

S.O. 27957

Report of Test 6014-6/2-DA

for

First Broadcasting Capital Partners, LLC

KMCQ 104.5 MHz Covington, WA

OBJECTIVE:

The objective of this test was to demonstrate the directional characteristics of a 6014-6/2-DA to meet the needs of KMCQ and to comply with the requirements of the FCC construction permit, file number BMPH-20090929ALM.

RESULTS:

The following Figures are the results of the measurements from our pattern range:

Figure 1A - Measured Azimuth Pattern with the FCC Composite

Figure 1B - Measured Composite Azimuth Pattern with the FCC Composite

Figure 1C - Tabulation of the Horizontal Polarization for the Measured Azimuth Pattern

Figure 1D - Tabulation of the Vertical Polarization for the Measured Azimuth Pattern

Figure 1E - Tabulation of the Measured Composite Azimuth Pattern

Figure 1F - Tabulation of the FCC Composite

The calculated elevation pattern of the antenna is shown in Figure 3.

Construction permit file number BMPH-20090929ALM indicates that the Horizontal radiation component shall not exceed 7.100 kW at any azimuth and is restricted to the following values at the azimuths specified:

80 - 110 Degrees T: 0.444 kW



APPENDIX B - ANTENNA MANUFACTURER

This 6 bay panel antenna was originally built in 2000.

Use by KMCQ of a directional antenna is voluntary - **Not a Section 73.215.**

Operation by KMCQ required no outside construction.

From Figure 1A, the maximum radiation of the Horizontal component occurs at 208 Degrees T to 221 Degrees T, and at 338 Degrees T to 356 Degrees T. At the restricted azimuth of 80 - 110 Degrees T the Horizontal component is 13.51 dB down from the maximum of 7.100 kW, or 0.316 kW. The Vertical component does not exceed the horizontal component and therefore complies with the construction permit.

The R.M.S. of the Horizontal component is 0.729. The total Horizontal power gain is 6.073. The R.M.S. of the Vertical component is 0.698. The total Vertical power gain is 5.952. See Figure 4 for calculations. The R.M.S. of the FCC composite pattern is 0.810. The R.M.S. of the measured composite pattern is 0.730. Eighty-five percent (85%) of the original authorized FCC composite pattern is 0.688. Therefore this pattern complies with the FCC requirement of 73.316(c)(2)(ix)(A).

METHOD OF DIRECTIONALIZATION:

One bay of the 6014-6/2-DA was mounted on a tower of precise scale to the tower at the KMCQ site. The spacing and alignment of the antenna to the tower was varied to achieve the horizontal and vertical patterns shown in Figure 1A. See Figure 2 for mechanical details.

METHOD OF MEASUREMENT:

As allowed by the construction permit, file number BMPH-20090929ALM, a single level of the 6014-6/2-DA was set up on the Howell Laboratories scale model antenna pattern measuring range. A scale of 4.5:1 was used.

SUPERVISION:

Mr. Surette was graduated from Lowell Technological Institute, Lowell, Massachusetts in 1973 with the degree of Bachelor of Science in Electrical Engineering. He has been directly involved with design and development of broadcast antennas, filter systems and RF transmission components since 1974, as an RF Engineer for six years with the original Shively Labs in Raymond, ME and for a short period of time with Dielectric Communications. He is currently an Associate Member of the AFCCE and a Senior Member of IEEE. He has authored a chapter on filters and combining systems for the latest edition of the CRC Electronics Handbook and for the 9th and 10th Editions of the NAB Handbook.

EQUIPMENT:

The scale model pattern range consists of a wooden rotating pedestal equipped with a position indicator. The scale model bay is placed on the top of this pedestal and is used in the transmission mode at approximately 20 feet above ground level. The receiving corner reflector is spaced 50 feet away from the rotating pedestal at the same level above ground as the transmitting model. The transmitting and receiving signals are carried to a control building by means of RG-9/U double shielded coax cable.

