

ENGINEERING STATEMENT
REQUEST FOR MODIFICATION OF CONSTRUCTION PERMIT
(FCC FILE NO. BMPEDT-20040730AKR)
ON BEHALF OF
MONTANA STATE UNIVERSITY
KUSM-DT, BOZEMAN, MONTANA
CHANNEL 8 17.9 KW MAX ERP 271 METERS HAAT

MARCH 2005

COHEN, DIPPELL AND EVERIST, P.C.
CONSULTING ENGINEERS
RADIO AND TELEVISION
WASHINGTON, D.C.

COHEN, DIPPELL AND EVERIST, P. C.

City of Washington)
District of Columbia) ss

Donald G. Everist, being duly sworn upon his oath, deposes and states that:

He is a graduate electrical engineer, a Registered Professional Engineer in the District of Columbia, and is President, Secretary and Treasurer of Cohen, Dippell and Everist, P.C., Consulting Engineers, Radio - Television, with offices at 1300 L Street, N.W., Suite 1100, Washington, D.C. 20005;

That his qualifications are a matter of record in the Federal Communications Commission:

That the attached engineering report was prepared by him or under his supervision and direction and

That the facts stated herein are true of his own knowledge, except such facts as are stated to be on information and belief, and as to such facts he believes them to be true.

Donald G. Everist
District of Columbia
Professional Engineer
Registration No. 5714

Subscribed and sworn to before me this 29th day of March, 2005.



My Commission Expires:

My Commission Expires: 2/28/2008

COHEN, DIPPELL AND EVERIST, P. C.

City of Washington)
)
) ss
District of Columbia)

Martin R. Doczkat being duly sworn upon his oath, deposes and states that:

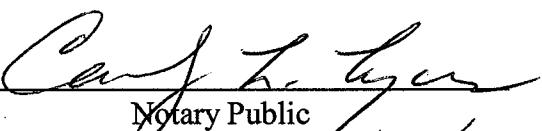
He is a graduate electrical engineer of the Pennsylvania State University, and is a staff engineer at Cohen, Dippell and Everist, P.C., Consulting Engineers, Radio - Television, with offices at 1300 L Street, N.W., Suite 1100, Washington, D.C. 20005;

That the attached engineering report was prepared by him or under his supervision and direction and

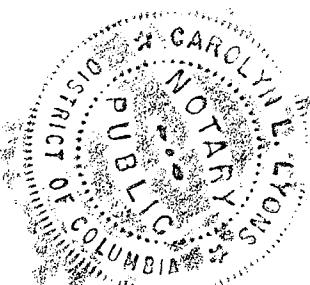
That the facts stated herein are true of his own knowledge, except such facts as are stated to be on information and belief, and as to such facts he believes them to be true.


Martin R. Doczkat

Subscribed and sworn to before me this 29th day of March, 2005.


Carolyn L. Taylor
Notary Public

My Commission Expires: 3/26/2008



INTRODUCTION

This report has been prepared on behalf of Montana State University, licensee of KUSM(TV), in support of its request to modify its construction permit (FCC File No. BPRM-20010215ABK) for DTV facilities at the Green Mountain electronics site.

TRANSMITTER SITE

It is proposed to top-mount a master antenna to an existing guyed tower. The proposed operation will implement a broadband antenna and accept the input from the proposed DTV Channel 8 and a DTV Channel 13 operation. The DTV antenna will be mounted on an existing tower with FCC Tower Registration Number 1000681. Exhibit E-1 depicts the vertical elevation for the tower and master antennas.

North Latitude: 45° 40' 24"

West Longitude: 110° 52' 02"

NAD-27

POWER AND EQUIPMENT DATA

| | | |
|--|---------|-----------|
| Transmitter output | 1.8 kW | 2.55 dBk |
| Combiner efficiency/loss | 0.955 | 0.2 dB |
| Transmission line efficiency/loss Type EIA/DCA 3-1/8" 50 ohm, or equivalent, 100 meters (328 feet) | 0.882 | 0.544 dB |
| Antenna input | 1.52 kW | 1.81 dBk |
| Antenna gain | 11.8 | 10.73 |
| Maximum Effective Radiated Power (ERP) | 17.9 kW | 12.54 dBk |

ELEVATION DATA

| | |
|---|--------------------------------|
| Vertical dimension of the Channel 8 antenna | 6.2 Meters (20.4 Feet) |
| Elevation of site above mean sea level | 2015 Meters (6610.9 Feet) |
| Overall height above ground of the existing antenna structure including all appurtenances | 106.7 Meters (350 Feet) |
| Overall height above mean sea level of existing antenna structure including all appurtenances | 2121.7 Meters (6960.9 Feet) |
| Center of radiation of antenna above ground | 95.8 Meters (314.3 Feet) |
| Center of radiation of antenna above mean sea level | 2110.8 Meters (6925.2 Feet) |
| Antenna height above average terrain | 271 Meters |

Note: Slight height differences result due to rounding and conversion between units.

The proposed antenna is a Dielectric, Type THA-P2-2H/4HD-1, or the equivalent. This is a directional antenna implementing a “peanut” shaped pattern. All exhibits required by Section 73.625 of the Commission’s rules have been included as Exhibit E-2.

ALLOCATION AND INTERFERENCE ANALYSIS

A DTV allocation study was not performed from the proposed site since the facilities requested are less than that authorized by the construction permit, and therefore, an interference analysis is not required.

COVERAGE

The average elevation data for 3.2 to 16.1 kilometers along each radial equally spaced at 10° has been determined based upon 3-second terrain data. Utilizing the formula in Section 73.625(b)(2)

of the rules for the effective heights, the depression angle is determined to vary from 0.090 to 0.675 degrees. The relative field in the vertical plane is greater than 90% for all calculated depression angles; accordingly, the maximum power was used to determine the distance to the DTV noise limited contour. Table I provides a tabulation of the azimuth at every ten degrees beginning at True North, the effective radiated power in kW and the distance to each contour in km. A map is included as Exhibit E-3 of this report showing the predicted 43 and 36 dBu contours.

Radio Frequency Field Level

This section evaluates the radio frequency field (“RFF”) exposure condition created by the operation of the proposed KUSM-DT operation.

The RFF study will consider the following stations:

| | |
|----------|------------|
| KUSM-DT | Channel 8 |
| KUSM(TV) | Channel 9 |
| KBZK(TV) | Channel 7 |
| KBZK-DT | Channel 13 |

and stations as measured in 1999 described below.

The RFF contribution of each station will be calculated using the following formula:

$$S = \frac{33.4(F^2) \text{ Total ERP}}{R^2}$$

where:

S = power density in $\mu\text{W}/\text{cm}^2$

F = relative field factor

Total ERP = ERP Horizontal Polarization + ERP Vertical Polarization

R = RCAGL - 2 meters

ERP = RMS ERP in watts for DTV Stations

ERP = $[0.4 \text{ ERP}_V + \text{ERP}_A]$ for NTSC Stations

ERP_V = peak visual ERP in watts

ERP_A = RMS aural ERP in watts

The proposed KUSM-DT, Channel 8 operation, is proposed to transmit through the same antenna as the proposed KBZK-DT at 17.9 kW creating RFF level two meters above the base of the tower which is computed to be less than $0.68 : \mu\text{W/cm}^2$. This results in less than 0.3% of the limit for controlled exposure and less than 1.36% for uncontrolled exposure.

DETAILED CALCULATION

KUSM-DT DTV Facility

| | | |
|-----------|-------------------|-------------------|
| Channel 8 | Freq: | 180-186 MHz range |
| | ERP = | 17.9 kW |
| | Polarization = | Horizontal |
| | RCAGL -2 meters = | 93.8 meters |

KUSM-DT proposes to utilize a Dielectric, Type THA-P2-2H/4HD-1 antenna with 0° electrical beam tilt. The manufacturer's vertical plane pattern for this antenna is included as Exhibit E-2. Based on this plot, the field factor will be less than 0.2 at any angle greater than 25 degrees below the horizon. A value of 0.2 will be used in the calculation.

$$S = \frac{33.4 (F^2) \text{ Tot ERP}}{R^2}$$

Tot ERP = 17.9 kW (Horizontal Only)
R = 93.8 meters
F = 0.2 (field factor)

$$S = 2.72 \mu\text{W/cm}^2$$

KUSM-DT contributes less than $2.72 \mu\text{W/cm}^2$ at 2 meters above ground. The limit for an uncontrolled environment is $200 \mu\text{W/cm}^2$ for a station broadcasting on 183.3 MHz.

Therefore:

KUSM-DT DTV facility contributes less than 1.36% RFF for an uncontrolled environment two meters above ground at the tower site.

It is also proposed to mount another NTSC operation on the tower to transmit NTSC Channel

9. The maximum ERP for the proposed KUSM(TV) operation will be 44 kW, at a radiation center

of 102.2 meters above ground. Assuming a relative downward radiation factor of approximately 0.2 towards the ground in the vicinity of the tower for the total of the NTSC operations, the RFF in the vicinity of the base of the tower will be less than 0.15% of the maximum allowed for the controlled exposure and less than 0.74% maximum allowed for uncontrolled exposure to the general population.

DETAILED CALCULATION

KUSM(TV) NTSC Facility

| | | |
|-----------|-------------------|---|
| Channel 9 | Freq: | 186-192 MHz range |
| | ERP = | 22 kW [0.4 (44 kW Visual) + (4.4 kW Aural)] |
| | Polarization = | Horizontal |
| | RCAGL -2 meters = | 100.2 meters |

KUSM(TV) will utilize a Dielectric, Type THA-P2-SH/4HD-1 antenna with 0° electrical beam tilt. The manufacturer's vertical plane pattern for this antenna is included in Exhibit E-2. Based on this plot, the field factor will be less than 0.2 at any angle greater than 25 degrees below the horizon. A value of 0.2 will be used in the calculation.

$$S = \frac{33.4 (F^2) \text{ Tot ERP}}{R^2}$$

Tot ERP = 22 kW (Horizontal Only)
R = 100.2 meters
F = 0.2 (field factor)

$$S = 1.47 \mu\text{W/cm}^2$$

KUSM(TV) contributes less than $1.47 \mu\text{W/cm}^2$ at 2 meters above ground. The limit for an uncontrolled environment is $200 \mu\text{W/cm}^2$ for a station broadcasting in the 186-192 MHz.

Therefore:

KUSM(TV) NTSC facility contributes less than 0.74% RFF for an uncontrolled environment two meters above ground at the tower site.

For DTV, Channel 13, KBZK-DT and DTV Channel 8, KUSM-DT operations, will use a Dielectric, Type THA-P2-2H/4HD-1, or equivalent antenna. The antenna manufacturer's data indicates that the elevation pattern for this antenna has a maximum relative field of less than 0.1 at any angle greater than 30° below the horizontal in the vicinity of the tower. The RFF level is calculated using this relative field factor and the procedures prescribed in OET Bulletin No. 65, at an ERP of 18.9 kW for KBZK-DT and a radiation center of 95.8 meters above ground. The maximum resulting RFF two meters above the base of the tower is computed to be less than 0.72 $\mu\text{W}/\text{cm}^2$. This is less than 0.1% of the maximum allowed controlled exposure and less than 0.36% of the maximum allowed uncontrolled exposure for the general population.

DETAILED CALCULATION

KBZK-DT DTV Facility

| | | |
|------------|-------------------|-------------------|
| Channel 13 | Freq: | 210-216 MHz range |
| | ERP = | 18.9 kW |
| | Polarization = | Horizontal |
| | RCAGL -2 meters = | 93.8 meters |

KBZK-DT proposes to utilize a Dielectric, Type THA-P2-2H/4HD-1 antenna with 0° electrical beam tilt. The manufacturer's vertical plane pattern for this antenna is included in Exhibit E-2. Based on this plot, the field factor will be less than 0.1 at any angle greater than 30 degrees below the horizon. A value of 0.1 will be used in the calculation.

$$S = \frac{33.4 (F^2) \text{ Tot ERP}}{R^2}$$

Tot ERP = 18.9 kW (Horizontal Only)
R = 93.8 meters
F = 0.1 (field factor)

$$S = 0.72 \mu\text{W}/\text{cm}^2$$

KBZK-DT contributes less than 0.72 $\mu\text{W}/\text{cm}^2$ at 2 meters above ground. The limit for an uncontrolled environment is 200 $\mu\text{W}/\text{cm}^2$ for a station broadcasting on 213 MHz.

Therefore:

KBZK-DT DTV facility contributes less than 0.36% RFF for an uncontrolled environment two meters above ground at the tower site.

The KBZK(TV), channel 7 operation, will utilize the same antenna as the proposed KUSM(TV) operation. The maximum ERP for the proposed KBZK(TV) operation will be 43.7 kW, at a radiation center of 102.2 meters above ground. Assuming a relative downward radiation factor of approximately 0.2 towards the ground in the vicinity of the tower for the total of the NTSC operations, the RFF in the vicinity of the base of the tower will be less than 0.15% of the maximum allowed for the controlled exposure and less than 0.73% maximum allowed for uncontrolled exposure to the general population.

DETAILED CALCULATION

KBZK(TV) NTSC Facility

| | | |
|-----------|-------------------|---|
| Channel 7 | Freq: | 174-180 MHz range |
| | ERP = | 21.85 kW = [0.4 (43.7 kW Visual) + (4.37 kW Aural)] |
| | Polarization = | Horizontal |
| | RCAGL -2 meters = | 100.2 meters |

KBZK(TV) will utilize a Dielectric, Type THA-P2-2H/4HD-1 antenna with 0° electrical beam tilt. The manufacturer's vertical plane pattern for this antenna is included in Exhibit E-2. Based on this plot, the field factor will be less than 0.2 at any angle greater than 30 degrees below the horizon. A value of 0.2 will be used in the calculation.

$$S = \frac{33.4 (F^2) \text{ Tot ERP}}{R^2}$$

Tot ERP = 21.85 kW (Horizontal Only)
R = 100.2 meters
F = 0.2 (field factor)

$$S = 1.46 \mu\text{W/cm}^2$$

KBZK(TV) contributes less than 1.46 $\mu\text{W/cm}^2$ at 2 meters above ground. The limit for an uncontrolled environment is 200 $\mu\text{W/cm}^2$ for a station broadcasting in the 174-180 MHz range.

Therefore:

KBZK(TV) NTSC facility contributes less than 0.73% RFF for an uncontrolled environment two meters above ground at the tower site.

There are no AM towers within 3.2 kilometers of the proposed site. According to the CDBS database dated February 11, 2005, there are three FM stations broadcasting from the KBZK(TV) tower, and two television translators within 100 meters. According to the property owner, K32EP in fact, is not located near this site and is not included in the evaluation.

As reported by the station in 1999, the chief engineer of the property owner at that time evaluated the RFF levels two meters above the base of the tower and found the RFF levels to be 25% of the permissible amount. These measurements were performed with KBZK-TV¹, KMMS-FM, KISN-FM, and KYWB-LP operating at full power. This is presumed to be unchanged. In addition, the FCC CDBS database indicates KXLB-FM operates on this tower with an ERP of 94 kW and 82 meters above the ground. The KXLB-FM operation will introduce about another 7% to the RFF amount resulting in a total of 32% of the permissible amount existing around the base of the tower. Also listed in the CDBS, are three construction permits for full service FM facilities, which have not been built, and therefore are not included in the RFF evaluation.

Total RFF at Site

The total RFF contribution for all transmitters can now be calculated:

$$\text{Total additional proposed RFF} = 2.72 \text{ (KUSM-DT)} + 1.47 \text{ (KUSM(TV))} + 1.46 \text{ (KBZK(TV))} + 0.72 \text{ (KBZK-DT)} = 9.28 \mu\text{W/cm}^2$$

¹For this assessment, the measured value will be used since the antenna radiation center will increase and therefore should result in a reduction of RFF value.

Total RFF = 1.36% + 0.74% + 0.73% + 0.36% + 32% (existing) = 35.19 < 36%

In total, the RFF levels rate around the base of the tower will not exceed 36% of the maximum allowed for uncontrolled exposure with all facilities within 100 meters of the tower operating at full power.

Authorized personnel and rigging contractors will be alerted to the potential zone of high radiation on the tower, and if necessary, the station will operate with reduced power or terminate the operation of the transmitter as appropriate when it is necessary for authorized personnel or contractors to perform work on the tower. Workers and the general public therefore, will not be subjected to RFF levels in excess of the current FCC guidelines.

FCC RULE, SECTION 1.1307

The proposed operation based upon the current OET Bulletin No. 65, Edition 97-01, dated August 1997 and Supplement A meets the provisions of the FCC radio frequency field guidelines, and thus, complies with Section 1.1307 of the FCC Rules.

An environmental assessment (“EA”) is categorically excluded under Section 1.1306 of the FCC Rules and Regulations since the permittee indicates:

- (a)(1) The existing site is not located in an officially designated wilderness area.
- (a)(2) The existing site is not located in an officially designated wildlife preserve.
- (a)(3) The proposed facilities on an existing tower will not affect any listed threatened or endangered species or habitats.
- (a)(3)(ii) The proposed facilities will not jeopardize the continued existence of any proposed endangered or threatened species or likely to result in the destruction or adverse modification of proposed critical habitats.

- (a)(4) The proposed facilities will not affect any known districts, sites, buildings, structures, or objects significant in American history, architecture, archaeology, engineering or culture.
 - (a)(5) The existing site is not located near any known Indian religious sites.
 - (a)(6) The existing site is not located in a flood plain.
 - (a)(7) The installation of the new panel antenna on the modified tower will not involve a significant change in surface features of the ground in the vicinity of the tower.
 - (a)(8) It is not proposed to change the current lighting on the tower.
- (b) Workers and the general public will not be subjected to RFF levels in excess of the current FCC guidelines. Authorized personnel will be alerted to areas of the antennas where potential radiation is in excess of the FCC guidelines. A locked gate at the entrance road deters unauthorized access to the tower site.

