

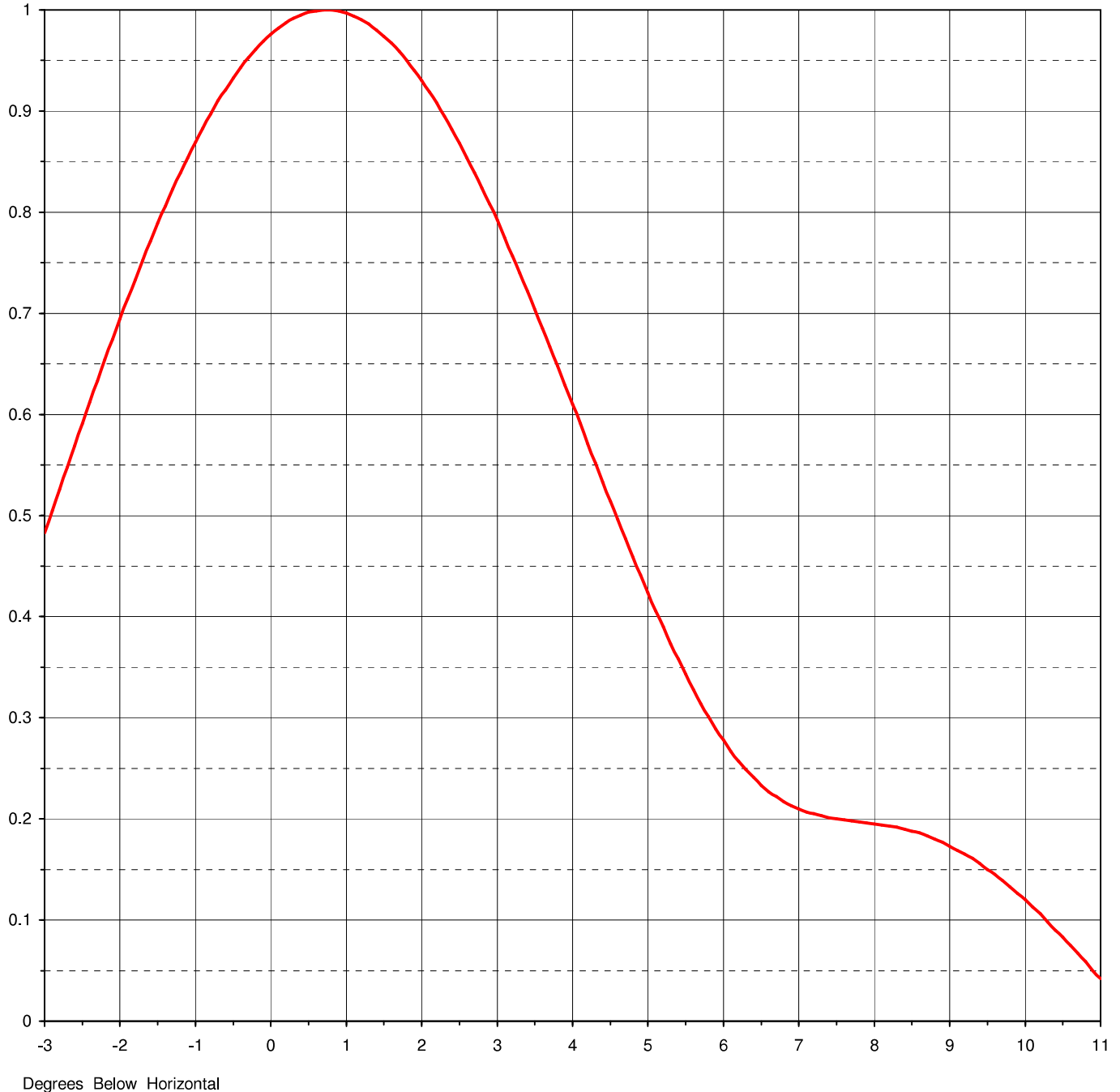


Proposal Number	<b>C-02505</b>	Revision:	<b>1</b>
Date	<b>10-Apr-08</b>		
Call Letters	<b>KEZI</b>	Channel	<b>9</b>
Location	<b>Eugene, OR</b>		
Customer	<b>Chambers Communications C</b>		
Antenna Type	<b>THV-10A9/VP-R C170</b>		