The control building is equipped with:

Hewlett Packard Model 8753 Network Analyzer

PC Based Controller

Hewlett Packard 7550A Graphics Plotter

The test equipment is calibrated to ANSI/NCSL Z540-1-1994.

TEST PROCEDURES:

The corner reflector is mounted so that the horizontal and vertical azimuth patterns are measured independently by rotating the corner reflector by 90 degrees. The network analyzer was set to 470.25 MHz. Calibrated pads are used to check the linearity of the measuring system. For example, 6 dB padding yields a scale reading of 50 from an unpadded reading of 100 in voltage. From the recorded patterns, the R.M.S. values are calculated and recorded as shown in Figure 1A.

Respectfully submitted by:

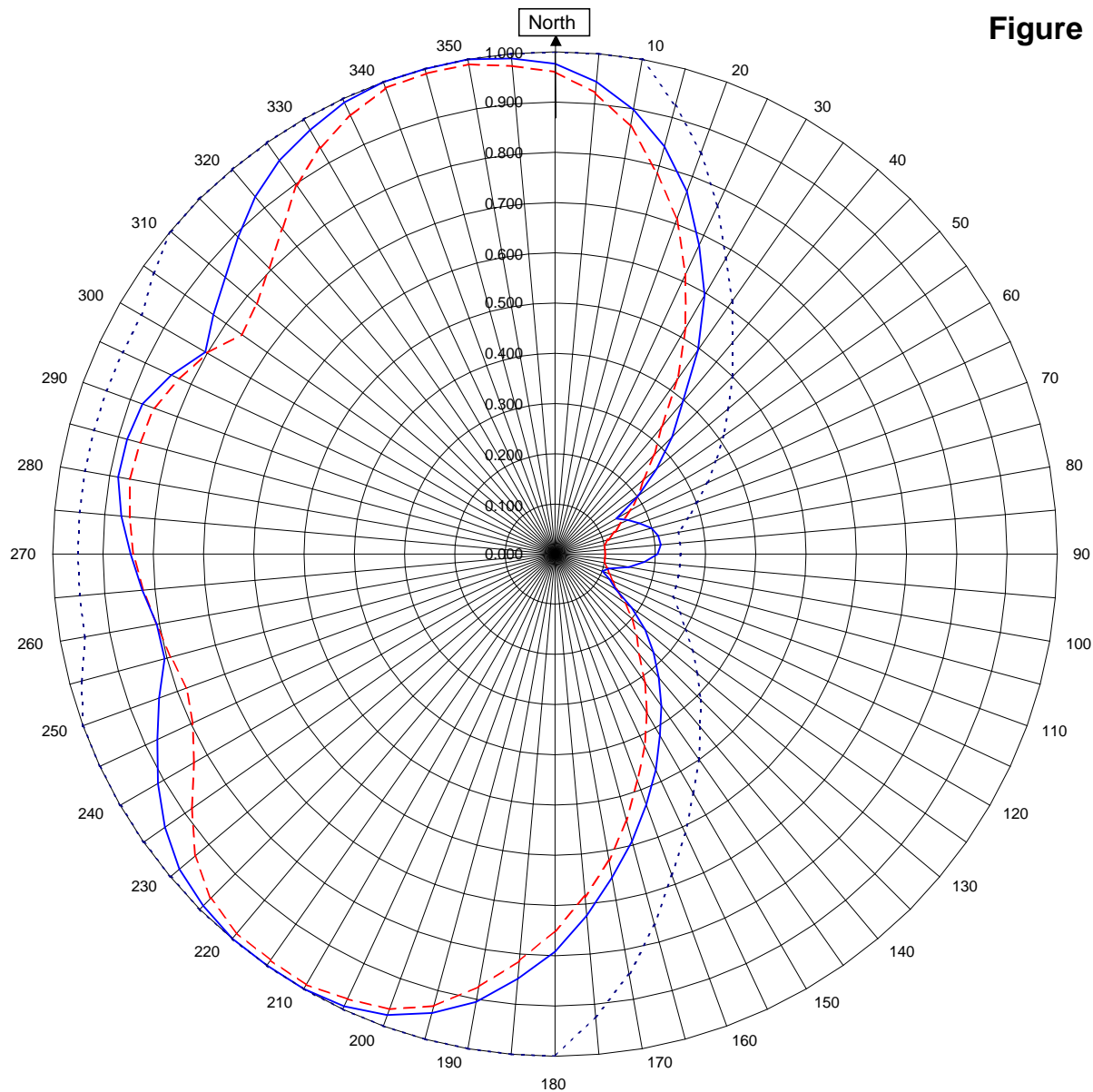


Robert A. Surette
Director of Sales Engineering
S/O 27957
Date January 12, 2010

Shively Labs

Shively Labs, a division of Howell Laboratories, Inc. Bridgton, ME (207)647-3327

Figure 1a



KMCQ Covington, WA

27957
January 12, 2010

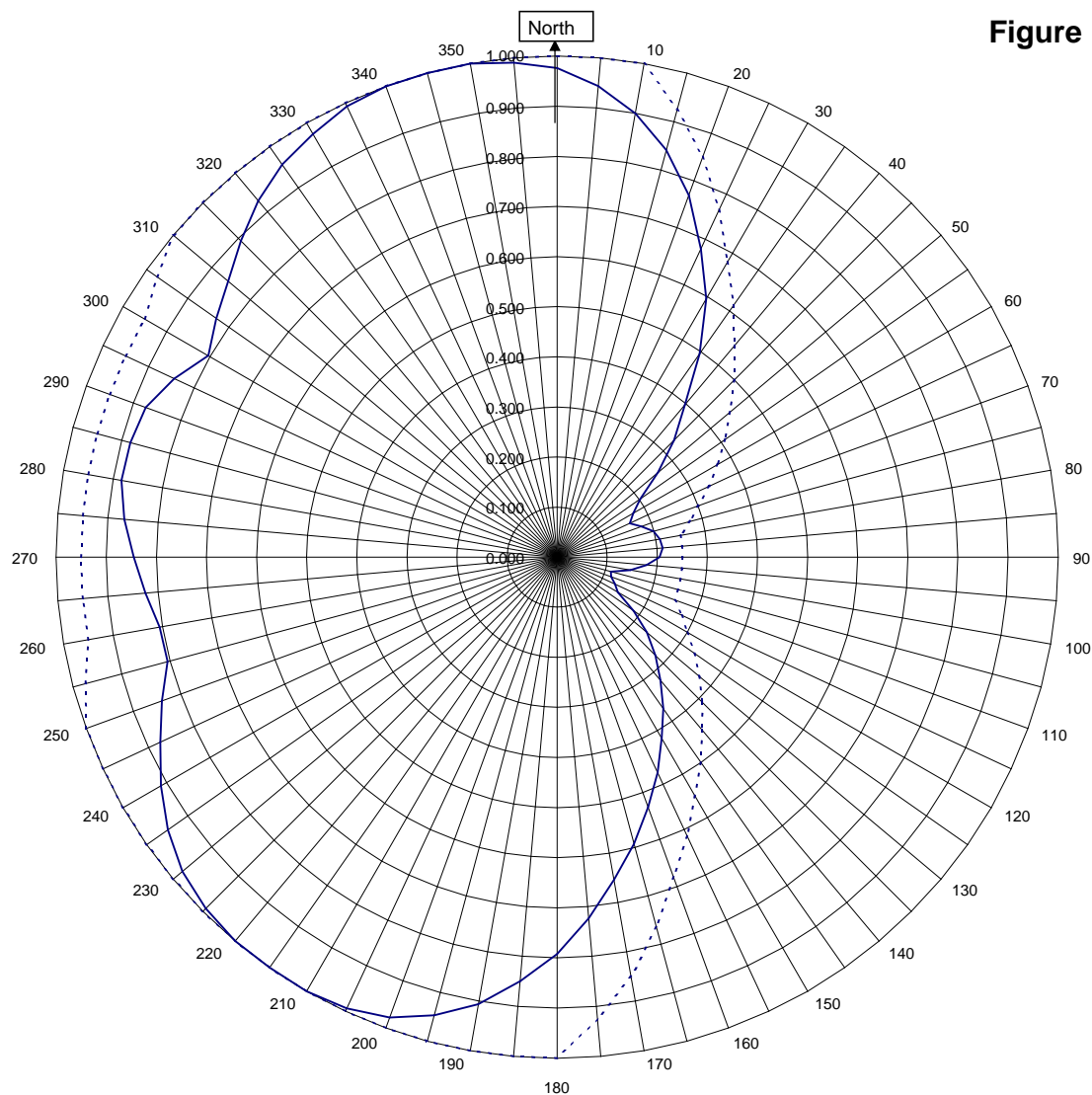
| | | | |
|-------------------|-------|-------------------------------------|--------------------|
| Horizontal RMS | 0.729 | Frequency | 104.5 / 470.25 MHz |
| Vertical RMS | 0.698 | Plot | Relative Field |
| H/V Composite RMS | 0.730 | Scale | 4.5 : 1 |
| FCC Composite RMS | 0.810 | See Figure 2 for Mechanical Details | |