ABOVE GROUND

106.7 METERS (350') _____
105.8 METERS (347') _____

C/R 102.2 METERS (335.3') _____

C/R 95.8 METERS (314.3') _____

91.4 METERS (300') _____

ABOVE MEAN SEA LEVEL

_____ (6960.9') 2121.7 METERS
_____ (6958') 2120.8 METERS

_____ (6946.2') 2117.2 METERS C/R

KUSM(TV)
KBZK(TV)

_____ (6925.2') 2110.8 METERS C/R

KUSM-DT CH. 8
KBZK-DT CH. 13

TOWER REGISTRATION
No. 1000681

NOT TO SCALE

0 METERS (0') _____ (6610.9') 2015 METERS

EXHIBIT E - 1
VERTICAL SKETCH
FOR THE PROPOSED OPERATION OF
KUSM-DT, BOZEMAN, MONTANA

MARCH 2005

TABLE I
COMPUTED COVERAGE DATA
FOR THE PROPOSED DTV OPERATION OF
KUSM-DT, BOZEMAN, MONTANA
CHANNEL 8 17.9 KW ERP (MAX DA) 271 METERS HAAT
MARCH 2005

| Radial Bearing N ° E, T | Average* <u>3.2-16.1 km</u> meters | Effective Height meters | Depression Angle degrees | ERP kW | Distance to Contour F(50,90) | |
|-------------------------------|--|-------------------------------|--------------------------------|-----------|------------------------------|-------------------------------|
| | | | | | 43 dBu City Grade km | 36 dBu Noise-Limited km |
| 0 | 1828.0 | 282.8 | 0.466 | 0.027 | 35.7 | 47.4 |
| 10 | 1954.8 | 155.9 | 0.346 | 0.067 | 33.8 | 45.6 |
| 20 | 2063.7 | 47.4 | 0.191 | 0.293 | 27.4 | 37.2 |
| 30 | 2100.9 | 10.5 | 0.090 | 0.447 | 19.4 | 26.8 |
| 40 | 2067.9 | 43.5 | 0.183 | 2.385 | 38.8 | 49.0 |
| 50 | 2003.5 | 107.2 | 0.287 | 6.126 | 59.6 | 71.1 |
| 60 | 1955.0 | 155.9 | 0.346 | 10.149 | 70.3 | 82.8 |
| 70 | 1901.9 | 209.7 | 0.401 | 13.767 | 77.4 | 89.7 |
| 80 | 1818.8 | 292.1 | 0.473 | 16.565 | 83.5 | 95.8 |
| 90 | 1709.5 | 404.9 | 0.557 | 17.900 | 91.9 | 104.8 |
| 100 | 1658.7 | 451.8 | 0.589 | 16.565 | 94.0 | 107.8 |
| 110 | 1733.1 | 377.6 | 0.538 | 13.767 | 88.0 | 100.6 |
| 120 | 1914.1 | 196.9 | 0.389 | 10.149 | 74.1 | 86.4 |
| 130 | 1983.3 | 127.1 | 0.312 | 6.126 | 62.4 | 74.9 |
| 140 | 2047.6 | 63.2 | 0.220 | 2.385 | 44.7 | 55.3 |
| 150 | 1847.3 | 263.7 | 0.450 | 0.447 | 54.6 | 66.4 |
| 160 | 1859.6 | 250.9 | 0.439 | 0.293 | 50.8 | 62.5 |
| 170 | 1910.3 | 200.1 | 0.392 | 0.067 | 37.5 | 48.9 |
| 180 | 2021.6 | 88.8 | 0.261 | 0.027 | 21.5 | 30.7 |
| 190 | 2025.8 | 84.7 | 0.255 | 0.067 | 25.7 | 36.1 |
| 200 | 2033.2 | 76.9 | 0.243 | 0.293 | 33.7 | 44.4 |
| 210 | 1901.4 | 208.5 | 0.400 | 0.447 | 51.4 | 63.1 |
| 220 | 1859.9 | 250.6 | 0.439 | 2.385 | 66.1 | 79.0 |
| 230 | 1749.6 | 361.2 | 0.526 | 6.126 | 80.7 | 93.1 |

TABLE I
COMPUTED COVERAGE DATA
FOR THE PROPOSED DTV OPERATION OF
KUSM-DT, BOZEMAN, MONTANA
CHANNEL 8 17.9 KW ERP (MAX DA) 271 METERS HAAT
MARCH 2005
(continued)

| Radial Bearing N ° E, T | Elevation meters | Effective Height meters | Depression Angle degrees | ERP kW | <u>Distance to Contour F(50,90)</u> | |
|-------------------------------|---------------------|-------------------------------|--------------------------------|-----------|-------------------------------------|-------------------------------|
| | | | | | 43 dBu City Grade km | 36 dBu Noise-Limited km |
| 240 | 1628.9 | 481.7 | 0.608 | 10.149 | 92.3 | 105.8 |
| 250 | 1576.7 | 533.9 | 0.640 | 13.767 | 98.4 | 111.5 |
| 260 | 1555.7 | 554.8 | 0.652 | 16.565 | 101.2 | 114.1 |
| 270 | 1516.2 | 594.4 | 0.675 | 17.900 | 103.6 | 117.2 |
| 280 | 1531.9 | 579.3 | 0.667 | 16.565 | 102.4 | 115.6 |
| 290 | 1553.3 | 557.5 | 0.654 | 13.767 | 99.9 | 112.8 |
| 300 | 1583.4 | 527.4 | 0.636 | 10.149 | 95.5 | 108.7 |
| 310 | 1736.3 | 374.4 | 0.536 | 6.126 | 81.5 | 94.1 |
| 320 | 1895.1 | 215.7 | 0.407 | 2.385 | 64.0 | 76.8 |
| 330 | 1977.1 | 133.5 | 0.320 | 0.447 | 45.0 | 56.3 |
| 340 | 1953.9 | 157.4 | 0.348 | 0.293 | 44.9 | 56.2 |
| 350 | 1783.8 | 327.0 | 0.501 | 0.067 | 44.7 | 56.3 |
| Average | 1840.0 | | | | | |

*Based on data from FCC 3-second data base

DTV Channel 8 (180-186 MHz)
 Average Elevation 3.2 to 16.1 km 1840 meters AMSL
 Center of Radiation 2110.8 meters AMSL
 Antenna Height Above Average Terrain 271 meters
 Effective Radiated Power 17.9 kW (12.53 dBk) Max.

North Latitude: 45° 40' 24"
 West Longitude: 110° 52' 02"

(NAD-27)

EXHIBIT E-2

ANTENNA MANUFACTURER DATA

KUSM-DT, BOZEMAN, MONTANA

Proposal Number **DCA-9073** Revision: **2**
 Date **15-Jan-01**
 Call Letters **KCTZ** Channel **8**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

ELEVATION PATTERN

RMS Gain at Main Lobe

4.30 (6.33 dB)

Beam Tilt

0.00 deg

RMS Gain at Horizontal

4.30 (6.33 dB)

Frequency

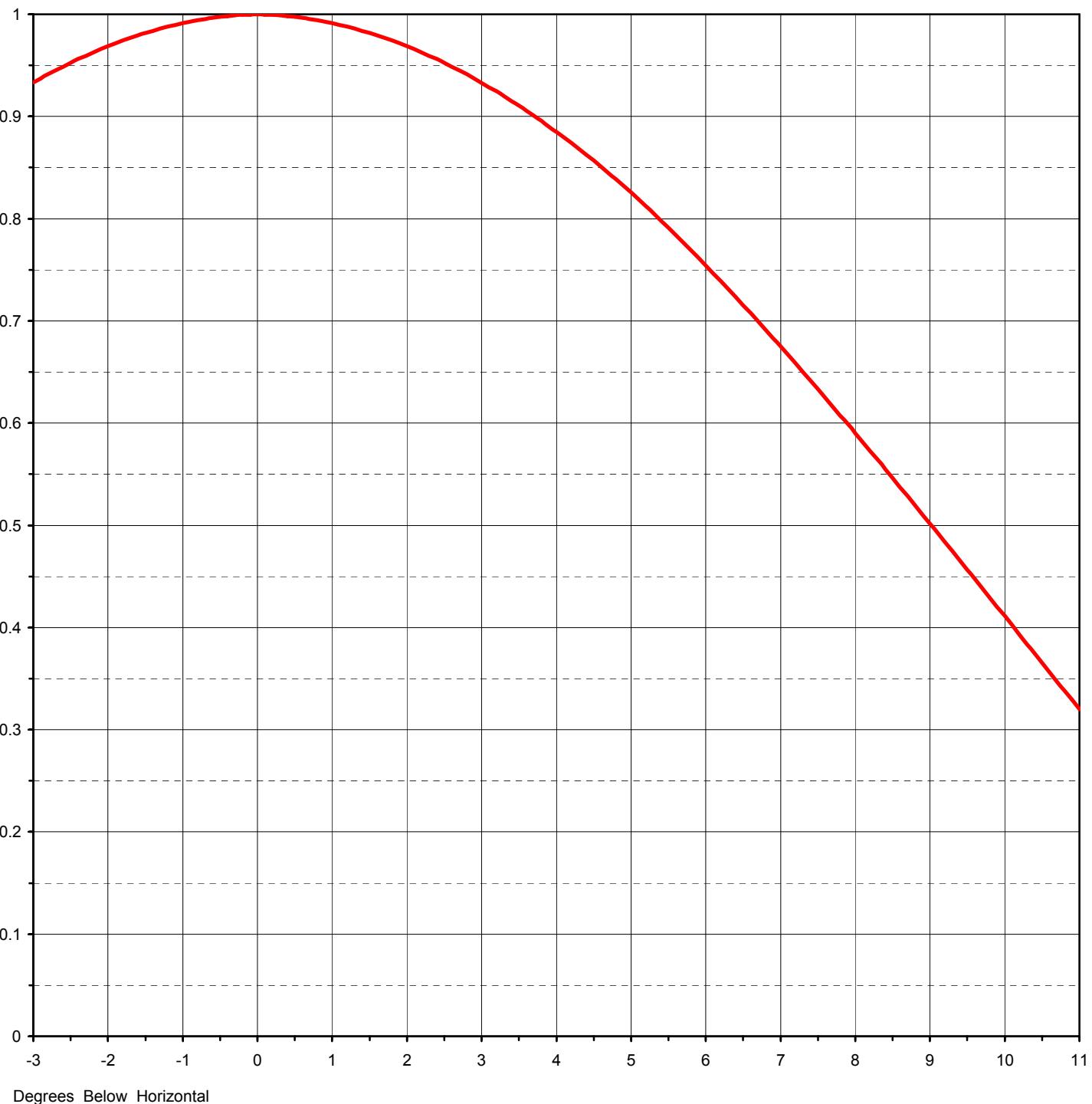
183.00 MHz

Calculated / Measured

Calculated

Drawing #

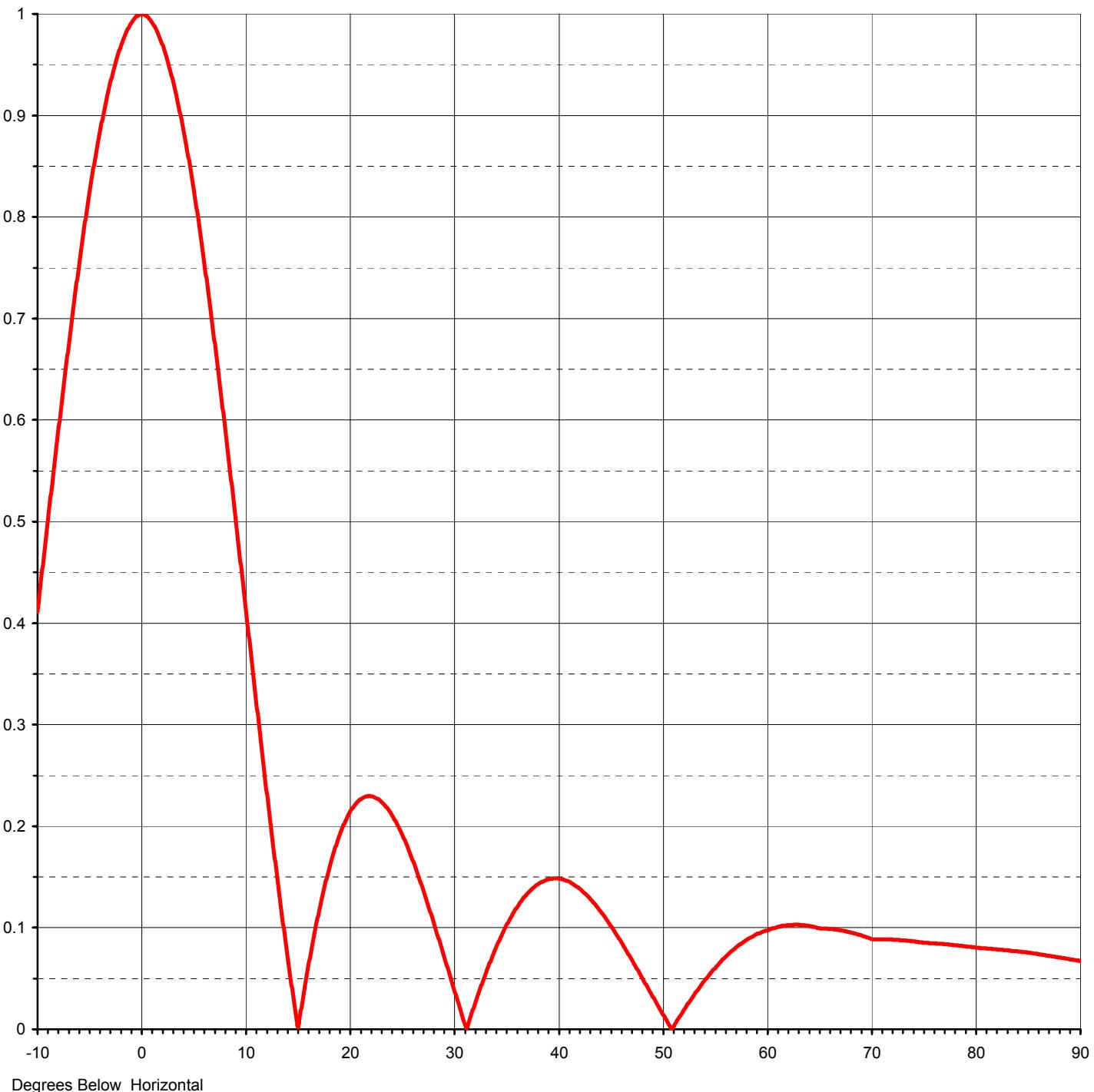
02H043000



Proposal Number **DCA-9073** Revision: **2**
 Date **15-Jan-01**
 Call Letters **KCTZ** Channel **8**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

ELEVATION PATTERN

| | | | |
|------------------------|-------------------------|-----------|---------------------|
| RMS Gain at Main Lobe | 4.30 (6.33 dB) | Beam Tilt | 0.00 deg |
| RMS Gain at Horizontal | 4.30 (6.33 dB) | Frequency | 183.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 02H043000-90 |



Degrees Below Horizontal



Proposal Number **DCA-9073** Revision: **2**
Date **15-Jan-01**
Call Letters **KCTZ** Channel **8**
Location **Bozeman, MT**
Customer **Cordillera**
Antenna Type **THA-P2-2H/4HD-1**

TABULATION OF ELEVATION PATTERN

Elevation Pattern Drawing #: **02H043000-90**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -10.0 | 0.411 | 2.4 | 0.956 | 10.6 | 0.366 | 30.5 | 0.024 | 51.0 | 0.001 | 71.5 | 0.089 |
| -9.5 | 0.457 | 2.6 | 0.949 | 10.8 | 0.347 | 31.0 | 0.008 | 51.5 | 0.010 | 72.0 | 0.088 |
| -9.0 | 0.502 | 2.8 | 0.941 | 11.0 | 0.329 | 31.5 | 0.008 | 52.0 | 0.018 | 72.5 | 0.088 |
| -8.5 | 0.546 | 3.0 | 0.933 | 11.5 | 0.284 | 32.0 | 0.024 | 52.5 | 0.026 | 73.0 | 0.088 |
| -8.0 | 0.590 | 3.2 | 0.924 | 12.0 | 0.240 | 32.5 | 0.039 | 53.0 | 0.033 | 73.5 | 0.087 |
| -7.5 | 0.633 | 3.4 | 0.915 | 12.5 | 0.197 | 33.0 | 0.053 | 53.5 | 0.040 | 74.0 | 0.086 |
| -7.0 | 0.675 | 3.6 | 0.906 | 13.0 | 0.156 | 33.5 | 0.066 | 54.0 | 0.047 | 74.5 | 0.086 |
| -6.5 | 0.715 | 3.8 | 0.896 | 13.5 | 0.115 | 34.0 | 0.079 | 54.5 | 0.054 | 75.0 | 0.085 |
| -6.0 | 0.754 | 4.0 | 0.885 | 14.0 | 0.077 | 34.5 | 0.090 | 55.0 | 0.060 | 75.5 | 0.085 |
| -5.5 | 0.791 | 4.2 | 0.874 | 14.5 | 0.040 | 35.0 | 0.101 | 55.5 | 0.065 | 76.0 | 0.085 |
| -5.0 | 0.826 | 4.4 | 0.863 | 15.0 | 0.005 | 35.5 | 0.111 | 56.0 | 0.071 | 76.5 | 0.084 |
| -4.5 | 0.857 | 4.6 | 0.851 | 15.5 | 0.028 | 36.0 | 0.119 | 56.5 | 0.075 | 77.0 | 0.084 |
| -4.0 | 0.885 | 4.8 | 0.839 | 16.0 | 0.058 | 36.5 | 0.126 | 57.0 | 0.080 | 77.5 | 0.083 |
| -3.5 | 0.910 | 5.0 | 0.826 | 16.5 | 0.086 | 37.0 | 0.133 | 57.5 | 0.084 | 78.0 | 0.083 |
| -3.0 | 0.933 | 5.2 | 0.812 | 17.0 | 0.112 | 37.5 | 0.138 | 58.0 | 0.087 | 78.5 | 0.082 |
| -2.8 | 0.941 | 5.4 | 0.798 | 17.5 | 0.135 | 38.0 | 0.142 | 58.5 | 0.091 | 79.0 | 0.082 |
| -2.6 | 0.949 | 5.6 | 0.784 | 18.0 | 0.156 | 38.5 | 0.145 | 59.0 | 0.093 | 79.5 | 0.081 |
| -2.4 | 0.956 | 5.8 | 0.769 | 18.5 | 0.174 | 39.0 | 0.147 | 59.5 | 0.095 | 80.0 | 0.080 |
| -2.2 | 0.963 | 6.0 | 0.754 | 19.0 | 0.190 | 39.5 | 0.148 | 60.0 | 0.097 | 80.5 | 0.080 |
| -2.0 | 0.969 | 6.2 | 0.739 | 19.5 | 0.202 | 40.0 | 0.148 | 60.5 | 0.099 | 81.0 | 0.080 |
| -1.8 | 0.974 | 6.4 | 0.723 | 20.0 | 0.213 | 40.5 | 0.147 | 61.0 | 0.101 | 81.5 | 0.079 |
| -1.6 | 0.979 | 6.6 | 0.707 | 20.5 | 0.221 | 41.0 | 0.146 | 61.5 | 0.102 | 82.0 | 0.079 |
| -1.4 | 0.984 | 6.8 | 0.691 | 21.0 | 0.226 | 41.5 | 0.143 | 62.0 | 0.102 | 82.5 | 0.078 |
| -1.2 | 0.988 | 7.0 | 0.675 | 21.5 | 0.229 | 42.0 | 0.139 | 62.5 | 0.103 | 83.0 | 0.078 |
| -1.0 | 0.991 | 7.2 | 0.659 | 22.0 | 0.230 | 42.5 | 0.135 | 63.0 | 0.103 | 83.5 | 0.077 |
| -0.8 | 0.994 | 7.4 | 0.642 | 22.5 | 0.228 | 43.0 | 0.130 | 63.5 | 0.103 | 84.0 | 0.077 |
| -0.6 | 0.997 | 7.6 | 0.625 | 23.0 | 0.225 | 43.5 | 0.124 | 64.0 | 0.102 | 84.5 | 0.076 |
| -0.4 | 0.998 | 7.8 | 0.608 | 23.5 | 0.219 | 44.0 | 0.117 | 64.5 | 0.101 | 85.0 | 0.075 |
| -0.2 | 0.999 | 8.0 | 0.590 | 24.0 | 0.212 | 44.5 | 0.110 | 65.0 | 0.099 | 85.5 | 0.075 |
| 0.0 | 1.000 | 8.2 | 0.573 | 24.5 | 0.204 | 45.0 | 0.103 | 65.5 | 0.099 | 86.0 | 0.074 |
| 0.2 | 0.999 | 8.4 | 0.555 | 25.0 | 0.193 | 45.5 | 0.095 | 66.0 | 0.099 | 86.5 | 0.073 |
| 0.4 | 0.998 | 8.6 | 0.537 | 25.5 | 0.181 | 46.0 | 0.087 | 66.5 | 0.098 | 87.0 | 0.072 |
| 0.6 | 0.997 | 8.8 | 0.520 | 26.0 | 0.168 | 46.5 | 0.079 | 67.0 | 0.097 | 87.5 | 0.072 |
| 0.8 | 0.994 | 9.0 | 0.502 | 26.5 | 0.154 | 47.0 | 0.070 | 67.5 | 0.097 | 88.0 | 0.071 |
| 1.0 | 0.991 | 9.2 | 0.484 | 27.0 | 0.140 | 47.5 | 0.061 | 68.0 | 0.095 | 88.5 | 0.070 |
| 1.2 | 0.988 | 9.4 | 0.466 | 27.5 | 0.124 | 48.0 | 0.052 | 68.5 | 0.094 | 89.0 | 0.069 |
| 1.4 | 0.984 | 9.6 | 0.447 | 28.0 | 0.108 | 48.5 | 0.043 | 69.0 | 0.092 | 89.5 | 0.068 |
| 1.6 | 0.979 | 9.8 | 0.438 | 28.5 | 0.091 | 49.0 | 0.034 | 69.5 | 0.091 | 90.0 | 0.067 |
| 1.8 | 0.974 | 10.0 | 0.420 | 29.0 | 0.074 | 49.5 | 0.025 | 70.0 | 0.089 | | |
| 2.0 | 0.969 | 10.2 | 0.402 | 29.5 | 0.058 | 50.0 | 0.016 | 70.5 | 0.089 | | |
| 2.2 | 0.963 | 10.4 | 0.384 | 30.0 | 0.041 | 50.5 | 0.007 | 71.0 | 0.089 | | |

Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

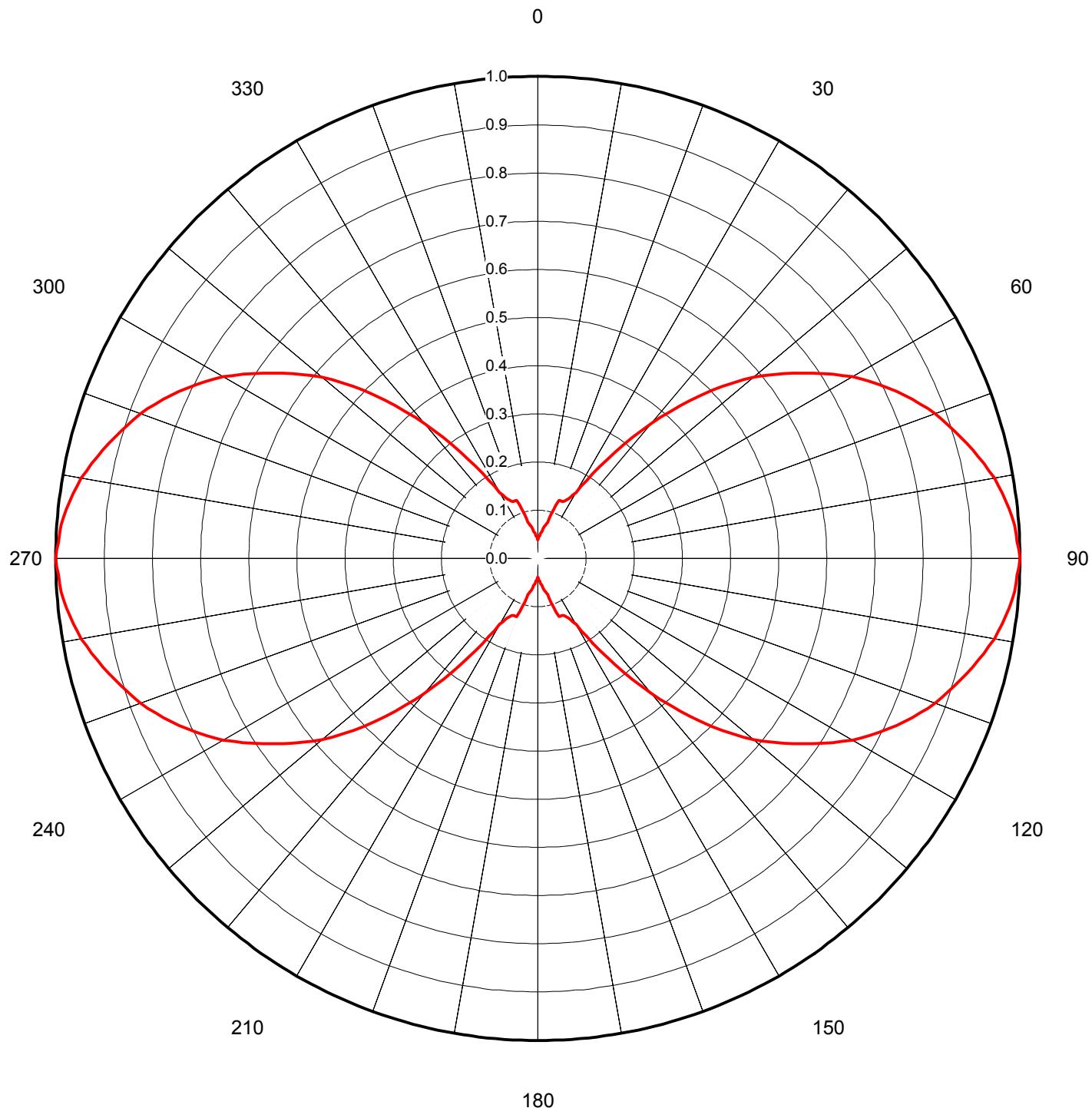
DCA-9073
15-Jan-01
KCTZ
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

Revision: **2**
Channel **8**

AZIMUTH PATTERN

Gain **2.75**
Calculated / Measured
(**4.40 dB**)
Calculated

Frequency
Drawing #
183.00 MHz
THA-P4-8





Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

DCA-9073
15-Jan-01
KCTZ
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

Revision: **2**
Channel **8**

TABULATION OF AZIMUTH PATTERN

Azimuth Pattern Drawing #: **THA-P4-8**

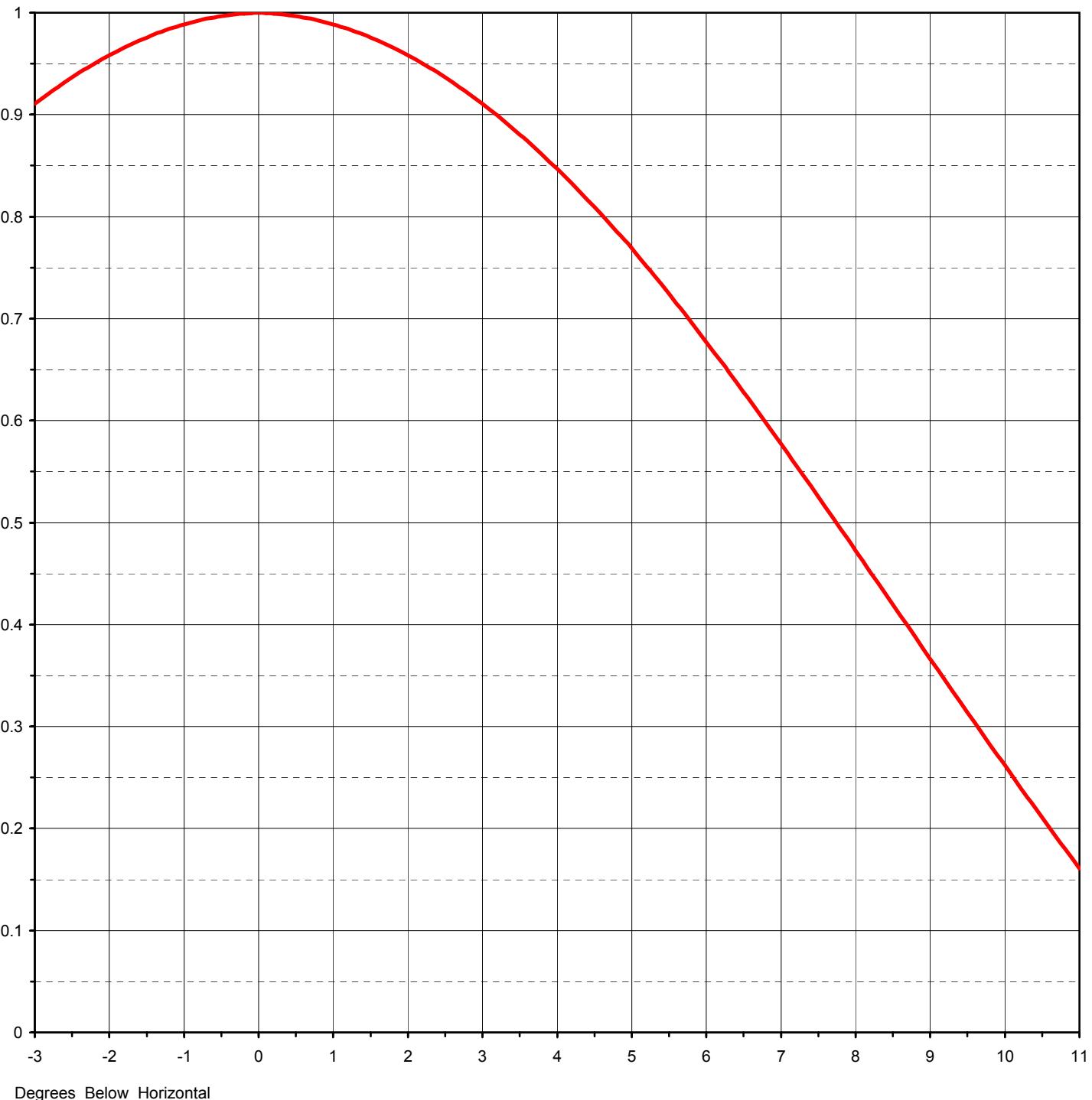
| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0.039 | 45 | 0.478 | 90 | 1.000 | 135 | 0.478 | 180 | 0.039 | 225 | 0.478 | 270 | 1.000 | 315 | 0.478 | | | | |
| 1 | 0.041 | 46 | 0.501 | 91 | 0.998 | 136 | 0.456 | 181 | 0.041 | 226 | 0.501 | 271 | 0.998 | 316 | 0.456 | | | | |
| 2 | 0.043 | 47 | 0.523 | 92 | 0.995 | 137 | 0.433 | 182 | 0.043 | 227 | 0.523 | 272 | 0.995 | 317 | 0.433 | | | | |
| 3 | 0.045 | 48 | 0.544 | 93 | 0.993 | 138 | 0.410 | 183 | 0.045 | 228 | 0.544 | 273 | 0.993 | 318 | 0.410 | | | | |
| 4 | 0.046 | 49 | 0.565 | 94 | 0.991 | 139 | 0.388 | 184 | 0.046 | 229 | 0.565 | 274 | 0.991 | 319 | 0.388 | | | | |
| 5 | 0.047 | 50 | 0.585 | 95 | 0.988 | 140 | 0.365 | 185 | 0.047 | 230 | 0.585 | 275 | 0.988 | 320 | 0.365 | | | | |
| 6 | 0.051 | 51 | 0.603 | 96 | 0.983 | 141 | 0.342 | 186 | 0.051 | 231 | 0.603 | 276 | 0.983 | 321 | 0.342 | | | | |
| 7 | 0.053 | 52 | 0.620 | 97 | 0.978 | 142 | 0.318 | 187 | 0.053 | 232 | 0.620 | 277 | 0.978 | 322 | 0.318 | | | | |
| 8 | 0.056 | 53 | 0.637 | 98 | 0.972 | 143 | 0.295 | 188 | 0.056 | 233 | 0.637 | 278 | 0.972 | 323 | 0.295 | | | | |
| 9 | 0.059 | 54 | 0.653 | 99 | 0.967 | 144 | 0.272 | 189 | 0.059 | 234 | 0.653 | 279 | 0.967 | 324 | 0.272 | | | | |
| 10 | 0.061 | 55 | 0.670 | 100 | 0.962 | 145 | 0.249 | 190 | 0.061 | 235 | 0.670 | 280 | 0.962 | 325 | 0.249 | | | | |
| 11 | 0.065 | 56 | 0.687 | 101 | 0.954 | 146 | 0.229 | 191 | 0.065 | 236 | 0.687 | 281 | 0.954 | 326 | 0.229 | | | | |
| 12 | 0.068 | 57 | 0.705 | 102 | 0.946 | 147 | 0.210 | 192 | 0.068 | 237 | 0.705 | 282 | 0.946 | 327 | 0.210 | | | | |
| 13 | 0.072 | 58 | 0.721 | 103 | 0.938 | 148 | 0.192 | 193 | 0.072 | 238 | 0.721 | 283 | 0.938 | 328 | 0.192 | | | | |
| 14 | 0.075 | 59 | 0.738 | 104 | 0.929 | 149 | 0.174 | 194 | 0.075 | 239 | 0.738 | 284 | 0.929 | 329 | 0.174 | | | | |
| 15 | 0.077 | 60 | 0.753 | 105 | 0.922 | 150 | 0.158 | 195 | 0.077 | 240 | 0.753 | 285 | 0.922 | 330 | 0.158 | | | | |
| 16 | 0.086 | 61 | 0.767 | 106 | 0.913 | 151 | 0.150 | 196 | 0.086 | 241 | 0.767 | 286 | 0.913 | 331 | 0.150 | | | | |
| 17 | 0.096 | 62 | 0.781 | 107 | 0.904 | 152 | 0.144 | 197 | 0.096 | 242 | 0.781 | 287 | 0.904 | 332 | 0.144 | | | | |
| 18 | 0.106 | 63 | 0.794 | 108 | 0.895 | 153 | 0.138 | 198 | 0.106 | 243 | 0.794 | 288 | 0.895 | 333 | 0.138 | | | | |
| 19 | 0.117 | 64 | 0.808 | 109 | 0.886 | 154 | 0.134 | 199 | 0.117 | 244 | 0.808 | 289 | 0.886 | 334 | 0.134 | | | | |
| 20 | 0.128 | 65 | 0.821 | 110 | 0.877 | 155 | 0.131 | 200 | 0.128 | 245 | 0.821 | 290 | 0.877 | 335 | 0.131 | | | | |
| 21 | 0.128 | 66 | 0.832 | 111 | 0.866 | 156 | 0.130 | 201 | 0.128 | 246 | 0.832 | 291 | 0.866 | 336 | 0.130 | | | | |
| 22 | 0.128 | 67 | 0.844 | 112 | 0.855 | 157 | 0.129 | 202 | 0.128 | 247 | 0.844 | 292 | 0.855 | 337 | 0.129 | | | | |
| 23 | 0.129 | 68 | 0.855 | 113 | 0.844 | 158 | 0.128 | 203 | 0.129 | 248 | 0.855 | 293 | 0.844 | 338 | 0.128 | | | | |
| 24 | 0.130 | 69 | 0.866 | 114 | 0.832 | 159 | 0.128 | 204 | 0.130 | 249 | 0.866 | 294 | 0.832 | 339 | 0.128 | | | | |
| 25 | 0.131 | 70 | 0.877 | 115 | 0.821 | 160 | 0.128 | 205 | 0.131 | 250 | 0.877 | 295 | 0.821 | 340 | 0.128 | | | | |
| 26 | 0.134 | 71 | 0.886 | 116 | 0.808 | 161 | 0.117 | 206 | 0.134 | 251 | 0.886 | 296 | 0.808 | 341 | 0.117 | | | | |
| 27 | 0.138 | 72 | 0.895 | 117 | 0.794 | 162 | 0.106 | 207 | 0.138 | 252 | 0.895 | 297 | 0.794 | 342 | 0.106 | | | | |
| 28 | 0.144 | 73 | 0.904 | 118 | 0.781 | 163 | 0.096 | 208 | 0.144 | 253 | 0.904 | 298 | 0.781 | 343 | 0.096 | | | | |
| 29 | 0.150 | 74 | 0.913 | 119 | 0.767 | 164 | 0.086 | 209 | 0.150 | 254 | 0.913 | 299 | 0.767 | 344 | 0.086 | | | | |
| 30 | 0.158 | 75 | 0.922 | 120 | 0.753 | 165 | 0.077 | 210 | 0.158 | 255 | 0.922 | 300 | 0.753 | 345 | 0.077 | | | | |
| 31 | 0.174 | 76 | 0.929 | 121 | 0.738 | 166 | 0.075 | 211 | 0.174 | 256 | 0.929 | 301 | 0.738 | 346 | 0.075 | | | | |
| 32 | 0.192 | 77 | 0.938 | 122 | 0.721 | 167 | 0.072 | 212 | 0.192 | 257 | 0.938 | 302 | 0.721 | 347 | 0.072 | | | | |
| 33 | 0.210 | 78 | 0.946 | 123 | 0.705 | 168 | 0.068 | 213 | 0.210 | 258 | 0.946 | 303 | 0.705 | 348 | 0.068 | | | | |
| 34 | 0.229 | 79 | 0.954 | 124 | 0.687 | 169 | 0.065 | 214 | 0.229 | 259 | 0.954 | 304 | 0.687 | 349 | 0.065 | | | | |
| 35 | 0.249 | 80 | 0.962 | 125 | 0.670 | 170 | 0.061 | 215 | 0.249 | 260 | 0.962 | 305 | 0.670 | 350 | 0.061 | | | | |
| 36 | 0.272 | 81 | 0.967 | 126 | 0.653 | 171 | 0.059 | 216 | 0.272 | 261 | 0.967 | 306 | 0.653 | 351 | 0.059 | | | | |
| 37 | 0.295 | 82 | 0.972 | 127 | 0.637 | 172 | 0.056 | 217 | 0.295 | 262 | 0.972 | 307 | 0.637 | 352 | 0.056 | | | | |
| 38 | 0.318 | 83 | 0.978 | 128 | 0.620 | 173 | 0.053 | 218 | 0.318 | 263 | 0.978 | 308 | 0.620 | 353 | 0.053 | | | | |
| 39 | 0.342 | 84 | 0.983 | 129 | 0.603 | 174 | 0.051 | 219 | 0.342 | 264 | 0.983 | 309 | 0.603 | 354 | 0.051 | | | | |
| 40 | 0.365 | 85 | 0.988 | 130 | 0.585 | 175 | 0.047 | 220 | 0.365 | 265 | 0.988 | 310 | 0.585 | 355 | 0.047 | | | | |
| 41 | 0.388 | 86 | 0.991 | 131 | 0.565 | 176 | 0.046 | 221 | 0.388 | 266 | 0.991 | 311 | 0.565 | 356 | 0.046 | | | | |
| 42 | 0.410 | 87 | 0.993 | 132 | 0.544 | 177 | 0.045 | 222 | 0.410 | 267 | 0.993 | 312 | 0.544 | 357 | 0.045 | | | | |
| 43 | 0.433 | 88 | 0.995 | 133 | 0.523 | 178 | 0.043 | 223 | 0.433 | 268 | 0.995 | 313 | 0.523 | 358 | 0.043 | | | | |
| 44 | 0.456 | 89 | 0.998 | 134 | 0.501 | 179 | 0.041 | 224 | 0.456 | 269 | 0.998 | 314 | 0.501 | 359 | 0.041 | | | | |

Proposal Number **DCA-9073**
 Date **15-Jan-01**
 Call Letters **KCTZ-DT**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