## ELEVATION PATTERN

RMS Gain at Main Lobe	<b>10.00 ( 10.00 dB )</b>
RMS Gain at Horizontal	<b>9.50 ( 9.78 dB )</b>
Calculated / Measured	<b>Calculated</b>

Beam Tilt	<b>0.75 deg</b>
Frequency	<b>189.00 MHz</b>
Drawing #	<b>10V100075</b>



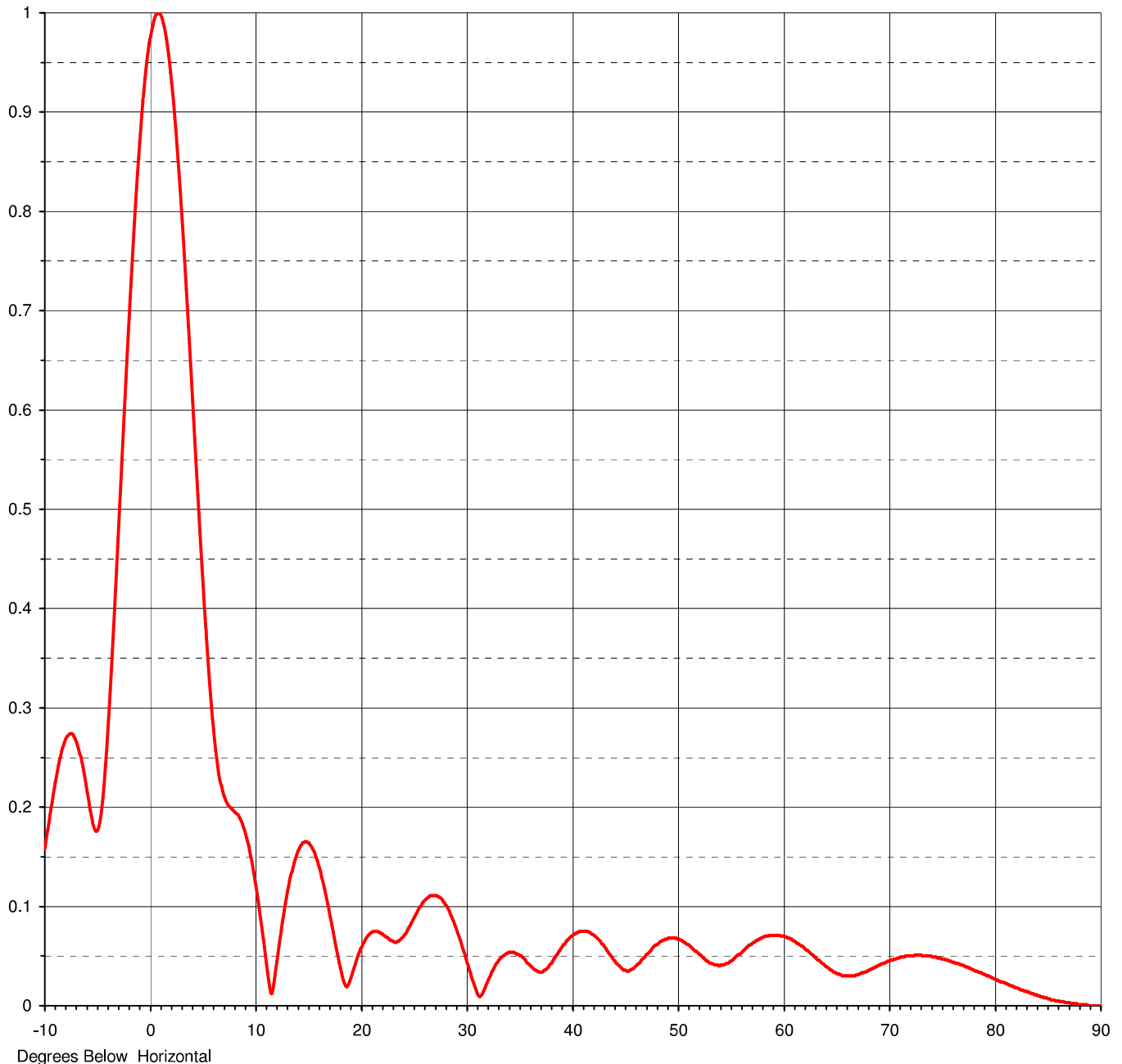


Proposal Number	<b>C-02505</b>	Revision:	<b>1</b>
Date	<b>10-Apr-08</b>		
Call Letters	<b>KEZI</b>	Channel	<b>9</b>
Location	<b>Eugene, OR</b>		
Customer	<b>Chambers Communications (</b>		
Antenna Type	<b>THV-10A9/VP-R C170</b>		