| | |
|---------------|---------------------|
| Antenna Model | Model 6014-6/2-DA |
| Pattern Type | Directional Azimuth |

Shively Labs

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Figure 1b



KMCQ Covington, WA

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January 12, 2010

| | |
|------------------------|-------|
| —————H/VComposite RMS | 0.730 |
|FCC Composite RMS | 0.810 |

| | |
|-------------------------------------|--------------------|
| Frequency | 104.5 / 470.25 MHz |
| Plot | Relative Field |
| Scale | 4.5 : 1 |
| See Figure 2 for Mechanical Details | |

| | |
|---------------|---------------------------|
| Antenna Model | Model 6014-6/2-DA |
| Pattern Type | Directional H/V Composite |

Figure 1c

Tabulation of Horizontal Azimuth Pattern
KMCQ Covington, WA

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0 | 0.976 | 180 | 0.792 |
| 10 | 0.899 | 190 | 0.906 |
| 20 | 0.768 | 200 | 0.977 |
| 30 | 0.595 | 210 | 1.000 |
| 40 | 0.396 | 220 | 1.000 |
| 45 | 0.330 | 225 | 0.991 |
| 50 | 0.263 | 230 | 0.976 |
| 60 | 0.141 | 240 | 0.913 |
| 70 | 0.179 | 250 | 0.839 |
| 80 | 0.208 | 260 | 0.805 |
| 90 | 0.204 | 270 | 0.845 |
| 100 | 0.149 | 280 | 0.883 |
| 110 | 0.100 | 290 | 0.874 |
| 120 | 0.139 | 300 | 0.804 |
| 130 | 0.234 | 310 | 0.857 |
| 135 | 0.278 | 315 | 0.893 |
| 140 | 0.321 | 320 | 0.928 |
| 150 | 0.417 | 330 | 0.975 |
| 160 | 0.531 | 340 | 1.000 |
| 170 | 0.654 | 350 | 1.000 |