Revision: **2**
 Channel **13**

ELEVATION PATTERN

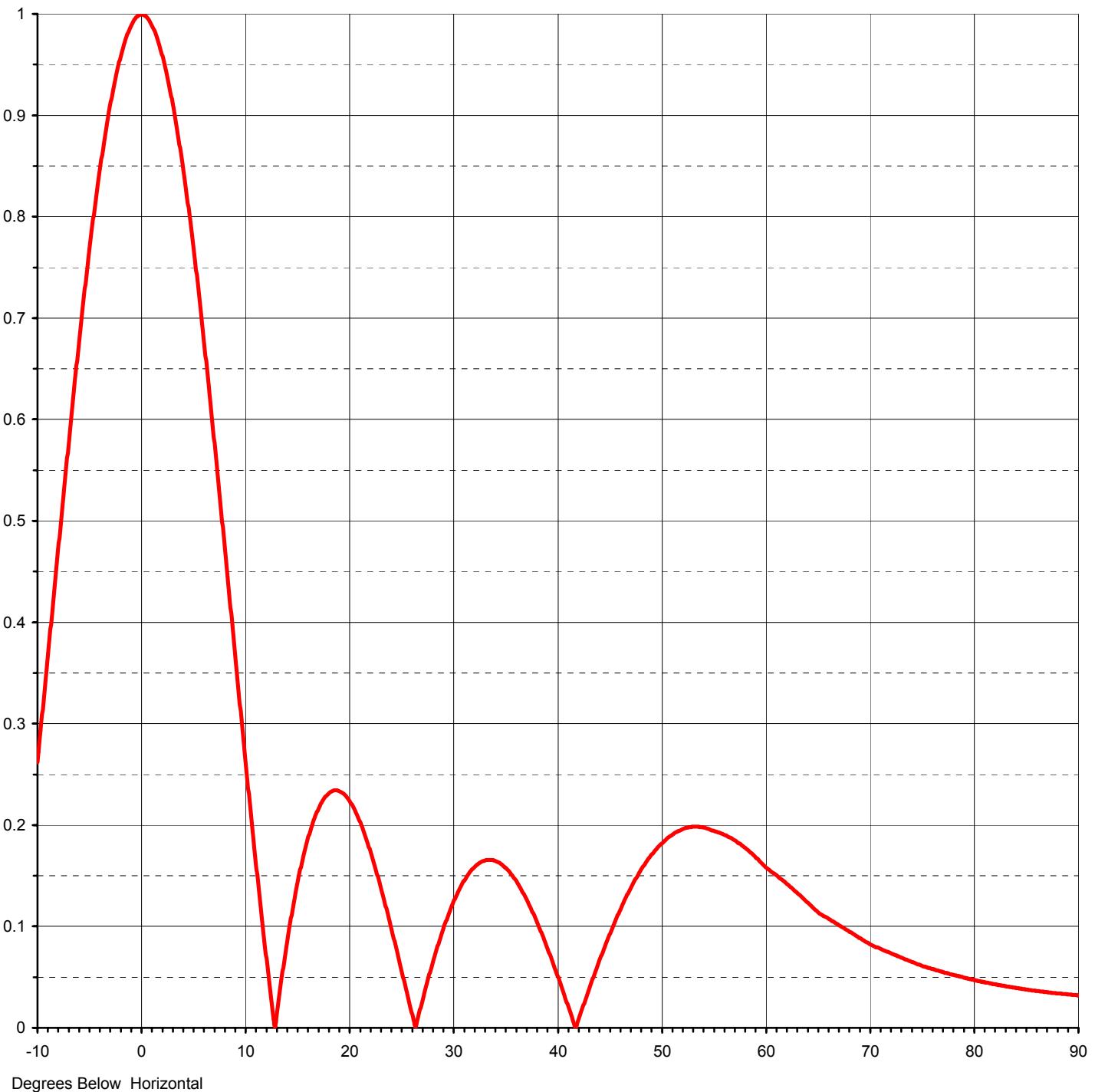
| | | | |
|------------------------|-------------------------|-----------|-------------------|
| RMS Gain at Main Lobe | 4.80 (6.81 dB) | Beam Tilt | 0.00 deg |
| RMS Gain at Horizontal | 4.80 (6.81 dB) | Frequency | 213.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 02H048000 |



| | | | |
|-----------------|------------------------|-----------|-----------|
| Proposal Number | DCA-9073 | Revision: | 2 |
| Date | 15-Jan-01 | | |
| Call Letters | KCTZ-DT | Channel | 13 |
| Location | Bozeman, MT | | |
| Customer | Cordillera | | |
| Antenna Type | THA-P2-2H/4HD-1 | | |

ELEVATION PATTERN

| | | | |
|------------------------|-------------------------|-----------|---------------------|
| RMS Gain at Main Lobe | 4.80 (6.81 dB) | Beam Tilt | 0.00 deg |
| RMS Gain at Horizontal | 4.80 (6.81 dB) | Frequency | 213.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 02H048000-90 |



Degrees Below Horizontal



Proposal Number **DCA-9073** Revision: **2**
Date **15-Jan-01**
Call Letters **KCTZ-DT** Channel **13**
Location **Bozeman, MT**
Customer **Cordillera**
Antenna Type **THA-P2-2H/4HD-1**

TABULATION OF ELEVATION PATTERN

Elevation Pattern Drawing #: **02H048000-90**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -10.0 | 0.262 | 2.4 | 0.941 | 10.6 | 0.211 | 30.5 | 0.134 | 51.0 | 0.190 | 71.5 | 0.076 |
| -9.5 | 0.314 | 2.6 | 0.932 | 10.8 | 0.191 | 31.0 | 0.144 | 51.5 | 0.193 | 72.0 | 0.073 |
| -9.0 | 0.366 | 2.8 | 0.921 | 11.0 | 0.171 | 31.5 | 0.152 | 52.0 | 0.196 | 72.5 | 0.071 |
| -8.5 | 0.420 | 3.0 | 0.910 | 11.5 | 0.123 | 32.0 | 0.158 | 52.5 | 0.197 | 73.0 | 0.069 |
| -8.0 | 0.473 | 3.2 | 0.899 | 12.0 | 0.077 | 32.5 | 0.162 | 53.0 | 0.198 | 73.5 | 0.067 |
| -7.5 | 0.525 | 3.4 | 0.887 | 12.5 | 0.034 | 33.0 | 0.165 | 53.5 | 0.198 | 74.0 | 0.065 |
| -7.0 | 0.577 | 3.6 | 0.874 | 13.0 | 0.007 | 33.5 | 0.166 | 54.0 | 0.198 | 74.5 | 0.063 |
| -6.5 | 0.628 | 3.8 | 0.861 | 13.5 | 0.045 | 34.0 | 0.165 | 54.5 | 0.196 | 75.0 | 0.061 |
| -6.0 | 0.677 | 4.0 | 0.847 | 14.0 | 0.079 | 34.5 | 0.162 | 55.0 | 0.194 | 75.5 | 0.060 |
| -5.5 | 0.724 | 4.2 | 0.832 | 14.5 | 0.111 | 35.0 | 0.159 | 55.5 | 0.193 | 76.0 | 0.058 |
| -5.0 | 0.769 | 4.4 | 0.817 | 15.0 | 0.139 | 35.5 | 0.153 | 56.0 | 0.191 | 76.5 | 0.056 |
| -4.5 | 0.809 | 4.6 | 0.802 | 15.5 | 0.163 | 36.0 | 0.146 | 56.5 | 0.188 | 77.0 | 0.055 |
| -4.0 | 0.847 | 4.8 | 0.786 | 16.0 | 0.184 | 36.5 | 0.138 | 57.0 | 0.185 | 77.5 | 0.054 |
| -3.5 | 0.881 | 5.0 | 0.769 | 16.5 | 0.201 | 37.0 | 0.128 | 57.5 | 0.182 | 78.0 | 0.052 |
| -3.0 | 0.911 | 5.2 | 0.751 | 17.0 | 0.214 | 37.5 | 0.118 | 58.0 | 0.178 | 78.5 | 0.051 |
| -2.8 | 0.921 | 5.4 | 0.733 | 17.5 | 0.224 | 38.0 | 0.106 | 58.5 | 0.174 | 79.0 | 0.049 |
| -2.6 | 0.932 | 5.6 | 0.715 | 18.0 | 0.231 | 38.5 | 0.094 | 59.0 | 0.169 | 79.5 | 0.048 |
| -2.4 | 0.941 | 5.8 | 0.696 | 18.5 | 0.234 | 39.0 | 0.081 | 59.5 | 0.164 | 80.0 | 0.047 |
| -2.2 | 0.950 | 6.0 | 0.677 | 19.0 | 0.234 | 39.5 | 0.067 | 60.0 | 0.159 | 80.5 | 0.046 |
| -2.0 | 0.958 | 6.2 | 0.658 | 19.5 | 0.231 | 40.0 | 0.053 | 60.5 | 0.155 | 81.0 | 0.045 |
| -1.8 | 0.966 | 6.4 | 0.638 | 20.0 | 0.225 | 40.5 | 0.039 | 61.0 | 0.151 | 81.5 | 0.044 |
| -1.6 | 0.973 | 6.6 | 0.618 | 20.5 | 0.216 | 41.0 | 0.024 | 61.5 | 0.147 | 82.0 | 0.043 |
| -1.4 | 0.979 | 6.8 | 0.598 | 21.0 | 0.205 | 41.5 | 0.009 | 62.0 | 0.143 | 82.5 | 0.042 |
| -1.2 | 0.984 | 7.0 | 0.577 | 21.5 | 0.192 | 42.0 | 0.006 | 62.5 | 0.138 | 83.0 | 0.041 |
| -1.0 | 0.988 | 7.2 | 0.557 | 22.0 | 0.177 | 42.5 | 0.021 | 63.0 | 0.134 | 83.5 | 0.040 |
| -0.8 | 0.992 | 7.4 | 0.536 | 22.5 | 0.160 | 43.0 | 0.036 | 63.5 | 0.129 | 84.0 | 0.039 |
| -0.6 | 0.995 | 7.6 | 0.515 | 23.0 | 0.141 | 43.5 | 0.050 | 64.0 | 0.124 | 84.5 | 0.038 |
| -0.4 | 0.998 | 7.8 | 0.494 | 23.5 | 0.122 | 44.0 | 0.064 | 64.5 | 0.119 | 85.0 | 0.038 |
| -0.2 | 0.999 | 8.0 | 0.473 | 24.0 | 0.102 | 44.5 | 0.077 | 65.0 | 0.114 | 85.5 | 0.037 |
| 0.0 | 1.000 | 8.2 | 0.451 | 24.5 | 0.081 | 45.0 | 0.090 | 65.5 | 0.111 | 86.0 | 0.036 |
| 0.2 | 0.999 | 8.4 | 0.430 | 25.0 | 0.060 | 45.5 | 0.103 | 66.0 | 0.108 | 86.5 | 0.036 |
| 0.4 | 0.998 | 8.6 | 0.409 | 25.5 | 0.038 | 46.0 | 0.115 | 66.5 | 0.105 | 87.0 | 0.035 |
| 0.6 | 0.995 | 8.8 | 0.388 | 26.0 | 0.017 | 46.5 | 0.126 | 67.0 | 0.101 | 87.5 | 0.034 |
| 0.8 | 0.992 | 9.0 | 0.366 | 26.5 | 0.004 | 47.0 | 0.136 | 67.5 | 0.098 | 88.0 | 0.034 |
| 1.0 | 0.988 | 9.2 | 0.345 | 27.0 | 0.024 | 47.5 | 0.146 | 68.0 | 0.095 | 88.5 | 0.034 |
| 1.2 | 0.984 | 9.4 | 0.324 | 27.5 | 0.043 | 48.0 | 0.154 | 68.5 | 0.092 | 89.0 | 0.033 |
| 1.4 | 0.979 | 9.6 | 0.303 | 28.0 | 0.062 | 48.5 | 0.162 | 69.0 | 0.089 | 89.5 | 0.032 |
| 1.6 | 0.973 | 9.8 | 0.293 | 28.5 | 0.079 | 49.0 | 0.169 | 69.5 | 0.085 | 90.0 | 0.032 |
| 1.8 | 0.966 | 10.0 | 0.272 | 29.0 | 0.095 | 49.5 | 0.176 | 70.0 | 0.082 | | |
| 2.0 | 0.958 | 10.2 | 0.252 | 29.5 | 0.109 | 50.0 | 0.181 | 70.5 | 0.080 | | |
| 2.2 | 0.950 | 10.4 | 0.231 | 30.0 | 0.123 | 50.5 | 0.186 | 71.0 | 0.078 | | |

Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

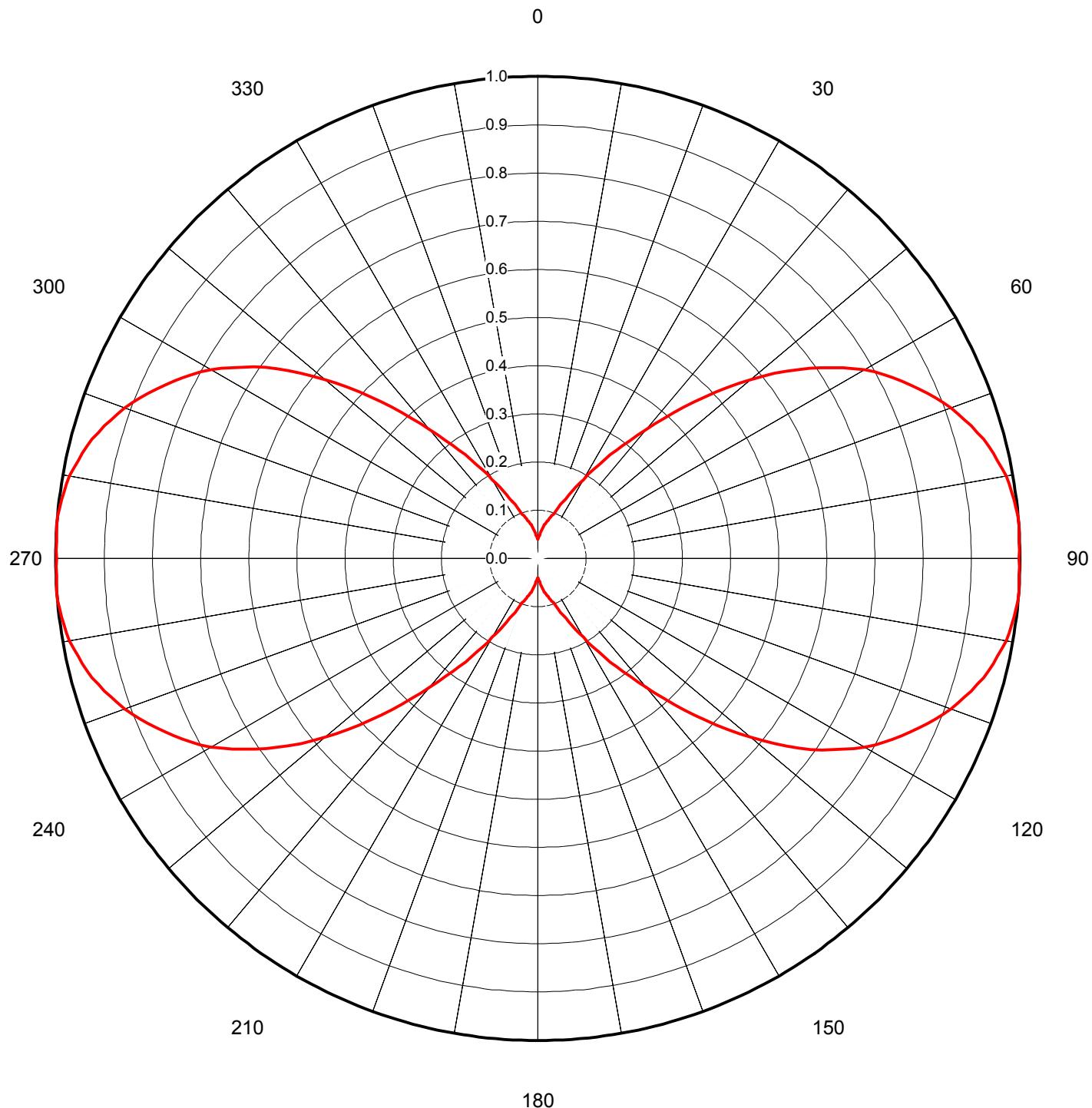
DCA-9073
15-Jan-01
KCTZ
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

