBISPO, CA BLCT-1159	6 + ZONE:2	100. 543	35-21-37 120-39-17	276.4 157.1	22.0 +254.4	CLEAR
KVIE CP TV	SACRAMENTO, CA BPET-19990927ABV	6 Z ZONE:2	100. 550	38-16-18 121-30-22	73.7 23.1	22.0 +51.7	CLEAR
KVIE LIC TV	SACRAMENTO, CA BLET-19861201L1	6 Z ZONE:2	100. 567	38-16-18 121-30-18	73.8 23.2	22.0 +51.8	CLEAR

12-22-2001

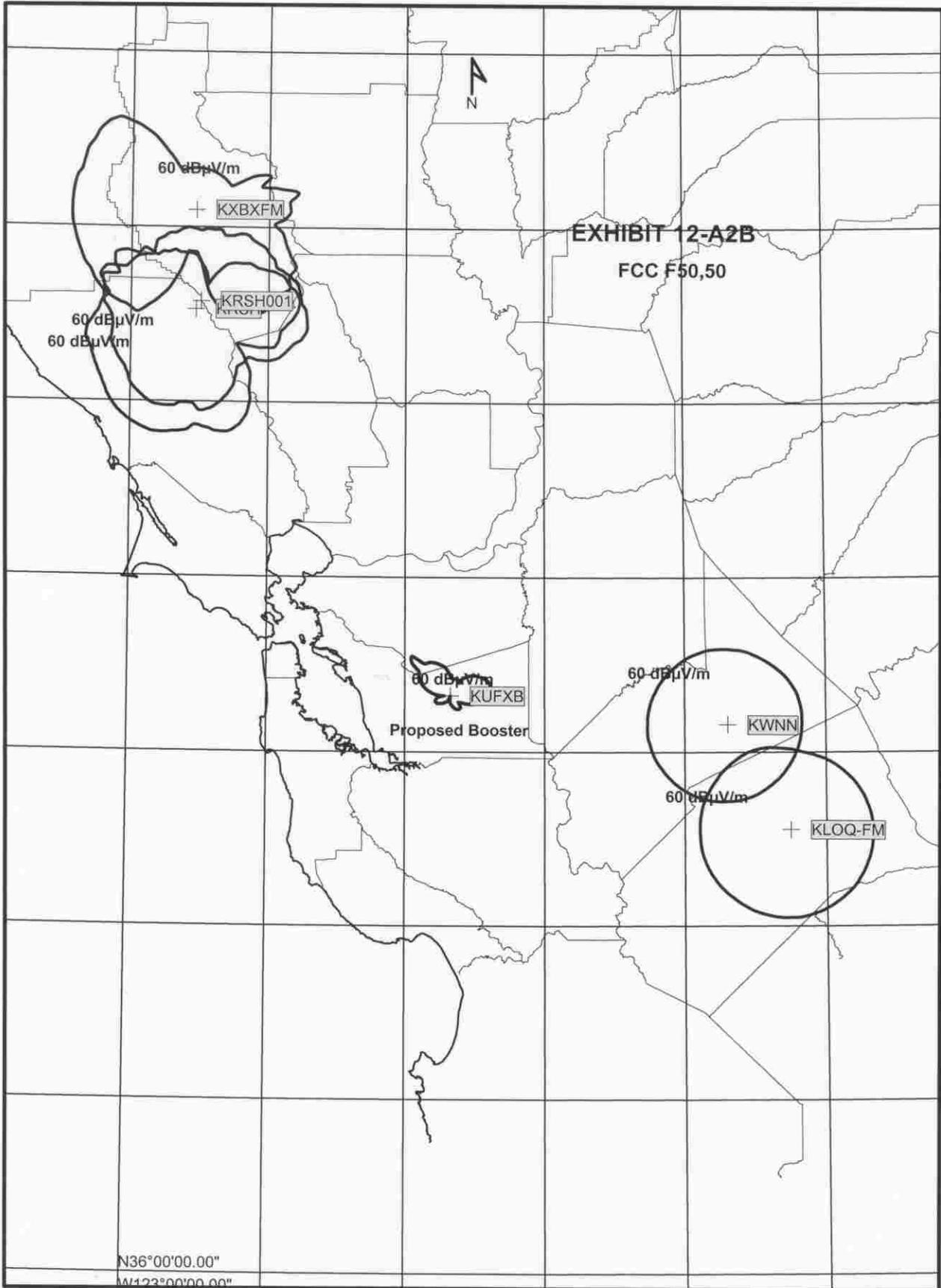
EXHIBIT 12-A2A
First Adjacent Channel Study