Figure 1d

Tabulation of Vertical Azimuth Pattern
KMCQ Covington, WA

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0 | 0.960 | 180 | 0.750 |
| 10 | 0.865 | 190 | 0.875 |
| 20 | 0.710 | 200 | 0.965 |
| 30 | 0.520 | 210 | 0.990 |
| 40 | 0.330 | 220 | 0.985 |
| 45 | 0.280 | 225 | 0.970 |
| 50 | 0.230 | 230 | 0.935 |
| 60 | 0.175 | 240 | 0.830 |
| 70 | 0.126 | 250 | 0.780 |
| 80 | 0.100 | 260 | 0.805 |
| 90 | 0.100 | 270 | 0.840 |
| 100 | 0.100 | 280 | 0.860 |
| 110 | 0.115 | 290 | 0.850 |
| 120 | 0.140 | 300 | 0.800 |
| 130 | 0.200 | 310 | 0.775 |
| 135 | 0.230 | 315 | 0.805 |
| 140 | 0.260 | 320 | 0.845 |
| 150 | 0.365 | 330 | 0.935 |
| 160 | 0.480 | 340 | 0.987 |
| 170 | 0.620 | 350 | 0.990 |

Figure 1e

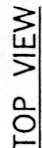
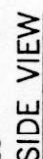
Tabulation of Composite Azimuth Pattern
KMCQ Covington, WA

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0 | 0.976 | 180 | 0.792 |
| 10 | 0.899 | 190 | 0.906 |
| 20 | 0.768 | 200 | 0.977 |
| 30 | 0.595 | 210 | 1.000 |
| 40 | 0.396 | 220 | 1.000 |
| 45 | 0.330 | 225 | 0.991 |
| 50 | 0.263 | 230 | 0.976 |
| 60 | 0.175 | 240 | 0.913 |
| 70 | 0.179 | 250 | 0.839 |
| 80 | 0.208 | 260 | 0.805 |
| 90 | 0.204 | 270 | 0.845 |
| 100 | 0.149 | 280 | 0.883 |
| 110 | 0.115 | 290 | 0.874 |
| 120 | 0.140 | 300 | 0.804 |
| 130 | 0.234 | 310 | 0.857 |
| 135 | 0.278 | 315 | 0.893 |
| 140 | 0.321 | 320 | 0.928 |
| 150 | 0.417 | 330 | 0.975 |
| 160 | 0.531 | 340 | 1.000 |
| 170 | 0.654 | 350 | 1.000 |

Figure 1f

Tabulation of FCC Directional Composite
KMCQ Covington, WA

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0 | 1.000 | 180 | 1.000 |
| 10 | 1.000 | 190 | 1.000 |
| 20 | 0.850 | 200 | 1.000 |
| 30 | 0.680 | 210 | 1.000 |
| 40 | 0.550 | 220 | 1.000 |
| 50 | 0.450 | 230 | 1.000 |
| 60 | 0.370 | 240 | 1.000 |
| 70 | 0.300 | 250 | 1.000 |
| 80 | 0.250 | 260 | 0.950 |
| 90 | 0.250 | 270 | 0.950 |
| 100 | 0.250 | 280 | 0.950 |
| 110 | 0.250 | 290 | 0.950 |
| 120 | 0.300 | 300 | 0.950 |
| 130 | 0.370 | 310 | 1.000 |
| 140 | 0.450 | 320 | 1.000 |
| 150 | 0.550 | 330 | 1.000 |
| 160 | 0.680 | 340 | 1.000 |
| 170 | 0.850 | 350 | 1.000 |