Revision: **2**
Channel **13**

AZIMUTH PATTERN

Gain **2.63**
Calculated / Measured
(4.20 dB)
Calculated

Frequency
Drawing #
213.00 MHz
THA-P4-13





Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

DCA-9073
15-Jan-01
KCTZ
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

Revision: **2**
Channel **13**

TABULATION OF AZIMUTH PATTERN

Azimuth Pattern Drawing #: **THA-P4-13**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0.040 | 45 | 0.459 | 90 | 0.998 | 135 | 0.459 | 180 | 0.040 | 225 | 0.459 | 270 | 0.998 | 315 | 0.459 | | | | |
| 1 | 0.041 | 46 | 0.483 | 91 | 0.999 | 136 | 0.436 | 181 | 0.041 | 226 | 0.483 | 271 | 0.999 | 316 | 0.436 | | | | |
| 2 | 0.043 | 47 | 0.506 | 92 | 0.999 | 137 | 0.414 | 182 | 0.043 | 227 | 0.506 | 272 | 0.999 | 317 | 0.414 | | | | |
| 3 | 0.045 | 48 | 0.530 | 93 | 0.999 | 138 | 0.391 | 183 | 0.045 | 228 | 0.530 | 273 | 0.999 | 318 | 0.391 | | | | |
| 4 | 0.047 | 49 | 0.554 | 94 | 1.000 | 139 | 0.370 | 184 | 0.047 | 229 | 0.554 | 274 | 1.000 | 319 | 0.370 | | | | |
| 5 | 0.048 | 50 | 0.578 | 95 | 1.000 | 140 | 0.348 | 185 | 0.048 | 230 | 0.578 | 275 | 1.000 | 320 | 0.348 | | | | |
| 6 | 0.053 | 51 | 0.601 | 96 | 0.997 | 141 | 0.329 | 186 | 0.053 | 231 | 0.601 | 276 | 0.997 | 321 | 0.329 | | | | |
| 7 | 0.057 | 52 | 0.623 | 97 | 0.995 | 142 | 0.311 | 187 | 0.057 | 232 | 0.623 | 277 | 0.995 | 322 | 0.311 | | | | |
| 8 | 0.061 | 53 | 0.645 | 98 | 0.992 | 143 | 0.294 | 188 | 0.061 | 233 | 0.645 | 278 | 0.992 | 323 | 0.294 | | | | |
| 9 | 0.064 | 54 | 0.667 | 99 | 0.989 | 144 | 0.278 | 189 | 0.064 | 234 | 0.667 | 279 | 0.989 | 324 | 0.278 | | | | |
| 10 | 0.068 | 55 | 0.688 | 100 | 0.987 | 145 | 0.262 | 190 | 0.068 | 235 | 0.688 | 280 | 0.987 | 325 | 0.262 | | | | |
| 11 | 0.071 | 56 | 0.708 | 101 | 0.981 | 146 | 0.246 | 191 | 0.071 | 236 | 0.708 | 281 | 0.981 | 326 | 0.246 | | | | |
| 12 | 0.074 | 57 | 0.727 | 102 | 0.975 | 147 | 0.231 | 192 | 0.074 | 237 | 0.727 | 282 | 0.975 | 327 | 0.231 | | | | |
| 13 | 0.077 | 58 | 0.746 | 103 | 0.969 | 148 | 0.216 | 193 | 0.077 | 238 | 0.746 | 283 | 0.969 | 328 | 0.216 | | | | |
| 14 | 0.079 | 59 | 0.765 | 104 | 0.963 | 149 | 0.202 | 194 | 0.079 | 239 | 0.765 | 284 | 0.963 | 329 | 0.202 | | | | |
| 15 | 0.081 | 60 | 0.783 | 105 | 0.957 | 150 | 0.189 | 195 | 0.081 | 240 | 0.783 | 285 | 0.957 | 330 | 0.189 | | | | |
| 16 | 0.086 | 61 | 0.798 | 106 | 0.948 | 151 | 0.178 | 196 | 0.086 | 241 | 0.798 | 286 | 0.948 | 331 | 0.178 | | | | |
| 17 | 0.089 | 62 | 0.812 | 107 | 0.940 | 152 | 0.167 | 197 | 0.089 | 242 | 0.812 | 287 | 0.940 | 332 | 0.167 | | | | |
| 18 | 0.093 | 63 | 0.826 | 108 | 0.931 | 153 | 0.157 | 198 | 0.093 | 243 | 0.826 | 288 | 0.931 | 333 | 0.157 | | | | |
| 19 | 0.096 | 64 | 0.839 | 109 | 0.922 | 154 | 0.147 | 199 | 0.096 | 244 | 0.839 | 289 | 0.922 | 334 | 0.147 | | | | |
| 20 | 0.098 | 65 | 0.852 | 110 | 0.913 | 155 | 0.137 | 200 | 0.098 | 245 | 0.852 | 290 | 0.913 | 335 | 0.137 | | | | |
| 21 | 0.106 | 66 | 0.865 | 111 | 0.901 | 156 | 0.129 | 201 | 0.106 | 246 | 0.865 | 291 | 0.901 | 336 | 0.129 | | | | |
| 22 | 0.114 | 67 | 0.877 | 112 | 0.889 | 157 | 0.122 | 202 | 0.114 | 247 | 0.877 | 292 | 0.889 | 337 | 0.122 | | | | |
| 23 | 0.122 | 68 | 0.889 | 113 | 0.877 | 158 | 0.114 | 203 | 0.122 | 248 | 0.889 | 293 | 0.877 | 338 | 0.114 | | | | |
| 24 | 0.129 | 69 | 0.901 | 114 | 0.865 | 159 | 0.106 | 204 | 0.129 | 249 | 0.901 | 294 | 0.865 | 339 | 0.106 | | | | |
| 25 | 0.137 | 70 | 0.913 | 115 | 0.852 | 160 | 0.098 | 205 | 0.137 | 250 | 0.913 | 295 | 0.852 | 340 | 0.098 | | | | |
| 26 | 0.147 | 71 | 0.922 | 116 | 0.839 | 161 | 0.096 | 206 | 0.147 | 251 | 0.922 | 296 | 0.839 | 341 | 0.096 | | | | |
| 27 | 0.157 | 72 | 0.931 | 117 | 0.826 | 162 | 0.093 | 207 | 0.157 | 252 | 0.931 | 297 | 0.826 | 342 | 0.093 | | | | |
| 28 | 0.167 | 73 | 0.940 | 118 | 0.812 | 163 | 0.089 | 208 | 0.167 | 253 | 0.940 | 298 | 0.812 | 343 | 0.089 | | | | |
| 29 | 0.178 | 74 | 0.948 | 119 | 0.798 | 164 | 0.086 | 209 | 0.178 | 254 | 0.948 | 299 | 0.798 | 344 | 0.086 | | | | |
| 30 | 0.189 | 75 | 0.957 | 120 | 0.783 | 165 | 0.081 | 210 | 0.189 | 255 | 0.957 | 300 | 0.783 | 345 | 0.081 | | | | |
| 31 | 0.202 | 76 | 0.963 | 121 | 0.765 | 166 | 0.079 | 211 | 0.202 | 256 | 0.963 | 301 | 0.765 | 346 | 0.079 | | | | |
| 32 | 0.216 | 77 | 0.969 | 122 | 0.747 | 167 | 0.077 | 212 | 0.216 | 257 | 0.969 | 302 | 0.747 | 347 | 0.077 | | | | |
| 33 | 0.231 | 78 | 0.975 | 123 | 0.729 | 168 | 0.074 | 213 | 0.231 | 258 | 0.975 | 303 | 0.729 | 348 | 0.074 | | | | |
| 34 | 0.246 | 79 | 0.981 | 124 | 0.710 | 169 | 0.071 | 214 | 0.246 | 259 | 0.981 | 304 | 0.710 | 349 | 0.071 | | | | |
| 35 | 0.262 | 80 | 0.987 | 125 | 0.691 | 170 | 0.068 | 215 | 0.262 | 260 | 0.987 | 305 | 0.691 | 350 | 0.068 | | | | |
| 36 | 0.278 | 81 | 0.989 | 126 | 0.669 | 171 | 0.064 | 216 | 0.278 | 261 | 0.989 | 306 | 0.669 | 351 | 0.064 | | | | |
| 37 | 0.294 | 82 | 0.992 | 127 | 0.647 | 172 | 0.061 | 217 | 0.294 | 262 | 0.992 | 307 | 0.647 | 352 | 0.061 | | | | |
| 38 | 0.311 | 83 | 0.995 | 128 | 0.625 | 173 | 0.057 | 218 | 0.311 | 263 | 0.995 | 308 | 0.625 | 353 | 0.057 | | | | |
| 39 | 0.329 | 84 | 0.997 | 129 | 0.602 | 174 | 0.053 | 219 | 0.329 | 264 | 0.997 | 309 | 0.602 | 354 | 0.053 | | | | |
| 40 | 0.348 | 85 | 1.000 | 130 | 0.578 | 175 | 0.048 | 220 | 0.348 | 265 | 1.000 | 310 | 0.578 | 355 | 0.048 | | | | |
| 41 | 0.370 | 86 | 1.000 | 131 | 0.554 | 176 | 0.047 | 221 | 0.370 | 266 | 1.000 | 311 | 0.554 | 356 | 0.047 | | | | |
| 42 | 0.391 | 87 | 0.999 | 132 | 0.530 | 177 | 0.045 | 222 | 0.391 | 267 | 0.999 | 312 | 0.530 | 357 | 0.045 | | | | |
| 43 | 0.414 | 88 | 0.999 | 133 | 0.506 | 178 | 0.043 | 223 | 0.414 | 268 | 0.999 | 313 | 0.506 | 358 | 0.043 | | | | |
| 44 | 0.436 | 89 | 0.999 | 134 | 0.483 | 179 | 0.041 | 224 | 0.436 | 269 | 0.999 | 314 | 0.483 | 359 | 0.041 | | | | |



Proposal #: **DCA-9073-2** Antenna Type: **THA-P2-2H/4HD-1** Channel: **8 DTV**
 Call Letters: **KCTZ** Location: **Bozeman, MT** Channel: **13 DTV**

| Electrical Specifications | | Value | | Remarks |
|---|-----------|------------------|--------------|--------------------------|
| | | Ratio | dB | |
| RMS Gain at Main Lobe over Halfwave Dipole | Hpol | 4.3 | 6.33 | D8; D13: 4.8 (6.81 dB) |
| | Vpol | | | |
| RMS Gain at Horizontal over Halfwave Dipole | Hpol | 4.3 | 6.33 | D8; D13: 4.8 (6.81 dB) |
| | Vpol | | | |
| Peak Directional Gain over Halfwave Dipole | Hpol | 11.8 | 10.72 | D8; D13: 12.6 (11.02 dB) |
| | Vpol | | | |
| Peak Directional Gain at Horizontal over Halfwave Dipole | Hpol | 11.8 | 10.72 | D8; D13: 12.6 (11.00 dB) |
| | Vpol | | | |
| Circularity | | dB | | |
| Axial Ratio | | dB | | |
| Beam Tilt | | 0.00 deg | | D8; D13: 0.00 deg |
| Average Power | DTV | 5 kW | 6.99 dBk | +5 kW DTV power |
| Antenna Input: | T/L | 3 1/8 in | 50.0 ohm | Type: EIA/DCA |
| Maximum Antenna Input VSWR | | | | |
| | | Channel 1.10 : 1 | | |
| Patterns | Azimuth | THA-P4-8 | THA-P4-13 | D8 D13 |
| | Elevation | 02H043000 | 02H043000-90 | |
| | | 02H048000 | 02H048000-90 | |
| Mechanical Specifications | | Metric | English | Preliminary |
| Height with Lightning Protector | H4 | | | Side mounted |
| Height Less Lightning Protector | H2 | | | |
| Height of Center of Radiation | H3 | | | |
| Basic Wind Speed | V | | | TIA/EIA-222-F. |
| Force Coeff. x Projected Area | CaAc | | | Excludes Mounts |
| Moment Arm | D1 | | | |
| Force Coeff. x Projected Area | CaAc | | | |
| Moment Arm | D3 | | | |
| Pole Bury Length | D2 | | | |
| Weight | W | | | Excludes Mounts |
| Antenna designed in accordance with AISC specifications for design of structural steel for building as prescribed by TIA/EIA-222-F. | | | | |

NOTE: **For loads see specifications sheet for Ch 7 & 9**

Prepared By : SRR
 Original Date : 1-Dec-00

Approved By : RN
 Revision: 2
 Rev. Date: 15-Jan-01

Proposal Number **DCA-9073** Revision: **2**
 Date **15-Jan-01**
 Call Letters **KCTZ, KUSM** Channel **7**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

ELEVATION PATTERN

RMS Gain at Main Lobe

4.20 (6.23 dB)

Beam Tilt

0.00 deg

RMS Gain at Horizontal

4.20 (6.23 dB)

Frequency

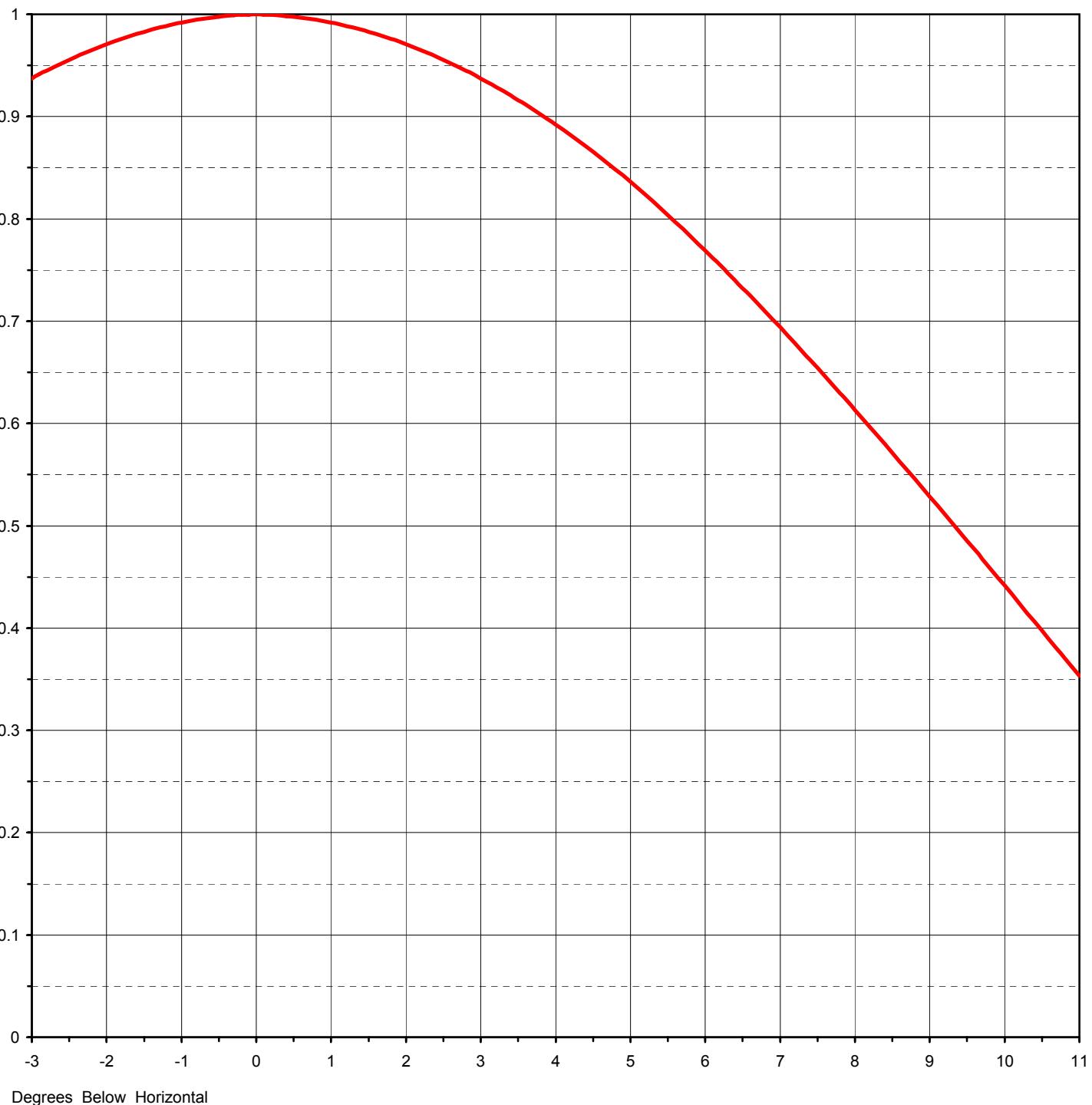
177.00 MHz

Calculated / Measured

Calculated

Drawing #

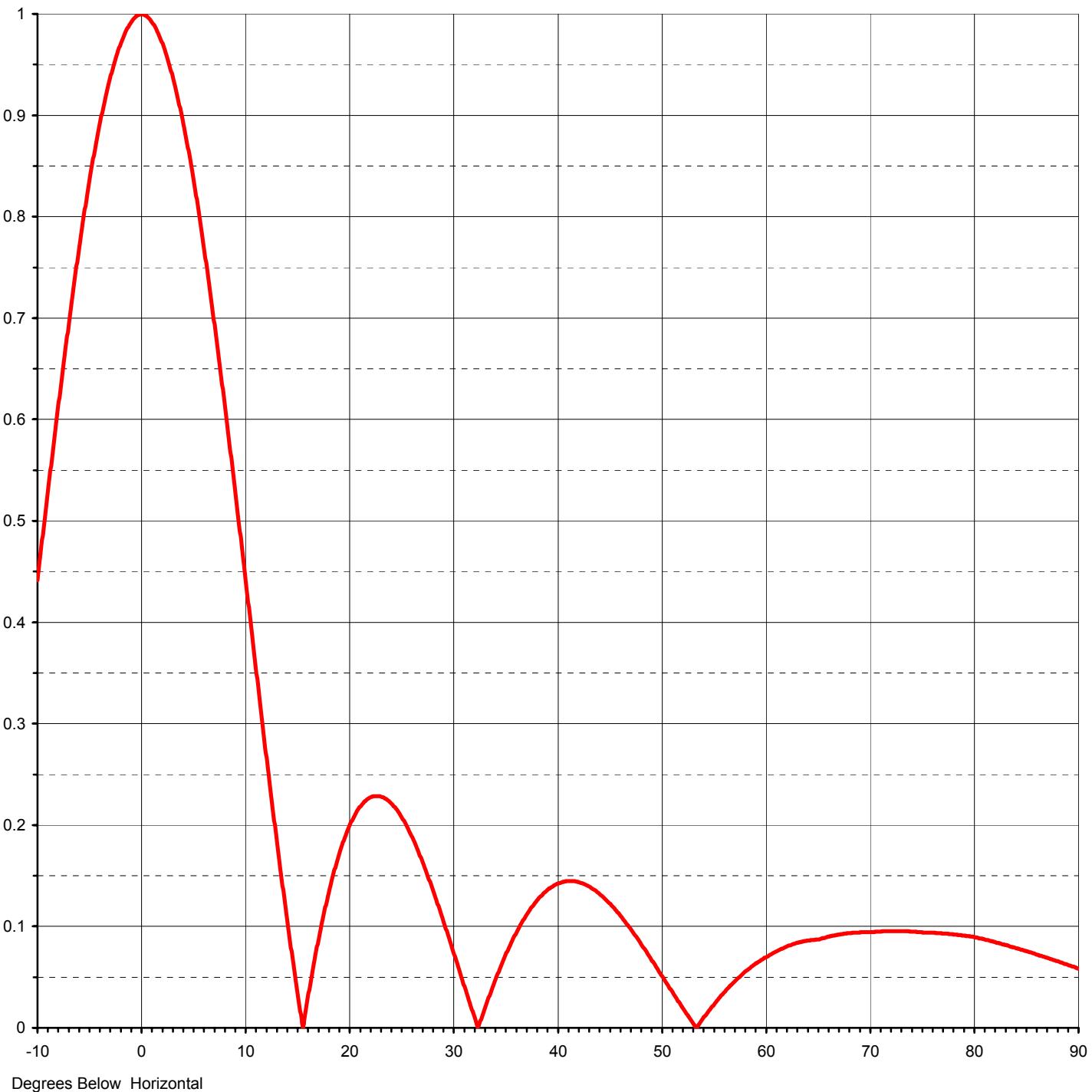
02H042000



Proposal Number **DCA-9073** Revision: **2**
 Date **15-Jan-01**
 Call Letters **KCTZ, KUSM** Channel **7**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

ELEVATION PATTERN

| | | | |
|------------------------|-------------------------|-----------|---------------------|
| RMS Gain at Main Lobe | 4.20 (6.23 dB) | Beam Tilt | 0.00 deg |
| RMS Gain at Horizontal | 4.20 (6.23 dB) | Frequency | 177.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 02H042000-90 |





Proposal Number **DCA-9073** Revision: **2**
Date **15-Jan-01**
Call Letters **KCTZ, KUSM** Channel **7**
Location **Bozeman, MT**
Customer **Cordillera**
Antenna Type **THA-P2-2H/4HD-1**