## ELEVATION PATTERN

RMS Gain at Main Lobe	<b>10.00 ( 10.00 dB )</b>
RMS Gain at Horizontal	<b>9.50 ( 9.78 dB )</b>
Calculated / Measured	<b>Calculated</b>

Beam Tilt	<b>0.75 deg</b>
Frequency	<b>189.00 MHz</b>
Drawing #	<b>10V100075-90</b>



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Proposal Number **C-02505** Revision: **1**  
 Date **10-Apr-08**  
 Call Letters **KEZI** Channel **9**  
 Location **Eugene, OR**  
 Customer **Chambers Communications Grou**  
 Antenna Type **THV-10A9/VP-R C170**

## TABULATION OF ELEVATION PATTERN

Elevation Pattern Drawing #: **10V100075-90**

Angle	Field	Angle	Field	Angle	Field	Angle	Field	Angle	Field	Angle	Field
-10.0	0.158	2.4	0.882	10.6	0.083	30.5	0.029	51.0	0.062	71.5	0.050
-9.5	0.192	2.6	0.854	10.8	0.067	31.0	0.014	51.5	0.057	72.0	0.050
-9.0	0.225	2.8	0.824	11.0	0.050	31.5	0.011	52.0	0.053	72.5	0.051
-8.5	0.251	3.0	0.792	11.5	0.013	32.0	0.023	52.5	0.048	73.0	0.051
-8.0	0.269	3.2	0.757	12.0	0.038	32.5	0.035	53.0	0.044	73.5	0.050
-7.5	0.274	3.4	0.722	12.5	0.075	33.0	0.044	53.5	0.041	74.0	0.049
-7.0	0.266	3.6	0.685	13.0	0.109	33.5	0.050	54.0	0.040	74.5	0.048
-6.5	0.245	3.8	0.648	13.5	0.135	34.0	0.054	54.5	0.042	75.0	0.047
-6.0	0.215	4.0	0.610	14.0	0.154	34.5	0.054	55.0	0.045	75.5	0.046
-5.5	0.185	4.2	0.571	14.5	0.164	35.0	0.051	55.5	0.049	76.0	0.044
-5.0	0.177	4.4	0.533	15.0	0.164	35.5	0.047	56.0	0.053	76.5	0.042
-4.5	0.210	4.6	0.496	15.5	0.157	36.0	0.041	56.5	0.058	77.0	0.040
-4.0	0.283	4.8	0.459	16.0	0.142	36.5	0.036	57.0	0.062	77.5	0.038
-3.5	0.378	5.0	0.424	16.5	0.122	37.0	0.034	57.5	0.066	78.0	0.036
-3.0	0.483	5.2	0.390	17.0	0.097	37.5	0.036	58.0	0.068	78.5	0.034
-2.8	0.526	5.4	0.358	17.5	0.069	38.0	0.042	58.5	0.070	79.0	0.031
-2.6	0.569	5.6	0.328	18.0	0.043	38.5	0.050	59.0	0.071	79.5	0.029
-2.4	0.612	5.8	0.301	18.5	0.022	39.0	0.058	59.5	0.071	80.0	0.027
-2.2	0.654	6.0	0.278	19.0	0.025	39.5	0.065	60.0	0.070	80.5	0.024
-2.0	0.694	6.2	0.257	19.5	0.041	40.0	0.070	60.5	0.068	81.0	0.022
-1.8	0.733	6.4	0.241	20.0	0.057	40.5	0.074	61.0	0.065	81.5	0.020
-1.6	0.771	6.6	0.227	20.5	0.068	41.0	0.075	61.5	0.062	82.0	0.018
-1.4	0.806	6.8	0.217	21.0	0.074	41.5	0.075	62.0	0.058	82.5	0.016
-1.2	0.839	7.0	0.210	21.5	0.075	42.0	0.072	62.5	0.054	83.0	0.014
-1.0	0.869	7.2	0.205	22.0	0.073	42.5	0.067	63.0	0.049	83.5	0.012
-0.8	0.897	7.4	0.201	22.5	0.069	43.0	0.061	63.5	0.045	84.0	0.010
-0.6	0.921	7.6	0.199	23.0	0.065	43.5	0.053	64.0	0.040	84.5	0.009
-0.4	0.943	7.8	0.197	23.5	0.065	44.0	0.046	64.5	0.036	85.0	0.007
-0.2	0.961	8.0	0.195	24.0	0.069	44.5	0.040	65.0	0.032	85.5	0.006
0.0	0.976	8.2	0.193	24.5	0.077	45.0	0.036	65.5	0.030	86.0	0.005
0.2	0.987	8.4	0.190	25.0	0.087	45.5	0.036	66.0	0.030	86.5	0.004
0.4	0.995	8.6	0.186	25.5	0.097	46.0	0.039	66.5	0.030	87.0	0.003
0.6	0.999	8.8	0.180	26.0	0.105	46.5	0.044	67.0	0.031	87.5	0.002
0.8	1.000	9.0	0.173	26.5	0.110	47.0	0.051	67.5	0.033	88.0	0.001
1.0	0.997	9.2	0.165	27.0	0.111	47.5	0.056	68.0	0.036	88.5	0.001
1.2	0.990	9.4	0.156	27.5	0.109	48.0	0.061	68.5	0.038	89.0	0.000
1.4	0.980	9.6	0.145	28.0	0.102	48.5	0.065	69.0	0.041	89.5	0.000
1.6	0.967	9.8	0.139	28.5	0.092	49.0	0.067	69.5	0.043	90.0	0.000
1.8	0.950	10.0	0.126	29.0	0.079	49.5	0.068	70.0	0.045		
2.0	0.930	10.2	0.113	29.5	0.064	50.0	0.067	70.5	0.047		
2.2	0.908	10.4	0.098	30.0	0.047	50.5	0.065	71.0	0.049		