PAGE 1

1st Adj Study for: Proposed Booster FCC DB Date: 12/20/2001 37-39-40
 Location: Pleasanton, CA Channel Class: D 121-50-12
 [*] by HAAT indicates calculated as missing in database.
 [^] by HAAT indicates value taken from 1999 VAX file.
 Call City, State Chan Class Freq kW Latitude Dist.
 Status Proponent File Number HAAT Longitude Azm.

 >>>>>>> Study For Channel 253 98.5 MHz <<<<<<<<<
 All first adjacent stations within 200 km of proposed coordinates

KWNN	TURLOCK, CA	252 A	98.3	2.00	37-34-46	87.9
LIC	Fac. No. 60427	BLH-19871001KC	119		120-50-48	95.6
KLOQFM	WINTON, CA	254 A	98.7	6.00	37-16-41	115.2
LIC	Fac. No. 65374	BLH-19990119KH	91		120-37-35	111.3
KRSH	MIDDLETOWN, CA	254 A	98.7	.340	38-45-55	147.1
CP	Fac. No. 72925	BMPH-19930406IA	420		122-45-54	326.7
KRSH	MIDDLETOWN, CA	254 A	98.7	.165	38-47-16	148.3
CP	Fac. No. 72925	BPH-19990329IF	572		122-44-50	327.8
KXBXFM	LAKEPORT, CA	252 A	98.3	4.80	39-02-56	174.2
LIC	Fac. No. 49198	BLH-20010207AAH	112		122-46-03	332.4



sxsc1fm-vrm98

327.00	92.4	-.7
328.00	90.8	-.8
329.00	88.9	-1.0
330.00	87.0	-1.2
331.00	84.9	-1.4
332.00	82.8	-1.6
333.00	80.7	-1.9
334.00	78.5	-2.1
335.00	76.2	-2.4
336.00	74.1	-2.6
337.00	71.9	-2.9
338.00	69.7	-3.1
339.00	67.6	-3.4
340.00	65.7	-3.6
341.00	63.7	-3.9
342.00	61.9	-4.2
343.00	60.0	-4.4
344.00	58.0	-4.7
345.00	56.2	-5.0
346.00	54.3	-5.3
347.00	52.4	-5.6
348.00	50.3	-6.0
349.00	48.4	-6.3
350.00	46.3	-6.7
351.00	44.2	-7.1
352.00	42.1	-7.5
353.00	39.9	-8.0
354.00	37.7	-8.5
355.00	35.2	-9.1
356.00	33.0	-9.6
357.00	30.6	-10.3
358.00	28.1	-11.0
359.00	25.7	-11.8
360.00	23.3	-12.7

AZIMUTH ANGLE FOR VRP : 317.0

ELEVATION RELATIVE FIELD
 (°) (%) (dB)

HORIZON → .00	100.0	.0
-1.00	99.9	.0
-2.00	99.8	.0
-3.00	99.6	.0
-4.00	99.4	-.1
-5.00	99.0	-.1
-6.00	98.6	-.1
-7.00	98.0	-.2
-8.00	97.5	-.2
-9.00	96.8	-.3
-10.00	96.1	-.3