TABULATION OF ELEVATION PATTERN

Elevation Pattern Drawing #: **02H042000-90**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -10.0 | 0.442 | 2.4 | 0.959 | 10.6 | 0.397 | 30.5 | 0.060 | 51.0 | 0.037 | 71.5 | 0.095 |
| -9.5 | 0.485 | 2.6 | 0.952 | 10.8 | 0.380 | 31.0 | 0.045 | 51.5 | 0.029 | 72.0 | 0.095 |
| -9.0 | 0.529 | 2.8 | 0.945 | 11.0 | 0.362 | 31.5 | 0.029 | 52.0 | 0.021 | 72.5 | 0.095 |
| -8.5 | 0.571 | 3.0 | 0.937 | 11.5 | 0.318 | 32.0 | 0.013 | 52.5 | 0.013 | 73.0 | 0.095 |
| -8.0 | 0.613 | 3.2 | 0.929 | 12.0 | 0.275 | 32.5 | 0.002 | 53.0 | 0.006 | 73.5 | 0.095 |
| -7.5 | 0.654 | 3.4 | 0.921 | 12.5 | 0.233 | 33.0 | 0.017 | 53.5 | 0.002 | 74.0 | 0.095 |
| -7.0 | 0.694 | 3.6 | 0.912 | 13.0 | 0.192 | 33.5 | 0.031 | 54.0 | 0.009 | 74.5 | 0.095 |
| -6.5 | 0.732 | 3.8 | 0.902 | 13.5 | 0.152 | 34.0 | 0.045 | 54.5 | 0.015 | 75.0 | 0.094 |
| -6.0 | 0.769 | 4.0 | 0.892 | 14.0 | 0.113 | 34.5 | 0.058 | 55.0 | 0.022 | 75.5 | 0.094 |
| -5.5 | 0.804 | 4.2 | 0.882 | 14.5 | 0.076 | 35.0 | 0.070 | 55.5 | 0.028 | 76.0 | 0.094 |
| -5.0 | 0.836 | 4.4 | 0.871 | 15.0 | 0.040 | 35.5 | 0.082 | 56.0 | 0.034 | 76.5 | 0.093 |
| -4.5 | 0.866 | 4.6 | 0.860 | 15.5 | 0.007 | 36.0 | 0.092 | 56.5 | 0.040 | 77.0 | 0.093 |
| -4.0 | 0.892 | 4.8 | 0.848 | 16.0 | 0.025 | 36.5 | 0.102 | 57.0 | 0.045 | 77.5 | 0.093 |
| -3.5 | 0.916 | 5.0 | 0.836 | 16.5 | 0.055 | 37.0 | 0.110 | 57.5 | 0.050 | 78.0 | 0.092 |
| -3.0 | 0.937 | 5.2 | 0.824 | 17.0 | 0.082 | 37.5 | 0.118 | 58.0 | 0.055 | 78.5 | 0.092 |
| -2.8 | 0.945 | 5.4 | 0.811 | 17.5 | 0.107 | 38.0 | 0.125 | 58.5 | 0.059 | 79.0 | 0.091 |
| -2.6 | 0.952 | 5.6 | 0.797 | 18.0 | 0.130 | 38.5 | 0.130 | 59.0 | 0.063 | 79.5 | 0.090 |
| -2.4 | 0.959 | 5.8 | 0.783 | 18.5 | 0.150 | 39.0 | 0.135 | 59.5 | 0.066 | 80.0 | 0.090 |
| -2.2 | 0.965 | 6.0 | 0.769 | 19.0 | 0.169 | 39.5 | 0.139 | 60.0 | 0.069 | 80.5 | 0.088 |
| -2.0 | 0.971 | 6.2 | 0.754 | 19.5 | 0.184 | 40.0 | 0.142 | 60.5 | 0.072 | 81.0 | 0.087 |
| -1.8 | 0.976 | 6.4 | 0.740 | 20.0 | 0.198 | 40.5 | 0.144 | 61.0 | 0.075 | 81.5 | 0.086 |
| -1.6 | 0.981 | 6.6 | 0.725 | 20.5 | 0.208 | 41.0 | 0.145 | 61.5 | 0.078 | 82.0 | 0.084 |
| -1.4 | 0.985 | 6.8 | 0.710 | 21.0 | 0.217 | 41.5 | 0.145 | 62.0 | 0.080 | 82.5 | 0.083 |
| -1.2 | 0.989 | 7.0 | 0.694 | 21.5 | 0.223 | 42.0 | 0.144 | 62.5 | 0.082 | 83.0 | 0.082 |
| -1.0 | 0.992 | 7.2 | 0.678 | 22.0 | 0.227 | 42.5 | 0.142 | 63.0 | 0.083 | 83.5 | 0.080 |
| -0.8 | 0.994 | 7.4 | 0.662 | 22.5 | 0.229 | 43.0 | 0.140 | 63.5 | 0.085 | 84.0 | 0.079 |
| -0.6 | 0.997 | 7.6 | 0.646 | 23.0 | 0.228 | 43.5 | 0.137 | 64.0 | 0.086 | 84.5 | 0.077 |
| -0.4 | 0.998 | 7.8 | 0.630 | 23.5 | 0.226 | 44.0 | 0.133 | 64.5 | 0.087 | 85.0 | 0.075 |
| -0.2 | 0.999 | 8.0 | 0.613 | 24.0 | 0.222 | 44.5 | 0.128 | 65.0 | 0.087 | 85.5 | 0.074 |
| 0.0 | 1.000 | 8.2 | 0.597 | 24.5 | 0.217 | 45.0 | 0.123 | 65.5 | 0.089 | 86.0 | 0.072 |
| 0.2 | 0.999 | 8.4 | 0.580 | 25.0 | 0.209 | 45.5 | 0.118 | 66.0 | 0.090 | 86.5 | 0.071 |
| 0.4 | 0.998 | 8.6 | 0.563 | 25.5 | 0.200 | 46.0 | 0.112 | 66.5 | 0.091 | 87.0 | 0.069 |
| 0.6 | 0.997 | 8.8 | 0.546 | 26.0 | 0.190 | 46.5 | 0.105 | 67.0 | 0.092 | 87.5 | 0.067 |
| 0.8 | 0.994 | 9.0 | 0.529 | 26.5 | 0.178 | 47.0 | 0.099 | 67.5 | 0.093 | 88.0 | 0.066 |
| 1.0 | 0.992 | 9.2 | 0.511 | 27.0 | 0.166 | 47.5 | 0.091 | 68.0 | 0.093 | 88.5 | 0.064 |
| 1.2 | 0.989 | 9.4 | 0.494 | 27.5 | 0.153 | 48.0 | 0.084 | 68.5 | 0.094 | 89.0 | 0.062 |
| 1.4 | 0.985 | 9.6 | 0.477 | 28.0 | 0.138 | 48.5 | 0.076 | 69.0 | 0.094 | 89.5 | 0.060 |
| 1.6 | 0.981 | 9.8 | 0.468 | 28.5 | 0.123 | 49.0 | 0.068 | 69.5 | 0.094 | 90.0 | 0.058 |
| 1.8 | 0.976 | 10.0 | 0.450 | 29.0 | 0.108 | 49.5 | 0.061 | 70.0 | 0.094 | | |
| 2.0 | 0.971 | 10.2 | 0.433 | 29.5 | 0.093 | 50.0 | 0.053 | 70.5 | 0.095 | | |
| 2.2 | 0.965 | 10.4 | 0.415 | 30.0 | 0.077 | 50.5 | 0.045 | 71.0 | 0.095 | | |

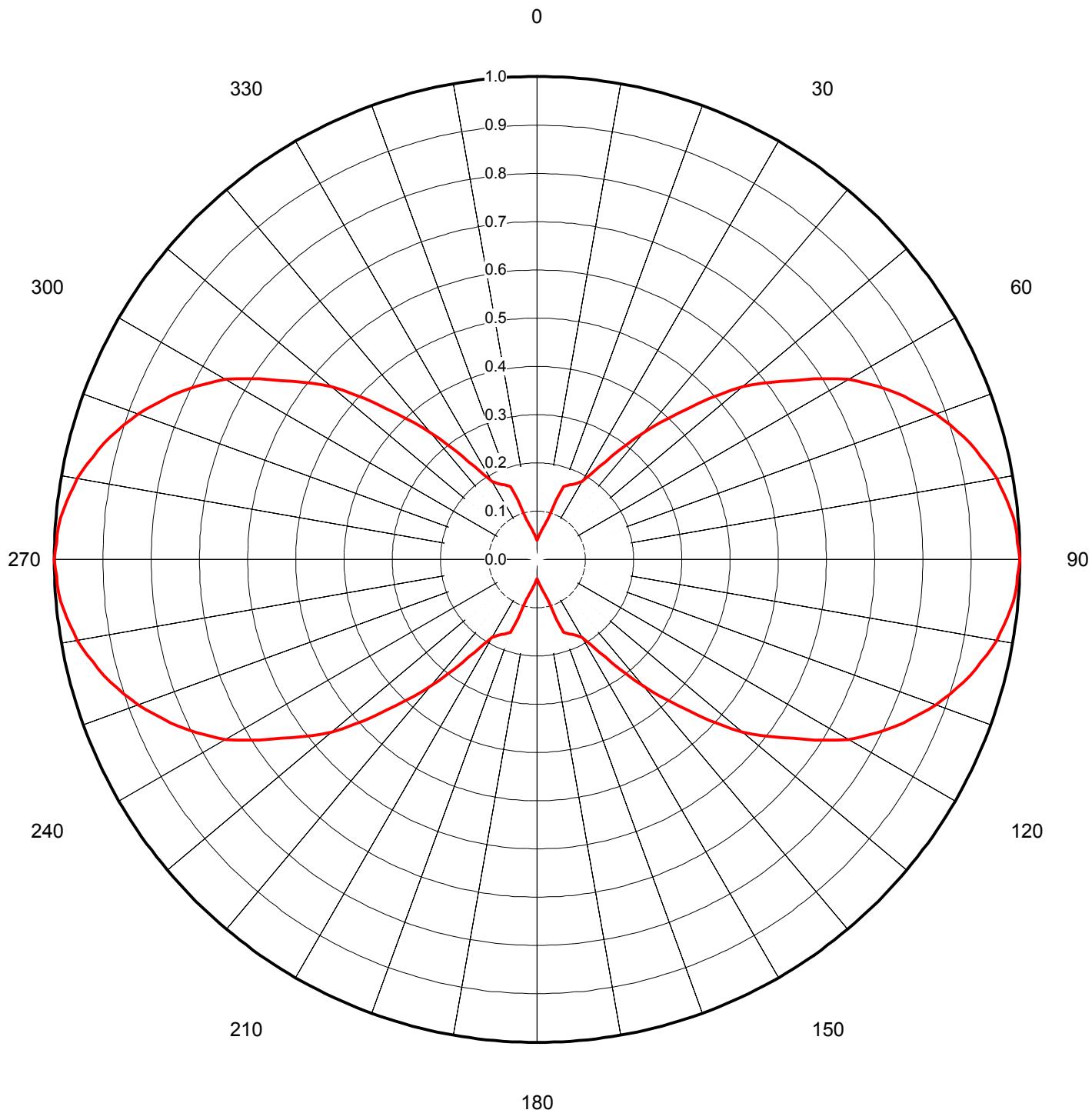
Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

DCA-9073 Revision: **2**
15-Jan-01
KCTZ, KUSM Channel **7**
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

AZIMUTH PATTERN

Gain **2.78** (4.44 dB)
Calculated / Measured **Calculated**

Frequency
Drawing #
177.00 MHz
THA-P2-7





Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

DCA-9073
15-Jan-01
KCTZ, KUSM
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

Revision: **2**
Channel **7**

TABULATION OF AZIMUTH PATTERN

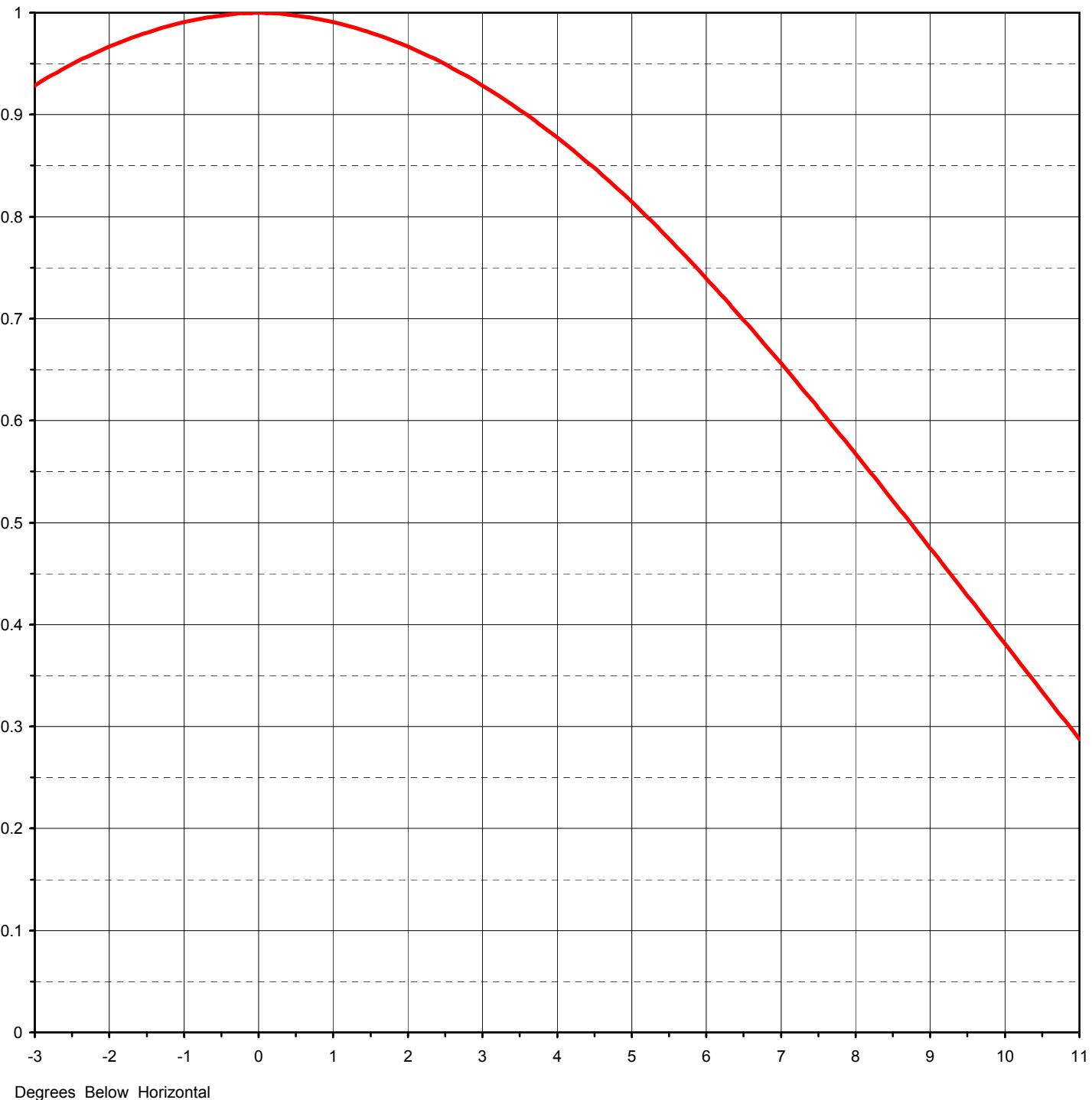
Azimuth Pattern Drawing #: **THA-P2-7**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0.040 | 45 | 0.442 | 90 | 1.000 | 135 | 0.442 | 180 | 0.040 | 225 | 0.442 | 270 | 1.000 | 315 | 0.442 | | | | |
| 1 | 0.042 | 46 | 0.465 | 91 | 0.998 | 136 | 0.421 | 181 | 0.042 | 226 | 0.465 | 271 | 0.998 | 316 | 0.421 | | | | |
| 2 | 0.043 | 47 | 0.488 | 92 | 0.996 | 137 | 0.401 | 182 | 0.043 | 227 | 0.488 | 272 | 0.996 | 317 | 0.401 | | | | |
| 3 | 0.045 | 48 | 0.511 | 93 | 0.995 | 138 | 0.381 | 183 | 0.045 | 228 | 0.511 | 273 | 0.995 | 318 | 0.381 | | | | |
| 4 | 0.047 | 49 | 0.534 | 94 | 0.993 | 139 | 0.361 | 184 | 0.047 | 229 | 0.534 | 274 | 0.993 | 319 | 0.361 | | | | |
| 5 | 0.049 | 50 | 0.556 | 95 | 0.991 | 140 | 0.342 | 185 | 0.049 | 230 | 0.556 | 275 | 0.991 | 320 | 0.342 | | | | |
| 6 | 0.052 | 51 | 0.575 | 96 | 0.986 | 141 | 0.322 | 186 | 0.052 | 231 | 0.575 | 276 | 0.986 | 321 | 0.322 | | | | |
| 7 | 0.055 | 52 | 0.592 | 97 | 0.981 | 142 | 0.302 | 187 | 0.055 | 232 | 0.592 | 277 | 0.981 | 322 | 0.302 | | | | |
| 8 | 0.058 | 53 | 0.610 | 98 | 0.976 | 143 | 0.283 | 188 | 0.058 | 233 | 0.610 | 278 | 0.976 | 323 | 0.283 | | | | |
| 9 | 0.061 | 54 | 0.628 | 99 | 0.972 | 144 | 0.264 | 189 | 0.061 | 234 | 0.628 | 279 | 0.972 | 324 | 0.264 | | | | |
| 10 | 0.064 | 55 | 0.645 | 100 | 0.967 | 145 | 0.247 | 190 | 0.064 | 235 | 0.645 | 280 | 0.967 | 325 | 0.247 | | | | |
| 11 | 0.069 | 56 | 0.666 | 101 | 0.959 | 146 | 0.232 | 191 | 0.069 | 236 | 0.666 | 281 | 0.959 | 326 | 0.232 | | | | |
| 12 | 0.073 | 57 | 0.686 | 102 | 0.952 | 147 | 0.219 | 192 | 0.073 | 237 | 0.686 | 282 | 0.952 | 327 | 0.219 | | | | |
| 13 | 0.077 | 58 | 0.706 | 103 | 0.944 | 148 | 0.207 | 193 | 0.077 | 238 | 0.706 | 283 | 0.944 | 328 | 0.207 | | | | |
| 14 | 0.081 | 59 | 0.726 | 104 | 0.937 | 149 | 0.196 | 194 | 0.081 | 239 | 0.726 | 284 | 0.937 | 329 | 0.196 | | | | |
| 15 | 0.084 | 60 | 0.746 | 105 | 0.929 | 150 | 0.186 | 195 | 0.084 | 240 | 0.746 | 285 | 0.929 | 330 | 0.186 | | | | |
| 16 | 0.099 | 61 | 0.760 | 106 | 0.919 | 151 | 0.182 | 196 | 0.099 | 241 | 0.760 | 286 | 0.919 | 331 | 0.182 | | | | |
| 17 | 0.114 | 62 | 0.775 | 107 | 0.910 | 152 | 0.179 | 197 | 0.114 | 242 | 0.775 | 287 | 0.910 | 332 | 0.179 | | | | |
| 18 | 0.130 | 63 | 0.790 | 108 | 0.900 | 153 | 0.176 | 198 | 0.130 | 243 | 0.790 | 288 | 0.900 | 333 | 0.176 | | | | |
| 19 | 0.145 | 64 | 0.804 | 109 | 0.890 | 154 | 0.174 | 199 | 0.145 | 244 | 0.804 | 289 | 0.890 | 334 | 0.174 | | | | |
| 20 | 0.160 | 65 | 0.818 | 110 | 0.880 | 155 | 0.171 | 200 | 0.160 | 245 | 0.818 | 290 | 0.880 | 335 | 0.171 | | | | |
| 21 | 0.163 | 66 | 0.831 | 111 | 0.868 | 156 | 0.169 | 201 | 0.163 | 246 | 0.831 | 291 | 0.868 | 336 | 0.169 | | | | |
| 22 | 0.165 | 67 | 0.843 | 112 | 0.856 | 157 | 0.167 | 202 | 0.165 | 247 | 0.843 | 292 | 0.856 | 337 | 0.167 | | | | |
| 23 | 0.167 | 68 | 0.856 | 113 | 0.843 | 158 | 0.165 | 203 | 0.167 | 248 | 0.856 | 293 | 0.843 | 338 | 0.165 | | | | |
| 24 | 0.169 | 69 | 0.868 | 114 | 0.831 | 159 | 0.163 | 204 | 0.169 | 249 | 0.868 | 294 | 0.831 | 339 | 0.163 | | | | |
| 25 | 0.171 | 70 | 0.880 | 115 | 0.818 | 160 | 0.160 | 205 | 0.171 | 250 | 0.880 | 295 | 0.818 | 340 | 0.160 | | | | |
| 26 | 0.174 | 71 | 0.890 | 116 | 0.804 | 161 | 0.145 | 206 | 0.174 | 251 | 0.890 | 296 | 0.804 | 341 | 0.145 | | | | |
| 27 | 0.176 | 72 | 0.900 | 117 | 0.790 | 162 | 0.130 | 207 | 0.176 | 252 | 0.900 | 297 | 0.790 | 342 | 0.130 | | | | |
| 28 | 0.179 | 73 | 0.910 | 118 | 0.775 | 163 | 0.114 | 208 | 0.179 | 253 | 0.910 | 298 | 0.775 | 343 | 0.114 | | | | |
| 29 | 0.182 | 74 | 0.919 | 119 | 0.760 | 164 | 0.099 | 209 | 0.182 | 254 | 0.919 | 299 | 0.760 | 344 | 0.099 | | | | |
| 30 | 0.186 | 75 | 0.929 | 120 | 0.746 | 165 | 0.084 | 210 | 0.186 | 255 | 0.929 | 300 | 0.746 | 345 | 0.084 | | | | |
| 31 | 0.196 | 76 | 0.937 | 121 | 0.726 | 166 | 0.081 | 211 | 0.196 | 256 | 0.937 | 301 | 0.726 | 346 | 0.081 | | | | |
| 32 | 0.207 | 77 | 0.944 | 122 | 0.706 | 167 | 0.077 | 212 | 0.207 | 257 | 0.944 | 302 | 0.706 | 347 | 0.077 | | | | |
| 33 | 0.219 | 78 | 0.952 | 123 | 0.686 | 168 | 0.073 | 213 | 0.219 | 258 | 0.952 | 303 | 0.686 | 348 | 0.073 | | | | |
| 34 | 0.232 | 79 | 0.959 | 124 | 0.666 | 169 | 0.069 | 214 | 0.232 | 259 | 0.959 | 304 | 0.666 | 349 | 0.069 | | | | |
| 35 | 0.247 | 80 | 0.967 | 125 | 0.645 | 170 | 0.064 | 215 | 0.247 | 260 | 0.967 | 305 | 0.645 | 350 | 0.064 | | | | |
| 36 | 0.264 | 81 | 0.972 | 126 | 0.628 | 171 | 0.061 | 216 | 0.264 | 261 | 0.972 | 306 | 0.628 | 351 | 0.061 | | | | |
| 37 | 0.283 | 82 | 0.976 | 127 | 0.610 | 172 | 0.058 | 217 | 0.283 | 262 | 0.976 | 307 | 0.610 | 352 | 0.058 | | | | |
| 38 | 0.302 | 83 | 0.981 | 128 | 0.592 | 173 | 0.055 | 218 | 0.302 | 263 | 0.981 | 308 | 0.592 | 353 | 0.055 | | | | |
| 39 | 0.322 | 84 | 0.986 | 129 | 0.575 | 174 | 0.052 | 219 | 0.322 | 264 | 0.986 | 309 | 0.575 | 354 | 0.052 | | | | |
| 40 | 0.342 | 85 | 0.991 | 130 | 0.556 | 175 | 0.049 | 220 | 0.342 | 265 | 0.991 | 310 | 0.556 | 355 | 0.049 | | | | |
| 41 | 0.361 | 86 | 0.993 | 131 | 0.534 | 176 | 0.047 | 221 | 0.361 | 266 | 0.993 | 311 | 0.534 | 356 | 0.047 | | | | |
| 42 | 0.381 | 87 | 0.995 | 132 | 0.511 | 177 | 0.045 | 222 | 0.381 | 267 | 0.995 | 312 | 0.511 | 357 | 0.045 | | | | |
| 43 | 0.401 | 88 | 0.996 | 133 | 0.488 | 178 | 0.043 | 223 | 0.401 | 268 | 0.996 | 313 | 0.488 | 358 | 0.043 | | | | |
| 44 | 0.421 | 89 | 0.998 | 134 | 0.465 | 179 | 0.042 | 224 | 0.421 | 269 | 0.998 | 314 | 0.465 | 359 | 0.042 | | | | |