DATE: 9-29-99

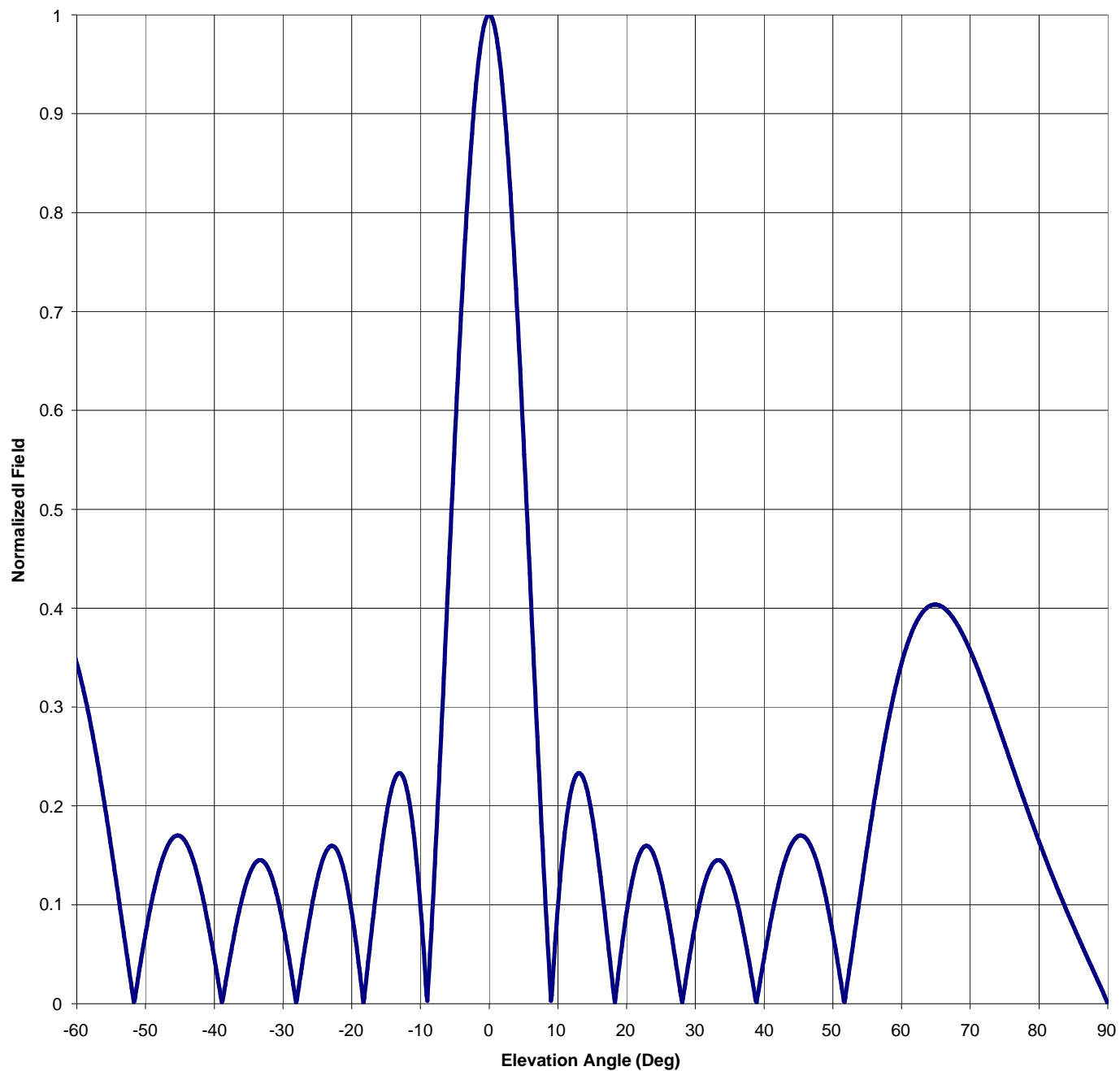
FIGURE 2

TOWER BY: VALMONT-MICROFLECT
MODEL: 300 FT. SELF-SUPPORTING

Antenna Mfg.: Shively Labs
Antenna Type: Model 6014-6/2-DA
Station: KMCQ
Frequency: 104.5
Channel #: 283
Figure: FIGURE 3

Date: 1/12/2010

| | | |
|----------------|-------|----------|
| Beam Til | 0 | |
| Gain (Max) | 6.073 | 7.834 dB |
| Gain (Horizon) | 6.073 | 7.834 dB |