sxsclfm-frm98

-11.00	95.5	-.4
-12.00	94.8	-.5
-13.00	94.0	-.5
-14.00	93.2	-.6
-15.00	92.3	-.7
-16.00	91.3	-.8
-17.00	90.3	-.9
-18.00	89.1	-1.0
-19.00	87.8	-1.1
-20.00	86.4	-1.3
-21.00	84.8	-1.4
-22.00	83.0	-1.6
-23.00	81.2	-1.8
-24.00	79.3	-2.0
-25.00	77.4	-2.2
-26.00	75.5	-2.4
-27.00	73.7	-2.7
-28.00	71.8	-2.9
-29.00	70.0	-3.1
-30.00	68.2	-3.3
-31.00	66.6	-3.5
-32.00	64.9	-3.8
-33.00	63.3	-4.0
-34.00	61.7	-4.2
-35.00	60.1	-4.4
-36.00	58.5	-4.7
-37.00	56.9	-4.9
-38.00	55.3	-5.1
-39.00	53.7	-5.4
-40.00	52.1	-5.7
-41.00	50.5	-5.9
-42.00	48.9	-6.2
-43.00	47.3	-6.5
-44.00	45.7	-6.8
-45.00	44.1	-7.1
-46.00	42.5	-7.4
-47.00	40.9	-7.8
-48.00	39.3	-8.1
-49.00	37.7	-8.5
-50.00	36.2	-8.8
-51.00	34.8	-9.2
-52.00	33.4	-9.5
-53.00	32.1	-9.9
-54.00	30.7	-10.3
-55.00	29.3	-10.7
-56.00	27.7	-11.2
-57.00	26.0	-11.7
-58.00	24.4	-12.2

sxscifm-vrm98

-59.00	22.8	-12.8
-60.00	21.3	-13.4
-61.00	19.9	-14.0
-62.00	18.7	-14.6
-63.00	17.5	-15.2
-64.00	16.3	-15.7
-65.00	15.3	-16.3
-66.00	14.4	-16.8
-67.00	13.5	-17.4
-68.00	12.7	-17.9
-69.00	12.0	-18.4
-70.00	11.2	-19.0
-71.00	10.4	-19.7
-72.00	9.5	-20.5
-73.00	8.7	-21.3
-74.00	7.9	-22.1
-75.00	7.2	-22.9
-76.00	6.7	-23.5
-77.00	6.2	-24.1
-78.00	5.8	-24.7
-79.00	5.5	-25.3
-80.00	5.1	-25.8
-81.00	4.6	-26.7
-82.00	4.2	-27.6
-83.00	3.8	-28.5
-84.00	3.4	-29.4
-85.00	3.1	-30.3
-86.00	3.0	-30.6
-87.00	2.9	-30.6
-88.00	3.0	-30.6
-89.00	3.0	-30.5
-90.00	3.1	-30.3

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TWO CL-FM LOG-PERIODICS, VERTICAL STACKED
 HORIZONTAL POLARIZATION - VERTICAL PLANE PATTERN

Azimuth	Relative Field	Relative dB	dBd	Power Gain
90	1.000	0.0	9.5	8.913
91	0.998	-0.0	9.5	8.913
92	0.995	-0.0	9.5	8.913
93	0.990	-0.1	9.4	8.710
94	0.984	-0.1	9.4	8.710
95	0.977	-0.2	9.3	8.511
96	0.967	-0.3	9.2	8.318
97	0.956	-0.4	9.1	8.128
98	0.944	-0.5	9.0	7.943
99	0.930	-0.6	8.9	7.762
100	0.915	-0.8	8.7	7.413
101	0.897	-0.9	8.6	7.244
102	0.878	-1.1	8.4	6.918
103	0.858	-1.3	8.2	6.607
104	0.836	-1.6	7.9	6.166
105	0.815	-1.8	7.7	5.888
106	0.791	-2.0	7.5	5.623
107	0.766	-2.3	7.2	5.248
108	0.741	-2.6	6.9	4.898
109	0.715	-2.9	6.6	4.571
110	0.689	-3.2	6.3	4.266
111	0.661	-3.6	5.9	3.890
112	0.634	-4.0	5.5	3.548
113	0.606	-4.4	5.1	3.236
114	0.578	-4.8	4.7	2.951
115	0.549	-5.2	4.3	2.692
116	0.520	-5.7	3.8	2.399
117	0.491	-6.2	3.3	2.138
118	0.462	-6.7	2.8	1.905
119	0.433	-7.3	2.2	1.660
120	0.405	-7.8	1.7	1.479
121	0.377	-8.5	1.0	1.259
122	0.349	-9.2	0.3	1.072
123	0.321	-9.9	-0.4	0.912
124	0.294	-10.6	-1.1	0.776
125	0.269	-11.4	-1.9	0.646
126	0.243	-12.3	-2.8	0.525
127	0.218	-13.2	-3.7	0.427
128	0.194	-14.2	-4.7	0.339
129	0.171	-15.3	-5.8	0.263
130	0.149	-16.5	-7.0	0.200
131	0.128	-17.9	-8.4	0.145
132	0.107	-19.4	-9.9	0.102
133	0.087	-21.2	-11.7	0.068
134	0.069	-23.3	-13.8	0.042
135	0.051	-25.9	-16.4	0.023
136	0.034	-29.3	-19.8	0.010
137	0.018	-34.7	-25.2	0.003
138	0.010	-40.0	-30.5	0.001
139	0.010	-40.0	-30.5	0.001
140	0.023	-32.9	-23.4	0.005