Proposal Number **DCA-9073** Revision: **2**
 Date **15-Jan-01**
 Call Letters **KCTZ, KUSM-D** Channel **9**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

ELEVATION PATTERN

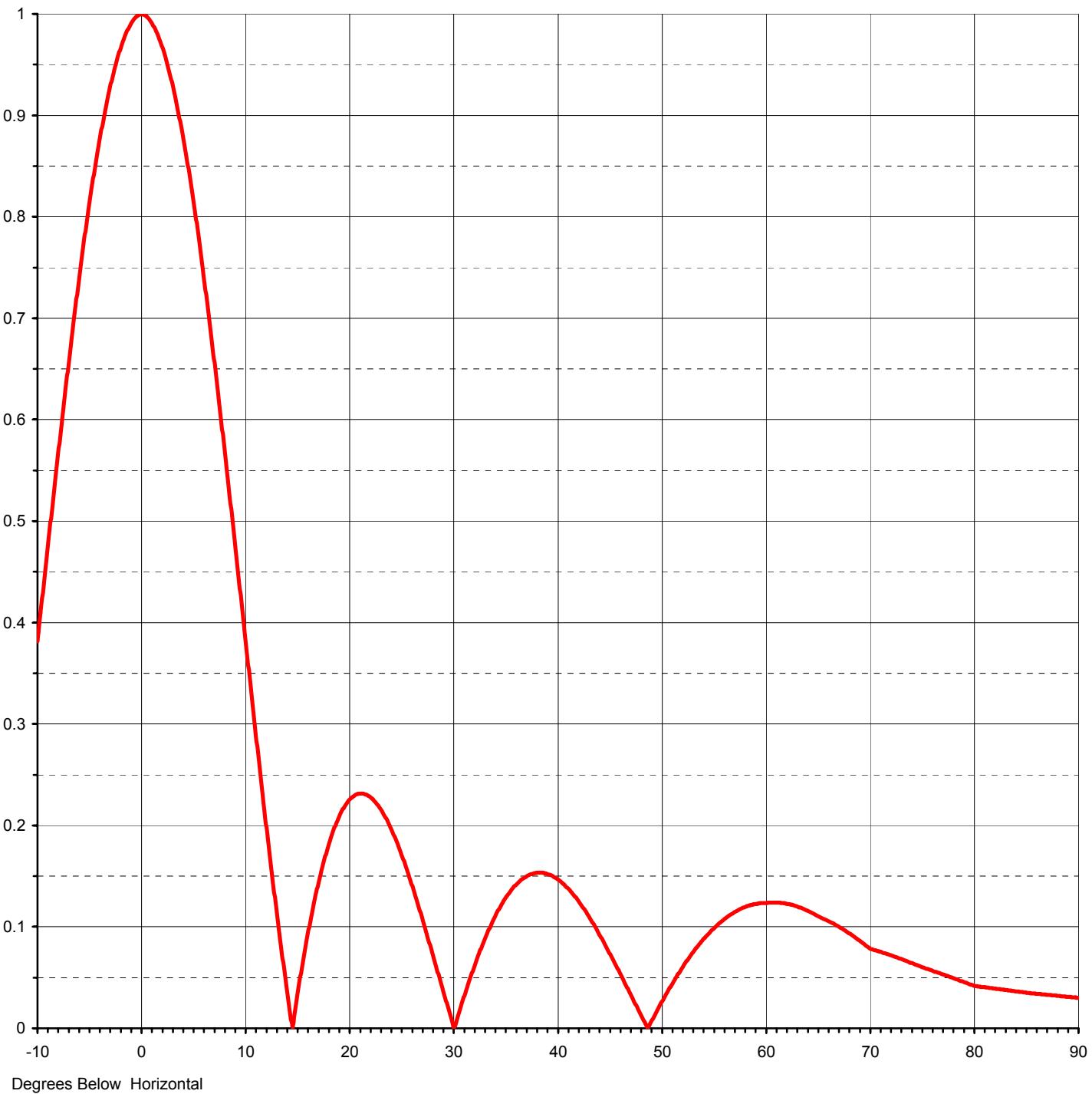
| | | | |
|------------------------|-------------------------|-----------|-------------------|
| RMS Gain at Main Lobe | 4.40 (6.43 dB) | Beam Tilt | 0.00 deg |
| RMS Gain at Horizontal | 4.40 (6.43 dB) | Frequency | 189.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 02H044000 |



Proposal Number **DCA-9073** Revision: **2**
 Date **15-Jan-01**
 Call Letters **KCTZ, KUSM-D** Channel **9**
 Location **Bozeman, MT**
 Customer **Cordillera**
 Antenna Type **THA-P2-2H/4HD-1**

ELEVATION PATTERN

| | | | |
|------------------------|-------------------------|-----------|---------------------|
| RMS Gain at Main Lobe | 4.40 (6.43 dB) | Beam Tilt | 0.00 deg |
| RMS Gain at Horizontal | 4.40 (6.43 dB) | Frequency | 189.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 02H044000-90 |



Degrees Below Horizontal



Proposal Number **DCA-9073** Revision: **2**
Date **15-Jan-01**
Call Letters **KCTZ, KUSM-I** Channel **9**
Location **Bozeman, MT**
Customer **Cordillera**
Antenna Type **THA-P2-2H/4HD-1**

TABULATION OF ELEVATION PATTERN

Elevation Pattern Drawing #: **02H044000-90**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -10.0 | 0.382 | 2.4 | 0.953 | 10.6 | 0.334 | 30.5 | 0.012 | 51.0 | 0.043 | 71.5 | 0.074 |
| -9.5 | 0.428 | 2.6 | 0.946 | 10.8 | 0.316 | 31.0 | 0.029 | 51.5 | 0.051 | 72.0 | 0.072 |
| -9.0 | 0.475 | 2.8 | 0.937 | 11.0 | 0.297 | 31.5 | 0.044 | 52.0 | 0.059 | 72.5 | 0.070 |
| -8.5 | 0.521 | 3.0 | 0.929 | 11.5 | 0.251 | 32.0 | 0.059 | 52.5 | 0.067 | 73.0 | 0.068 |
| -8.0 | 0.567 | 3.2 | 0.919 | 12.0 | 0.206 | 32.5 | 0.073 | 53.0 | 0.074 | 73.5 | 0.066 |
| -7.5 | 0.612 | 3.4 | 0.910 | 12.5 | 0.163 | 33.0 | 0.086 | 53.5 | 0.081 | 74.0 | 0.064 |
| -7.0 | 0.656 | 3.6 | 0.900 | 13.0 | 0.121 | 33.5 | 0.098 | 54.0 | 0.087 | 74.5 | 0.062 |
| -6.5 | 0.699 | 3.8 | 0.889 | 13.5 | 0.081 | 34.0 | 0.109 | 54.5 | 0.093 | 75.0 | 0.060 |
| -6.0 | 0.739 | 4.0 | 0.878 | 14.0 | 0.042 | 34.5 | 0.119 | 55.0 | 0.098 | 75.5 | 0.058 |
| -5.5 | 0.778 | 4.2 | 0.866 | 14.5 | 0.006 | 35.0 | 0.127 | 55.5 | 0.102 | 76.0 | 0.057 |
| -5.0 | 0.815 | 4.4 | 0.854 | 15.0 | 0.028 | 35.5 | 0.135 | 56.0 | 0.107 | 76.5 | 0.055 |
| -4.5 | 0.848 | 4.6 | 0.841 | 15.5 | 0.060 | 36.0 | 0.141 | 56.5 | 0.111 | 77.0 | 0.053 |
| -4.0 | 0.878 | 4.8 | 0.828 | 16.0 | 0.089 | 36.5 | 0.146 | 57.0 | 0.114 | 77.5 | 0.051 |
| -3.5 | 0.905 | 5.0 | 0.815 | 16.5 | 0.115 | 37.0 | 0.149 | 57.5 | 0.117 | 78.0 | 0.049 |
| -3.0 | 0.929 | 5.2 | 0.800 | 17.0 | 0.139 | 37.5 | 0.152 | 58.0 | 0.119 | 78.5 | 0.047 |
| -2.8 | 0.937 | 5.4 | 0.786 | 17.5 | 0.160 | 38.0 | 0.153 | 58.5 | 0.121 | 79.0 | 0.046 |
| -2.6 | 0.946 | 5.6 | 0.771 | 18.0 | 0.178 | 38.5 | 0.153 | 59.0 | 0.122 | 79.5 | 0.044 |
| -2.4 | 0.953 | 5.8 | 0.755 | 18.5 | 0.194 | 39.0 | 0.152 | 59.5 | 0.123 | 80.0 | 0.042 |
| -2.2 | 0.960 | 6.0 | 0.739 | 19.0 | 0.207 | 39.5 | 0.150 | 60.0 | 0.123 | 80.5 | 0.041 |
| -2.0 | 0.967 | 6.2 | 0.723 | 19.5 | 0.217 | 40.0 | 0.147 | 60.5 | 0.124 | 81.0 | 0.041 |
| -1.8 | 0.973 | 6.4 | 0.707 | 20.0 | 0.225 | 40.5 | 0.143 | 61.0 | 0.124 | 81.5 | 0.040 |
| -1.6 | 0.978 | 6.6 | 0.690 | 20.5 | 0.229 | 41.0 | 0.139 | 61.5 | 0.124 | 82.0 | 0.039 |
| -1.4 | 0.983 | 6.8 | 0.673 | 21.0 | 0.231 | 41.5 | 0.133 | 62.0 | 0.123 | 82.5 | 0.038 |
| -1.2 | 0.987 | 7.0 | 0.656 | 21.5 | 0.231 | 42.0 | 0.126 | 62.5 | 0.122 | 83.0 | 0.038 |
| -1.0 | 0.991 | 7.2 | 0.639 | 22.0 | 0.228 | 42.5 | 0.119 | 63.0 | 0.120 | 83.5 | 0.037 |
| -0.8 | 0.994 | 7.4 | 0.621 | 22.5 | 0.224 | 43.0 | 0.111 | 63.5 | 0.119 | 84.0 | 0.036 |
| -0.6 | 0.996 | 7.6 | 0.603 | 23.0 | 0.217 | 43.5 | 0.103 | 64.0 | 0.116 | 84.5 | 0.036 |
| -0.4 | 0.998 | 7.8 | 0.586 | 23.5 | 0.208 | 44.0 | 0.094 | 64.5 | 0.113 | 85.0 | 0.035 |
| -0.2 | 0.999 | 8.0 | 0.567 | 24.0 | 0.198 | 44.5 | 0.085 | 65.0 | 0.110 | 85.5 | 0.034 |
| 0.0 | 1.000 | 8.2 | 0.549 | 24.5 | 0.186 | 45.0 | 0.075 | 65.5 | 0.108 | 86.0 | 0.034 |
| 0.2 | 0.999 | 8.4 | 0.531 | 25.0 | 0.173 | 45.5 | 0.065 | 66.0 | 0.106 | 86.5 | 0.034 |
| 0.4 | 0.998 | 8.6 | 0.512 | 25.5 | 0.159 | 46.0 | 0.055 | 66.5 | 0.103 | 87.0 | 0.033 |
| 0.6 | 0.996 | 8.8 | 0.494 | 26.0 | 0.143 | 46.5 | 0.045 | 67.0 | 0.100 | 87.5 | 0.032 |
| 0.8 | 0.994 | 9.0 | 0.475 | 26.5 | 0.127 | 47.0 | 0.035 | 67.5 | 0.097 | 88.0 | 0.032 |
| 1.0 | 0.991 | 9.2 | 0.456 | 27.0 | 0.110 | 47.5 | 0.025 | 68.0 | 0.093 | 88.5 | 0.032 |
| 1.2 | 0.987 | 9.4 | 0.438 | 27.5 | 0.093 | 48.0 | 0.014 | 68.5 | 0.090 | 89.0 | 0.031 |
| 1.4 | 0.983 | 9.6 | 0.419 | 28.0 | 0.075 | 48.5 | 0.004 | 69.0 | 0.086 | 89.5 | 0.031 |
| 1.6 | 0.978 | 9.8 | 0.410 | 28.5 | 0.057 | 49.0 | 0.005 | 69.5 | 0.082 | 90.0 | 0.030 |
| 1.8 | 0.973 | 10.0 | 0.391 | 29.0 | 0.040 | 49.5 | 0.015 | 70.0 | 0.078 | | |
| 2.0 | 0.967 | 10.2 | 0.372 | 29.5 | 0.022 | 50.0 | 0.024 | 70.5 | 0.077 | | |
| 2.2 | 0.960 | 10.4 | 0.353 | 30.0 | 0.004 | 50.5 | 0.034 | 71.0 | 0.075 | | |



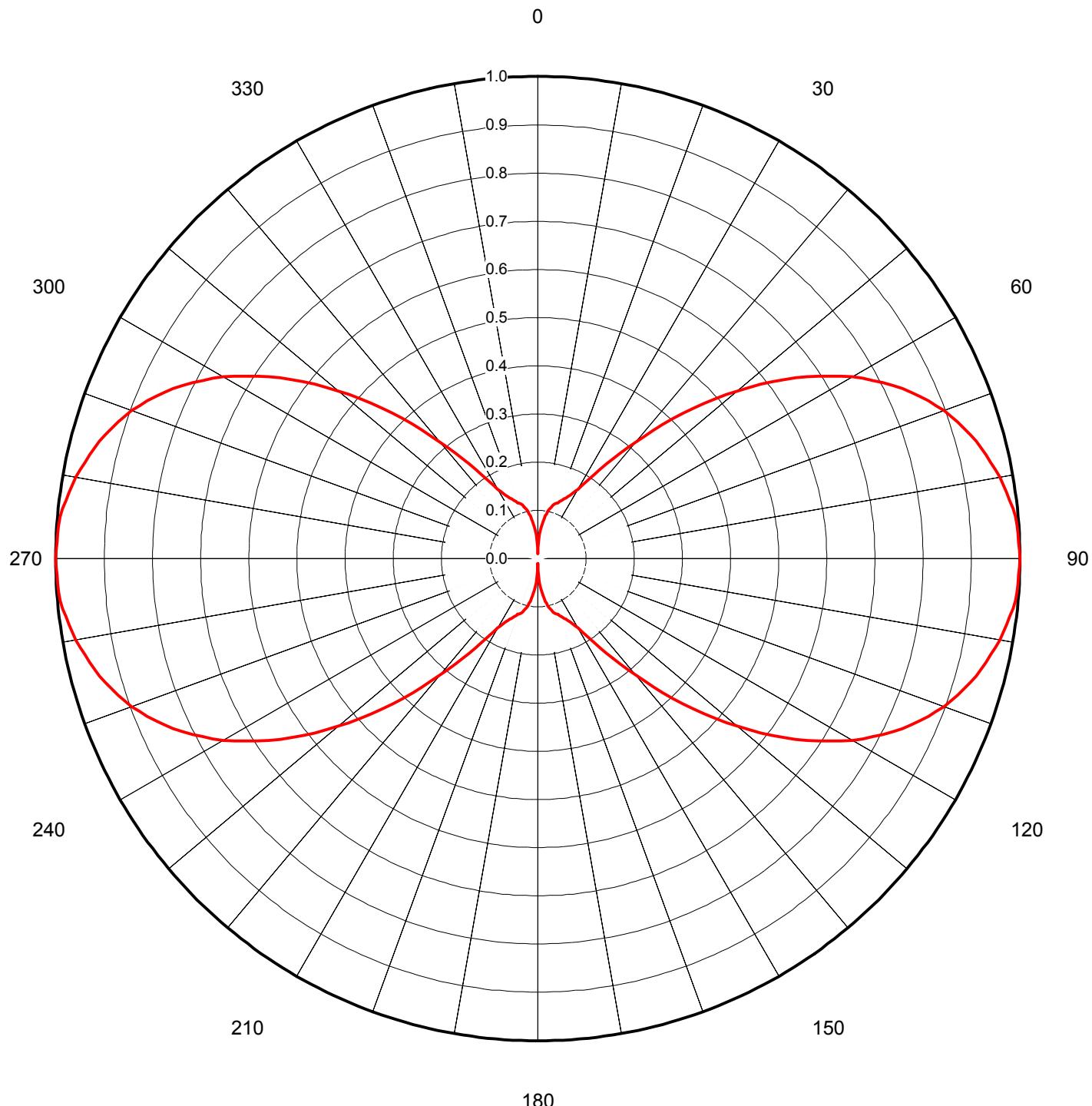
Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

DCA-9073 Revision: 2
15-Jan-01
KCTZ, KUSM-L Channel 9
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