Antenna Mfg.: Shively Labs
Antenna Type: Model 6014-6/2-DA

Date: 1/12/2010

Station: KMCQ

Beam Tilt 0

Frequency: 104.5

Gain (Max) 6.073 7.834 dB

Channel #: 283

Gain (Horizon) 6.073 7.834 dB

Figure: FIGURE 3

| Angle of Depression (Deg) | Relative Field | Angle of Depression (Deg) | Relative Field | Angle of Depression (Deg) | Relative Field | Angle of Depression (Deg) | Relative Field |
|---------------------------|----------------|---------------------------|----------------|---------------------------|----------------|---------------------------|----------------|
| -90 | 0.000 | -44 | 0.162 | 0 | 1.000 | 46 | 0.168 |
| -89 | 0.016 | -43 | 0.144 | 1 | 0.980 | 47 | 0.156 |
| -88 | 0.032 | -42 | 0.118 | 2 | 0.922 | 48 | 0.136 |
| -87 | 0.047 | -41 | 0.085 | 3 | 0.830 | 49 | 0.107 |
| -86 | 0.063 | -40 | 0.046 | 4 | 0.710 | 50 | 0.071 |
| -85 | 0.078 | -39 | 0.006 | 5 | 0.570 | 51 | 0.029 |
| -84 | 0.094 | -38 | 0.035 | 6 | 0.420 | 52 | 0.016 |
| -83 | 0.111 | -37 | 0.073 | 7 | 0.270 | 53 | 0.063 |
| -82 | 0.128 | -36 | 0.105 | 8 | 0.128 | 54 | 0.111 |
| -81 | 0.146 | -35 | 0.129 | 9 | 0.003 | 55 | 0.158 |
| -80 | 0.164 | -34 | 0.143 | 10 | 0.099 | 56 | 0.203 |
| -79 | 0.183 | -33 | 0.145 | 11 | 0.173 | 57 | 0.245 |
| -78 | 0.202 | -32 | 0.135 | 12 | 0.218 | 58 | 0.283 |
| -77 | 0.222 | -31 | 0.113 | 13 | 0.233 | 59 | 0.316 |
| -76 | 0.242 | -30 | 0.081 | 14 | 0.222 | 60 | 0.344 |
| -75 | 0.262 | -29 | 0.041 | 15 | 0.189 | 61 | 0.367 |
| -74 | 0.283 | -28 | 0.003 | 16 | 0.139 | 62 | 0.384 |
| -73 | 0.303 | -27 | 0.049 | 17 | 0.080 | 63 | 0.395 |
| -72 | 0.322 | -26 | 0.091 | 18 | 0.017 | 64 | 0.402 |
| -71 | 0.340 | -25 | 0.126 | 19 | 0.042 | 65 | 0.404 |
| -70 | 0.357 | -24 | 0.150 | 20 | 0.093 | 66 | 0.401 |
| -69 | 0.372 | -23 | 0.159 | 21 | 0.131 | 67 | 0.394 |
| -68 | 0.385 | -22 | 0.153 | 22 | 0.153 | 68 | 0.385 |
| -67 | 0.394 | -21 | 0.131 | 23 | 0.159 | 69 | 0.372 |
| -66 | 0.401 | -20 | 0.093 | 24 | 0.150 | 70 | 0.357 |
| -65 | 0.404 | -19 | 0.042 | 25 | 0.126 | 71 | 0.340 |
| -64 | 0.402 | -18 | 0.017 | 26 | 0.091 | 72 | 0.322 |
| -63 | 0.395 | -17 | 0.080 | 27 | 0.049 | 73 | 0.303 |
| -62 | 0.384 | -16 | 0.139 | 28 | 0.003 | 74 | 0.283 |
| -61 | 0.367 | -15 | 0.189 | 29 | 0.041 | 75 | 0.262 |
| -60 | 0.344 | -14 | 0.222 | 30 | 0.081 | 76 | 0.242 |
| -59 | 0.316 | -13 | 0.233 | 31 | 0.113 | 77 | 0.222 |
| -58 | 0.283 | -12 | 0.218 | 32 | 0.135 | 78 | 0.202 |
| -57 | 0.245 | -11 | 0.173 | 33 | 0.145 | 79 | 0.183 |
| -56 | 0.203 | -10 | 0.099 | 34 | 0.143 | 80 | 0.164 |
| -55 | 0.158 | -9 | 0.003 | 35 | 0.129 | 81 | 0.146 |
| -54 | 0.111 | -8 | 0.128 | 36 | 0.105 | 82 | 0.128 |
| -53 | 0.063 | -7 | 0.270 | 37 | 0.073 | 83 | 0.111 |
| -52 | 0.016 | -6 | 0.420 | 38 | 0.035 | 84 | 0.094 |
| -51 | 0.029 | -5 | 0.570 | 39 | 0.006 | 85 | 0.078 |
| -50 | 0.071 | -4 | 0.710 | 40 | 0.046 | 86 | 0.063 |
| -49 | 0.107 | -3 | 0.830 | 41 | 0.085 | 87 | 0.047 |
| -48 | 0.136 | -2 | 0.922 | 42 | 0.118 | 88 | 0.032 |
| -47 | 0.156 | -1 | 0.980 | 43 | 0.144 | 89 | 0.016 |
| -46 | 0.168 | 0 | 1.000 | 44 | 0.162 | 90 | 0.000 |
| -45 | 0.170 | | | 45 | 0.170 | | |