TWO CL-FM LOG-PERIODICS, VERTICAL STACKED
HORIZONTAL POLARIZATION - VERTICAL PLANE PATTERN

Azimuth	Relative Field	Relative dB	dBd	Power Gain
141	0.034	-29.3	-19.8	0.010
142	0.045	-26.9	-17.4	0.018
143	0.055	-25.2	-15.7	0.027
144	0.064	-23.9	-14.4	0.036
145	0.071	-22.9	-13.4	0.046
146	0.078	-22.1	-12.6	0.055
147	0.084	-21.5	-12.0	0.063
148	0.089	-21.0	-11.5	0.071
149	0.094	-20.6	-11.1	0.078
150	0.097	-20.2	-10.7	0.085
151	0.099	-20.1	-10.6	0.087
152	0.100	-20.0	-10.5	0.089
153	0.101	-19.9	-10.4	0.091
154	0.100	-20.0	-10.5	0.089
155	0.099	-20.1	-10.6	0.087
156	0.096	-20.4	-10.9	0.081
157	0.092	-20.7	-11.2	0.076
158	0.087	-21.2	-11.7	0.068
159	0.081	-21.8	-12.3	0.059
160	0.075	-22.5	-13.0	0.050
161	0.071	-23.0	-13.5	0.045
162	0.066	-23.6	-14.1	0.039
163	0.061	-24.3	-14.8	0.033
164	0.055	-25.2	-15.7	0.027
165	0.049	-26.2	-16.7	0.021
166	0.045	-27.0	-17.5	0.018
167	0.040	-28.0	-18.5	0.014
168	0.035	-29.2	-19.7	0.011
169	0.029	-30.6	-21.1	0.008
170	0.024	-32.4	-22.9	0.005
171	0.022	-33.0	-23.5	0.004
172	0.021	-33.7	-24.2	0.004
173	0.019	-34.5	-25.0	0.003
174	0.017	-35.4	-25.9	0.003
175	0.015	-36.4	-26.9	0.002
176	0.015	-36.4	-26.9	0.002
177	0.015	-36.4	-26.9	0.002
178	0.015	-36.3	-26.8	0.002
179	0.015	-36.3	-26.8	0.002
180	0.015	-36.3	-26.8	0.002