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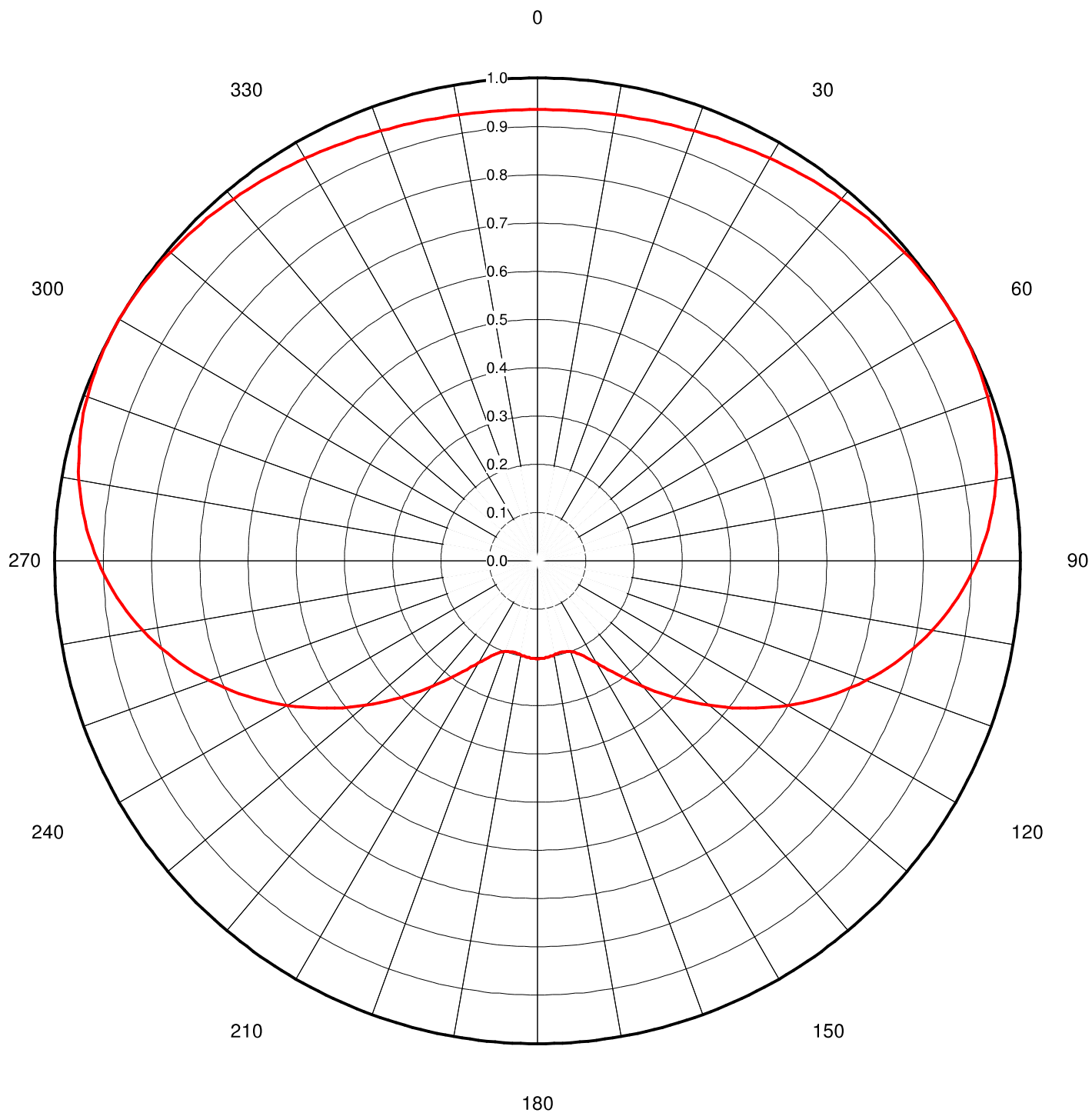