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Figure 4

VALIDATION OF TOTAL POWER GAIN CALCULATION

KMCQ Covington, WA

Model 6014-6/2-DA

Elevation Gain of Antenna

3.090

Horizontal RMS value divided by the Vertical RMS value equals the Horiz. - Vert. Ratio

| | | | | | |
|-------|-------|-------|-------|-----------|-------|
| H RMS | 0.729 | V RMS | 0.698 | H/V Ratio | 1.044 |
|-------|-------|-------|-------|-----------|-------|

| | |
|--|-------|
| Elevation Gain of Horizontal Component | 3.227 |
|--|-------|

| | |
|--------------------------------------|-------|
| Elevation Gain of Vertical Component | 2.959 |
|--------------------------------------|-------|

| | |
|---|-------|
| Horizontal Azimuth Gain equals $1/(\text{RMS})^2$. | 1.882 |
|---|-------|

| | |
|---|-------|
| Vertical Azimuth Gain equals $1/(\text{RMS}/\text{Max Vert})^2$. | 2.012 |
| Max. Vertical | 0.99 |

***Total Horizontal Power Gain is the Elevation Gain Times the Azimuth Gain**

Total Horizontal Power Gain = 6.073

***Total Vertical Power Gain is the Elevation Gain Times the Azimuth Gain**

Total Vertical Power Gain = 5.952

=====

ERP divided by Horizontal Power Gain equals Antenna Input Power

| | | | | | | |
|-----|--------|-------------------|-------|--------|------|--------------------------|
| 7.1 | kW ERP | Divided by H Gain | 6.073 | equals | 1.17 | kW H Antenna Input Power |
|-----|--------|-------------------|-------|--------|------|--------------------------|

Antenna Input Power times Vertical Power Gain equals Vertical ERP

| | | | | | | |
|------|----|--------------|-------|--------|------|----------|
| 1.17 | kW | Times V Gain | 5.952 | equals | 6.96 | kW V ERP |
|------|----|--------------|-------|--------|------|----------|

Maximum Value of the Vertical Component squared times the Maximum ERP equals the Vertical ERP

| | | | | | |
|------------|-------|------|--------|------|-----------------|
| $(0.99)^2$ | Times | 7.10 | Equals | 6.96 | kW Vertical ERP |
|------------|-------|------|--------|------|-----------------|

NOTE: Calculating the ERP of the Vertical Component by two methods validates the total power gain calculations