TWO CL-FM LOG-PERIODICS, VERTICAL STACKED
 VERTICAL POLARIZATION - VERTICAL PLANE PATTERN

Azimuth	Relative Field	Relative dB	dBd	Power Gain
90	1.000	0.0	9.5	8.913
91	0.995	-0.0	9.5	8.913
92	0.987	-0.1	9.4	8.710
93	0.976	-0.2	9.3	8.511
94	0.963	-0.3	9.2	8.318
95	0.948	-0.5	9.0	7.943
96	0.928	-0.6	8.9	7.762
97	0.906	-0.9	8.6	7.244
98	0.882	-1.1	8.4	6.918
99	0.856	-1.4	8.1	6.457
100	0.828	-1.6	7.9	6.166
101	0.794	-2.0	7.5	5.623
102	0.759	-2.4	7.1	5.129
103	0.722	-2.8	6.7	4.677
104	0.684	-3.3	6.2	4.169
105	0.646	-3.8	5.7	3.715
106	0.604	-4.4	5.1	3.236
107	0.562	-5.0	4.5	2.818
108	0.520	-5.7	3.8	2.399
109	0.478	-6.4	3.1	2.042
110	0.436	-7.2	2.3	1.698
111	0.394	-8.1	1.4	1.380
112	0.352	-9.1	0.4	1.096
113	0.311	-10.1	-0.6	0.871
114	0.272	-11.3	-1.8	0.661
115	0.233	-12.6	-3.1	0.490
116	0.196	-14.2	-4.7	0.339
117	0.159	-15.9	-6.4	0.229
118	0.125	-18.1	-8.6	0.138
119	0.092	-20.7	-11.2	0.076
120	0.061	-24.3	-14.8	0.033
121	0.031	-30.1	-20.6	0.009
122	0.010	-40.0	-30.5	0.001
123	0.022	-33.0	-23.5	0.004
124	0.047	-26.6	-17.1	0.019
125	0.069	-23.2	-13.7	0.043
126	0.089	-21.0	-11.5	0.071
127	0.108	-19.4	-9.9	0.102
128	0.124	-18.1	-8.6	0.138
129	0.139	-17.2	-7.7	0.170
130	0.151	-16.4	-6.9	0.204
131	0.161	-15.9	-6.4	0.229
132	0.168	-15.5	-6.0	0.251
133	0.173	-15.2	-5.7	0.269
134	0.177	-15.1	-5.6	0.275
135	0.178	-15.0	-5.5	0.282
136	0.178	-15.0	-5.5	0.282
137	0.176	-15.1	-5.6	0.275
138	0.172	-15.3	-5.8	0.263
139	0.166	-15.6	-6.1	0.245
140	0.159	-16.0	-6.5	0.224

TWO CL-FM LOG-PERIODICS, VERTICAL STACKED
 VERTICAL POLARIZATION - VERTICAL PLANE PATTERN

Azimuth	Relative Field	Relative dB	dBd	Power Gain
141	0.153	-16.3	-6.8	0.209
142	0.145	-16.7	-7.2	0.191
143	0.137	-17.3	-7.8	0.166
144	0.127	-17.9	-8.4	0.145
145	0.116	-18.7	-9.2	0.120
146	0.108	-19.3	-9.8	0.105
147	0.100	-20.0	-10.5	0.089
148	0.091	-20.8	-11.3	0.074
149	0.081	-21.8	-12.3	0.059
150	0.071	-23.0	-13.5	0.045
151	0.065	-23.7	-14.2	0.038
152	0.059	-24.5	-15.0	0.032
153	0.053	-25.5	-16.0	0.025
154	0.047	-26.6	-17.1	0.019
155	0.040	-27.9	-18.4	0.014
156	0.036	-28.8	-19.3	0.012
157	0.032	-29.9	-20.4	0.009
158	0.028	-31.2	-21.7	0.007
159	0.023	-32.7	-23.2	0.005
160	0.019	-34.6	-25.1	0.003
161	0.017	-35.4	-25.9	0.003
162	0.015	-36.4	-26.9	0.002
163	0.013	-37.5	-28.0	0.002
164	0.011	-38.8	-29.3	0.001
165	0.010	-40.0	-30.5	0.001
166	0.010	-40.0	-30.5	0.001
167	0.010	-40.0	-30.5	0.001
168	0.010	-40.0	-30.5	0.001
169	0.010	-40.0	-30.5	0.001
170	0.010	-40.0	-30.5	0.001
171	0.010	-40.0	-30.5	0.001
172	0.010	-40.0	-30.5	0.001
173	0.010	-40.0	-30.5	0.001
174	0.010	-40.0	-30.5	0.001
175	0.010	-40.0	-30.5	0.001
176	0.010	-40.0	-30.5	0.001
177	0.010	-40.0	-30.5	0.001
178	0.010	-40.0	-30.5	0.001
179	0.010	-40.0	-30.5	0.001
180	0.010	-40.0	-30.5	0.001