Proposal Number	<b>C-02505</b>	Revision:	<b>1</b>
Date	<b>10-Apr-08</b>		
Call Letters	<b>KEZI</b>	Channel	<b>9</b>
Location	<b>Eugene, OR</b>		
Customer	<b>Chambers Communications Gro</b>		
Antenna Type	<b>THV-10A9/VP-R C170</b>		

## AZIMUTH PATTERN

Gain **1.70** **(2.30 dB)**  
Calculated / Measured **Calculated**

Frequency **189.00 MHz**  
Drawing # **THV\_C170HP**





Proposal Number **C-02505** Revision: **1**  
Date **10-Apr-08**  
Call Letters **KEZI** Channel **9**  
Location **Eugene, OR**  
Customer **Chambers Communications Group**  
Antenna Type **THV-10A9/VP-R C170**

## TABULATION OF AZIMUTH PATTERN

Azimuth Pattern Drawing #: **THV\_C170HP**

Angle	Field	Angle	Field	Angle	Field	Angle	Field	Angle	Field	Angle	Field	Angle	Field	Angle	Field
0	0.934	45	0.987	90	0.911	135	0.400	180	0.203	225	0.400	270	0.911	315	0.987
1	0.934	46	0.988	91	0.904	136	0.388	181	0.202	226	0.413	271	0.917	316	0.985
2	0.934	47	0.990	92	0.897	137	0.375	182	0.202	227	0.426	272	0.924	317	0.984
3	0.935	48	0.991	93	0.889	138	0.363	183	0.202	228	0.439	273	0.929	318	0.982
4	0.935	49	0.992	94	0.882	139	0.351	184	0.202	229	0.452	274	0.935	319	0.981
5	0.935	50	0.993	95	0.874	140	0.340	185	0.201	230	0.465	275	0.941	320	0.979
6	0.936	51	0.994	96	0.866	141	0.328	186	0.201	231	0.478	276	0.946	321	0.977
7	0.936	52	0.996	97	0.857	142	0.317	187	0.200	232	0.492	277	0.951	322	0.976
8	0.937	53	0.996	98	0.848	143	0.307	188	0.199	233	0.505	278	0.956	323	0.974
9	0.937	54	0.997	99	0.839	144	0.296	189	0.198	234	0.519	279	0.960	324	0.972
10	0.938	55	0.998	100	0.830	145	0.287	190	0.198	235	0.532	280	0.964	325	0.971
11	0.939	56	0.999	101	0.820	146	0.277	191	0.197	236	0.545	281	0.968	326	0.969
12	0.939	57	0.999	102	0.811	147	0.268	192	0.197	237	0.559	282	0.972	327	0.967
13	0.940	58	1.000	103	0.801	148	0.259	193	0.196	238	0.572	283	0.975	328	0.966
14	0.941	59	1.000	104	0.791	149	0.252	194	0.196	239	0.585	284	0.978	329	0.964
15	0.942	60	1.000	105	0.780	150	0.244	195	0.196	240	0.599	285	0.981	330	0.962
16	0.943	61	1.000	106	0.769	151	0.237	196	0.196	241	0.612	286	0.984	331	0.961
17	0.944	62	1.000	107	0.758	152	0.231	197	0.196	242	0.625	287	0.986	332	0.959