AZIMUTH PATTERN

Gain **2.76**
Calculated / Measured
(4.41 dB)
Calculated

Frequency
Drawing #
189.00 MHz
THA-P2-9





Proposal Number
Date
Call Letters
Location
Customer
Antenna Type

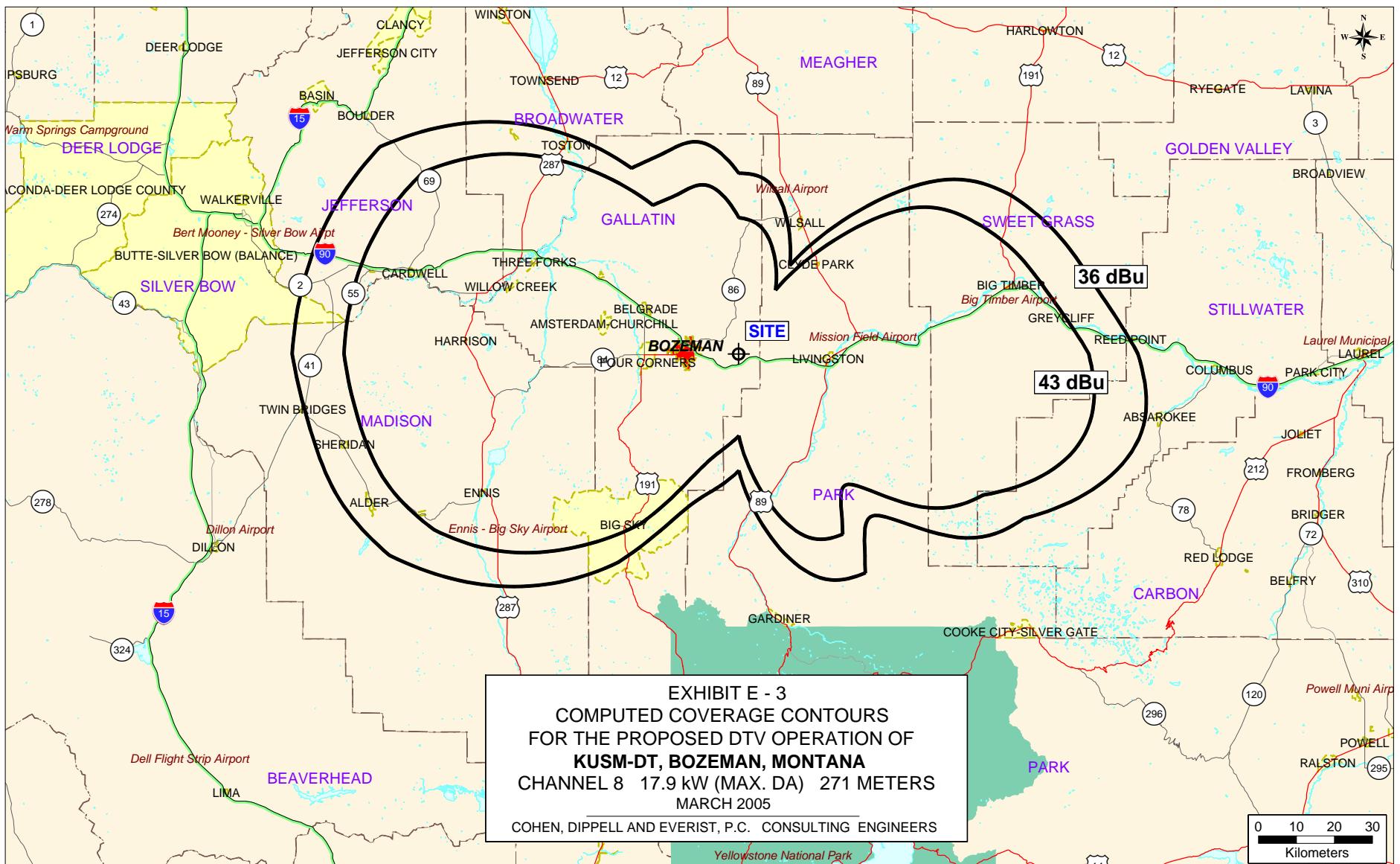
DCA-9073
15-Jan-01
KCTZ, KUSM-DT Channel
Bozeman, MT
Cordillera
THA-P2-2H/4HD-1

Revision: **2**
9

TABULATION OF AZIMUTH PATTERN

Azimuth Pattern Drawing #: **THA-P2-9**

| Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0.010 | 45 | 0.426 | 90 | 1.000 | 135 | 0.426 | 180 | 0.010 | 225 | 0.426 | 270 | 1.000 | 315 | 0.426 | | | | |
| 1 | 0.020 | 46 | 0.449 | 91 | 0.999 | 136 | 0.403 | 181 | 0.020 | 226 | 0.449 | 271 | 0.999 | 316 | 0.403 | | | | |
| 2 | 0.030 | 47 | 0.472 | 92 | 0.998 | 137 | 0.381 | 182 | 0.030 | 227 | 0.472 | 272 | 0.998 | 317 | 0.381 | | | | |
| 3 | 0.040 | 48 | 0.495 | 93 | 0.997 | 138 | 0.358 | 183 | 0.040 | 228 | 0.495 | 273 | 0.997 | 318 | 0.358 | | | | |
| 4 | 0.049 | 49 | 0.518 | 94 | 0.996 | 139 | 0.336 | 184 | 0.049 | 229 | 0.518 | 274 | 0.996 | 319 | 0.336 | | | | |
| 5 | 0.058 | 50 | 0.541 | 95 | 0.995 | 140 | 0.314 | 185 | 0.058 | 230 | 0.541 | 275 | 0.995 | 320 | 0.314 | | | | |
| 6 | 0.065 | 51 | 0.564 | 96 | 0.990 | 141 | 0.295 | 186 | 0.065 | 231 | 0.564 | 276 | 0.990 | 321 | 0.295 | | | | |
| 7 | 0.072 | 52 | 0.587 | 97 | 0.986 | 142 | 0.276 | 187 | 0.072 | 232 | 0.587 | 277 | 0.986 | 322 | 0.276 | | | | |
| 8 | 0.078 | 53 | 0.609 | 98 | 0.982 | 143 | 0.259 | 188 | 0.078 | 233 | 0.609 | 278 | 0.982 | 323 | 0.259 | | | | |
| 9 | 0.084 | 54 | 0.631 | 99 | 0.977 | 144 | 0.242 | 189 | 0.084 | 234 | 0.631 | 279 | 0.977 | 324 | 0.242 | | | | |
| 10 | 0.089 | 55 | 0.653 | 100 | 0.973 | 145 | 0.226 | 190 | 0.089 | 235 | 0.653 | 280 | 0.973 | 325 | 0.226 | | | | |
| 11 | 0.095 | 56 | 0.674 | 101 | 0.967 | 146 | 0.212 | 191 | 0.095 | 236 | 0.674 | 281 | 0.967 | 326 | 0.212 | | | | |
| 12 | 0.100 | 57 | 0.694 | 102 | 0.960 | 147 | 0.199 | 192 | 0.100 | 237 | 0.694 | 282 | 0.960 | 327 | 0.199 | | | | |
| 13 | 0.105 | 58 | 0.714 | 103 | 0.954 | 148 | 0.187 | 193 | 0.105 | 238 | 0.714 | 283 | 0.954 | 328 | 0.187 | | | | |
| 14 | 0.108 | 59 | 0.734 | 104 | 0.948 | 149 | 0.176 | 194 | 0.108 | 239 | 0.734 | 284 | 0.948 | 329 | 0.176 | | | | |
| 15 | 0.112 | 60 | 0.753 | 105 | 0.941 | 150 | 0.167 | 195 | 0.112 | 240 | 0.753 | 285 | 0.941 | 330 | 0.167 | | | | |
| 16 | 0.115 | 61 | 0.770 | 106 | 0.933 | 151 | 0.160 | 196 | 0.115 | 241 | 0.770 | 286 | 0.933 | 331 | 0.160 | | | | |
| 17 | 0.119 | 62 | 0.787 | 107 | 0.924 | 152 | 0.154 | 197 | 0.119 | 242 | 0.787 | 287 | 0.924 | 332 | 0.154 | | | | |
| 18 | 0.121 | 63 | 0.803 | 108 | 0.915 | 153 | 0.148 | 198 | 0.121 | 243 | 0.803 | 288 | 0.915 | 333 | 0.148 | | | | |
| 19 | 0.122 | 64 | 0.819 | 109 | 0.906 | 154 | 0.143 | 199 | 0.122 | 244 | 0.819 | 289 | 0.906 | 334 | 0.143 | | | | |
| 20 | 0.123 | 65 | 0.835 | 110 | 0.897 | 155 | 0.138 | 200 | 0.123 | 245 | 0.835 | 290 | 0.897 | 335 | 0.138 | | | | |
| 21 | 0.126 | 66 | 0.848 | 111 | 0.885 | 156 | 0.136 | 201 | 0.126 | 246 | 0.848 | 291 | 0.885 | 336 | 0.136 | | | | |
| 22 | 0.130 | 67 | 0.861 | 112 | 0.873 | 157 | 0.133 | 202 | 0.130 | 247 | 0.861 | 292 | 0.873 | 337 | 0.133 | | | | |
| 23 | 0.133 | 68 | 0.873 | 113 | 0.861 | 158 | 0.130 | 203 | 0.133 | 248 | 0.873 | 293 | 0.861 | 338 | 0.130 | | | | |
| 24 | 0.136 | 69 | 0.885 | 114 | 0.848 | 159 | 0.126 | 204 | 0.136 | 249 | 0.885 | 294 | 0.848 | 339 | 0.126 | | | | |
| 25 | 0.138 | 70 | 0.897 | 115 | 0.835 | 160 | 0.123 | 205 | 0.138 | 250 | 0.897 | 295 | 0.835 | 340 | 0.123 | | | | |
| 26 | 0.143 | 71 | 0.906 | 116 | 0.819 | 161 | 0.122 | 206 | 0.143 | 251 | 0.906 | 296 | 0.819 | 341 | 0.122 | | | | |
| 27 | 0.148 | 72 | 0.915 | 117 | 0.803 | 162 | 0.121 | 207 | 0.148 | 252 | 0.915 | 297 | 0.803 | 342 | 0.121 | | | | |
| 28 | 0.154 | 73 | 0.924 | 118 | 0.787 | 163 | 0.119 | 208 | 0.154 | 253 | 0.924 | 298 | 0.787 | 343 | 0.119 | | | | |
| 29 | 0.160 | 74 | 0.933 | 119 | 0.770 | 164 | 0.115 | 209 | 0.160 | 254 | 0.933 | 299 | 0.770 | 344 | 0.115 | | | | |
| 30 | 0.167 | 75 | 0.941 | 120 | 0.753 | 165 | 0.112 | 210 | 0.167 | 255 | 0.941 | 300 | 0.753 | 345 | 0.112 | | | | |
| 31 | 0.176 | 76 | 0.948 | 121 | 0.734 | 166 | 0.108 | 211 | 0.176 | 256 | 0.948 | 301 | 0.734 | 346 | 0.108 | | | | |
| 32 | 0.187 | 77 | 0.954 | 122 | 0.714 | 167 | 0.105 | 212 | 0.187 | 257 | 0.954 | 302 | 0.714 | 347 | 0.105 | | | | |
| 33 | 0.199 | 78 | 0.960 | 123 | 0.694 | 168 | 0.100 | 213 | 0.199 | 258 | 0.960 | 303 | 0.694 | 348 | 0.100 | | | | |
| 34 | 0.212 | 79 | 0.967 | 124 | 0.674 | 169 | 0.095 | 214 | 0.212 | 259 | 0.967 | 304 | 0.674 | 349 | 0.095 | | | | |
| 35 | 0.226 | 80 | 0.973 | 125 | 0.653 | 170 | 0.089 | 215 | 0.226 | 260 | 0.973 | 305 | 0.653 | 350 | 0.089 | | | | |
| 36 | 0.242 | 81 | 0.977 | 126 | 0.631 | 171 | 0.084 | 216 | 0.242 | 261 | 0.977 | 306 | 0.631 | 351 | 0.084 | | | | |
| 37 | 0.259 | 82 | 0.982 | 127 | 0.609 | 172 | 0.078 | 217 | 0.259 | 262 | 0.982 | 307 | 0.609 | 352 | 0.078 | | | | |
| 38 | 0.276 | 83 | 0.986 | 128 | 0.587 | 173 | 0.072 | 218 | 0.276 | 263 | 0.986 | 308 | 0.587 | 353 | 0.072 | | | | |
| 39 | 0.295 | 84 | 0.990 | 129 | 0.564 | 174 | 0.065 | 219 | 0.295 | 264 | 0.990 | 309 | 0.564 | 354 | 0.065 | | | | |
| 40 | 0.314 | 85 | 0.995 | 130 | 0.541 | 175 | 0.058 | 220 | 0.314 | 265 | 0.995 | 310 | 0.541 | 355 | 0.058 | | | | |
| 41 | 0.336 | 86 | 0.996 | 131 | 0.518 | 176 | 0.049 | 221 | 0.336 | 266 | 0.996 | 311 | 0.518 | 356 | 0.049 | | | | |
| 42 | 0.358 | 87 | 0.997 | 132 | 0.495 | 177 | 0.040 | 222 | 0.358 | 267 | 0.997 | 312 | 0.495 | 357 | 0.040 | | | | |
| 43 | 0.381 | 88 | 0.998 | 133 | 0.472 | 178 | 0.030 | 223 | 0.381 | 268 | 0.998 | 313 | 0.472 | 358 | 0.030 | | | | |
| 44 | 0.403 | 89 | 0.999 | 134 | 0.449 | 179 | 0.020 | 224 | 0.403 | 269 | 0.999 | 314 | 0.449 | 359 | 0.020 | | | | |



SECTION III-D - DTV Engineering

Complete Questions 1-5 of the Certification Checklist and provide all data and information for the proposed facility, as requested in Technical Specifications, Items 1-13.

Certification Checklist: A correct answer of "Yes" to all of the questions below will ensure an expeditious grant of a construction permit. However, if the proposed facility is located within the Canadian or Mexican borders, coordination of the proposal under the appropriate treaties may be required prior to grant of the application. An answer of "No" will require additional evaluation of the applicable information in this form before a construction permit can be granted.

1. The proposed DTV facility complies with 47 C.F.R. Section 73.622 in the following respects:
 - (a) It will operate on the DTV channel for this station as established in 47 C.F.R. Section 73.622. Yes No
 - (b) It will operate from a transmitting antenna located within 5.0 km (3.1 miles) of the DTV reference site for this station as established in 47 C.F.R. Section 73.622. Yes No
 - (c) It will operate with an effective radiated power (ERP) and antenna height above average terrain (HAAT) that do not exceed the DTV reference ERP and HAAT for this station as established in 47 C.F.R. Section 73.622. Yes No
2. The proposed facility will not have a significant environmental impact, including exposure of workers or the general public to levels of RF radiation exceeding the applicable health and safety guidelines, and therefore will not come within 47 C.F.R. Section 1.1307. Yes No

Applicant must **submit the Exhibit** called for in Item 13.

3. Pursuant to 47 C.F.R. Section 73.625, the DTV coverage contour of the proposed facility will encompass the allotted principal community. Yes No
4. The requirements of 47 C.F.R. Section 73.1030 regarding notification to radio astronomy installations, radio receiving installations and FCC monitoring stations have either been satisfied or are not applicable. Yes No
5. The antenna structure to be used by this facility has been registered by the Commission and will not require reregistration to support the proposed antenna, OR the FAA has previously determined that the proposed structure will not adversely effect safety in air navigation and this structure qualifies for later registration under the Commission's phased registration plan, OR the proposed installation on this structure does not require notification to the FAA pursuant to 47 C.F.R. Section 17.7. Yes No

SECTION III-D DTV Engineering

TECHNICAL SPECIFICATIONS

Ensure that the specifications below are accurate. Contradicting data found elsewhere in this application will be disregarded. All items must be completed. The response "on file" is not acceptable.

TECH BOX

1. Channel Number: DTV _____ Analog TV, if any _____

2. Zone: I II III

3. Antenna Location Coordinates: (NAD 27)

____ ° ____ ' ____ " N S Latitude
____ ° ____ ' ____ " E W Longitude

4. Antenna Structure Registration Number: _____

Not applicable FAA Notification Filed with FAA

5. Antenna Location Site Elevation Above Mean Sea Level: _____ meters

6. Overall Tower Height Above Ground Level: _____ meters

7. Height of Radiation Center Above Ground Level: _____ meters

8. Height of Radiation Center Above Average Terrain: _____ meters

9. Maximum Effective Radiated Power (average power): _____ kW

10. Antenna Specifications:

| | |
|-----------------|-------|
| a. Manufacturer | Model |
|-----------------|-------|

b. Electrical Beam Tilt: _____ degrees Not Applicable

c. Mechanical Beam Tilt: _____ degrees toward azimuth _____ degrees True Not Applicable

Attach as an Exhibit all data specified in 47 C.F.R. Section 73.625(c).

Exhibit No. _____

d. Polarization: Horizontal Circular Elliptical

TECH BOXe. Directional Antenna Relative Field Values: Not applicable (Nondirectional)Rotation: _____^o No rotation

| Degree | Value | Degree | Value | Degree | Value | Degree | Value | Degree | Value | Degree | Value |
|---------------------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|
| 0 | | 60 | | 120 | | 180 | | 240 | | 300 | |
| 10 | | 70 | | 130 | | 190 | | 250 | | 310 | |
| 20 | | 80 | | 140 | | 200 | | 260 | | 320 | |
| 30 | | 90 | | 150 | | 210 | | 270 | | 330 | |
| 40 | | 100 | | 160 | | 220 | | 280 | | 340 | |
| 50 | | 110 | | 170 | | 230 | | 290 | | 350 | |
| Additional Azimuths | | | | | | | | | | | |

If a directional antenna is proposed, the requirements of 47 C.F.R. Section 73.625(c) must be satisfied. **Exhibit required.**

 Exhibit No.

11. Does the proposed facility satisfy the interference protection provisions of 47 C.F.R. Section 73.623(a)? (Applicable only if **Certification Checklist** Items 1(a), (b), or (c) are answered "No.") Yes No

If "No," attach as an Exhibit justification therefor, including a summary of any related previously granted waivers.

 Exhibit No.

12. If the proposed facility will not satisfy the coverage requirement of 47 C.F.R. Section 73.625, attach as an Exhibit justification therefor. (Applicable only if **Certification Checklist** Item 3 is answered "No.")

 Exhibit No.

13. **Environmental Protection Act. Submit in an Exhibit** the following:

 Exhibit No.

- a. If **Certification Checklist** Item 2 is answered "Yes," a brief explanation of why an Environmental Assessment is not required. Also describe in the Exhibit the steps that will be taken to limit RF radiation exposure to the public and to persons authorized access to the tower site.

By checking "Yes" to **Certification Checklist** Item 2, the applicant also certifies that it, in coordination with other users of the site, will reduce power or cease operation as necessary to protect persons having access to the site, tower or antenna from radiofrequency electromagnetic exposure in excess of FCC guidelines.

If **Certification Checklist** Item 2 is answered "No," an Environmental Assessment as required by 47 C.F.R. Section 1.1311.

PREPARER'S CERTIFICATION IN SECTION III MUST BE COMPLETED AND SIGNED.

I certify that the statements in this application are true, complete, and correct to the best of my knowledge and belief, and are made in good faith. I acknowledge that all certifications and attached Exhibits are considered material representations. I hereby waive any claim to the use of any particular frequency as against the regulatory power of the United States because of the previous use of the same, whether by license or otherwise, and request an authorization in accordance with this application. (See Section 304 of the Communications Act of 1934, as amended.)

| | |
|---|--|
| Typed or Printed Name of Person Signing | Typed or Printed Title of Person Signing |
| Signature | Date |

WILLFUL FALSE STATEMENTS ON THIS FORM ARE PUNISHABLE BY FINE AND/OR IMPRISONMENT
(U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION PERMIT
(U.S. CODE, TITLE 47, SECTION 312(a)(1)), AND/OR FORFEITURE (U.S. CODE, TITLE 47, SECTION 503).

SECTION III PREPARER'S CERTIFICATION

I certify that I have prepared Section III (Engineering Data) on behalf of the applicant, and that after such preparation, I have examined and found it to be accurate and true to the best of my knowledge and belief.

| | | |
|---|--|----------------|
| Name Martin R. Doczkat | Relationship to Applicant (e.g., Consulting Engineer) Consulting Engineer | |
| Signature  | Date March 29, 2005 | |
| Mailing Address Cohen, Dippell and Everist, P.C., 1300 L Street, NW, Suite 1100 | | |
| City Washington | State or Country (if foreign address) DC | ZIP Code 20005 |
| Telephone Number (include area code) (202) 898-0111 | E-Mail Address (if available) cde@attglobal.net | |

WILLFUL FALSE STATEMENTS ON THIS FORM ARE PUNISHABLE BY FINE AND/OR IMPRISONMENT
(U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION PERMIT
(U.S. CODE, TITLE 47, SECTION 312(a)(1)), AND/OR FORFEITURE (U.S. CODE, TITLE 47, SECTION 503).