18	0.945	63	0.999	108	0.747	153	0.225	198	0.197	243	0.638	288	0.989	333	0.957
19	0.946	64	0.999	109	0.736	154	0.220	199	0.198	244	0.650	289	0.990	334	0.956
20	0.948	65	0.998	110	0.724	155	0.215	200	0.200	245	0.663	290	0.992	335	0.954
21	0.949	66	0.998	111	0.712	156	0.211	201	0.202	246	0.676	291	0.994	336	0.953
22	0.950	67	0.996	112	0.700	157	0.207	202	0.204	247	0.688	292	0.995	337	0.952
23	0.952	68	0.995	113	0.688	158	0.204	203	0.207	248	0.700	293	0.996	338	0.950
24	0.953	69	0.994	114	0.676	159	0.202	204	0.211	249	0.712	294	0.998	339	0.949
25	0.954	70	0.992	115	0.663	160	0.200	205	0.215	250	0.724	295	0.998	340	0.948
26	0.956	71	0.990	116	0.651	161	0.198	206	0.220	251	0.735	296	0.999	341	0.946
27	0.957	72	0.989	117	0.638	162	0.197	207	0.225	252	0.747	297	0.999	342	0.945
28	0.959	73	0.986	118	0.625	163	0.196	208	0.231	253	0.758	298	1.000	343	0.944
29	0.961	74	0.984	119	0.612	164	0.196	209	0.237	254	0.769	299	1.000	344	0.943
30	0.962	75	0.981	120	0.599	165	0.196	210	0.244	255	0.780	300	1.000	345	0.942
31	0.964	76	0.978	121	0.585	166	0.196	211	0.252	256	0.790	301	1.000	346	0.941
32	0.966	77	0.975	122	0.572	167	0.196	212	0.259	257	0.801	302	1.000	347	0.940
33	0.967	78	0.972	123	0.559	168	0.197	213	0.268	258	0.811	303	0.999	348	0.939
34	0.969	79	0.968	124	0.546	169	0.197	214	0.277	259	0.820	304	0.999	349	0.939
35	0.971	80	0.964	125	0.532	170	0.198	215	0.287	260	0.830	305	0.998	350	0.938
36	0.972	81	0.960	126	0.519	171	0.198	216	0.296	261	0.839	306	0.997	351	0.937
37	0.974	82	0.956	127	0.505	172	0.199	217	0.307	262	0.848	307	0.996	352	0.937
38	0.976	83	0.951	128	0.492	173	0.200	218	0.317	263	0.857	308	0.995	353	0.936
39	0.977	84	0.946	129	0.479	174	0.201	219	0.328	264	0.866	309	0.994	354	0.936
40	0.979	85	0.941	130	0.465	175	0.201	220	0.340	265	0.874	310	0.993	355	0.935
41	0.981	86	0.935	131	0.452	176	0.202	221	0.351	266	0.882	311	0.992	356	0.935
42	0.982	87	0.930	132	0.439	177	0.202	222	0.363	267	0.889	312	0.991	357	0.935
43	0.984	88	0.924	133	0.426	178	0.202	223	0.375	268	0.897	313	0.990	358	0.934
44	0.985	89	0.917	134	0.413	179	0.202	224	0.388	269	0.904	314	0.988	359	0.934

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