

BERNARD R. SEGAL, P. E.
CONSULTING ENGINEER
KENSINGTON, MARYLAND

ENGINEERING EXHIBIT
AMENDED APPLICATION FOR
MODIFICATION OF CONSTRUCTION PERMIT
GOLDEN ORANGE BROADCASTING CO., INC.
STATION KDOC-DT, ANAHEIM, CALIFORNIA
CH.32 1000 KW (MAX-DA) 938 METERS

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BERNARD R. SEGAL, P. E.
CONSULTING ENGINEER
KENSINGTON, MARYLAND

ENGINEERING EXHIBIT
AMENDED APPLICATION FOR
MODIFICATION OF DTV CONSTRUCTION PERMIT
GOLDEN ORANGE BROADCASTING CO., INC.
STATION KDOC-DT, ANAHEIM, CALIFORNIA
CH.32 1000 KW (MAX-DA) 938 METERS

ENGINEERING STATEMENT

The instant Engineering Exhibit has been prepared on behalf of Golden Orange Broadcasting Co., Inc., the permittee in BPCDT-19981028KE for a digital television (DTV) facility for KDOC-DT, Anaheim, California. The construction permit is for operation on Channel 32 with maximum effective radiated power of 200 kW and antenna radiation center height of 960 meters above average terrain. A maximization application, File Number BMPCDT-20000427ABH, is pending which seeks continued operation for KDOC-DT on Channel 32 with the maximum average effective radiated power increased to 1000 kW and the height above average terrain changed to 957 meters.

The applicant has been advised informally by the FCC staff that the appropriate Mexican authority has objected to the KDOC-DT modification proposal on the ground that the proposal violates the separation requirement of the Memorandum of Understanding with respect to the Tijuana, BC, Channel 32, allotment, and so would create interference to the allotment. The instant amendment proposes a new directional pattern which does not increase radiation over the arc of interest to the Tijuana allotment above the levels already sanctioned in the outstanding construction permit. The Appendix to this Engineering Exhibit is devoted entirely to the Mexican, Tijuana, Channel 32, protection issue, and has been formatted so that it may be used as a self-contained presentation for Mexican notification purposes, if desired.

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The site specified herein is the same as specified in the pending application. However, the coordinates have been corrected and a new antenna structure registration (ASR) number has been issued. The corrected site geographic coordinates are: 34° 13' 35" north latitude; 118° 03' 58" west longitude. These coordinates are NAD 27, and were derived by conversion from the NAD 83 coordinates which are shown in ASR 1221073.

The new antenna will be a Radio Frequency Systems (RFS), model PHP30C. The antenna will be comprised of three tiers of panels which will be side mounted on three faces of a five-sided supporting structure. Each tier will have a different electrical beam tilt. The antenna design configuration has been devised to address the service and protection requirements of the various stations which will share in its use.

The undersigned was furnished with the tabulated vertical plane data from 90° above the horizontal plane (minus angles) to 90° below the horizontal plane (plus angles) at 0.1° increments for each 10° around the compass, plus similar data for certain additional 45° increment bearings and several special azimuths important to the Mexican allocation protection problem. In order to keep the size of this exhibit manageable, only the data from -5° to +10° are provided in Figure 3 herein. The data in Figure 3 were employed to derive the various patterns used in the studies for the instant amendment.

Figure 1, Sheet 1, is the proposed composite pattern based on the relative field toward the radio horizon in each 10° azimuthal direction. The relative field values have been normalized to unity for the maximum radiation which occurs at a bearing of 270° True at a depression angle of 0.9° below the horizontal plane. Unity on Sheet 1 represents an effective radiated power of 778 kW. Figure 1, Sheet 2, is the composite

pattern for the antenna using the maximum radiation that occurs in the vertical plane in each direction. Figure 2 is the tabulation of data used in preparing Figure 1. Figure 2 includes the antenna radiation center heights above average terrain used to calculate the depression angles. The USGS 3 arc-second terrain elevation database was the source for the terrain elevation data.

The data in Figure 3 were used to develop the eight vertical plane patterns of Figure 4. The patterns have been normalized and the depression angle to the radio horizon is identified on each pattern. These graphs permitted a determination as to whether or not the radiation at the depression angle to the radio horizon was greater or less than 90% of the maximum in the vertical plane in each radial direction. In each instance, the radiation was less than 90% of the maximum, and the radiation occurring at the depression angle was used to calculate the distance to the 48 dBu, F(50,90), principal community service contour as required by the FCC Rules. Figure 5 is the normalized azimuth pattern used for the 48 dBu, F(50,90), contour determination. Figure 6 is the tabulation of data used to determine the distances to the 48 dBu, F(50,90), contour, and Figure 7 is a map showing that the contour encompasses all of Anaheim as required by the FCC rules.

Compliance with the FCC's requirements for interference protection to domestic NTSC and DTV facilities is achieved with the facilities proposed herein. The studies that were made to determine compliance used a FCC matched computer analysis taking into account the facilities for other NTSC and DTV stations according to the conditions at the time of the original allotments in Appendix B of the Second Memorandum Opinion and Order on Reconsideration of the Fifth and Sixth Report and Orders in MM Docket

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Number 87-268, and as currently authorized, or proposed, where the current existing or proposed facilities exceed the then authorized NTSC facilities, or the original DTV allotment facilities.

A Sunblade processor was used with the FCC's TV_Process program. The TV-Process program takes into account all possible interference scenarios in determining compliance with the FCC's interference criteria. The processor output was scanned for any "failed" condition. No report of a "failed" condition occurred. A "failed" condition would have signified that the proposed KDOC-DT facility would create more than 2%, de minimis, interference to the particular station under review. The NTSC stations that were reviewed were: KCET, Los Angeles, CA., Channel 28; KMEX-TV, Los Angeles, CA, Channel 34; and KTBN-TV, Santa Ana, CA, Channel 40. The DTV stations that were reviewed were: KMCC-DT, Laughlin, AZ (formerly, Lake Havasu City, AZ), Channel 32; KBAK-DT, Bakersfield, CA, Channel 33; and KTLA-DT, Los Angeles, CA, Channel 31

As a cross-check, calculations were performed, specifically, for the authorized 1000 kW maximization construction permit for station KTLA-DT, in BPCDT-20000425AAV and the authorized 110 kW construction permit for station KBAK-DT in BPCDT-20000425AAV using the FCC's FLR algorithm on an Alpha processor. The Alpha processor has been used in the past with excellent correlation with the FCC's Appendix B results. The FLR program showed a reduction in interference to KTLA-DT, referenced to the baseline conditions used in developing the mentioned Appendix B. No interference at all was caused to KBAK-DT by the KDOC-DT facilities that are now proposed.

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At the time that Appendix B was formulated, KDOC-DT was located at Sunset Ridge, approximately 32 kilometers from the currently authorized Mt. Wilson site. The re-location of KDOC-DT to Mt. Wilson benefited, not only KDOC-DT, but other Mt. Wilson sited stations of allocation interest, as well. The co-location of facilities helped to reduce mutual interference.

The pending KDOC-DT maximization proposal has priority under the policies established regarding Class A station protection, and, in any event, there are no Class A stations close enough to the proposed KDOC-DT site to merit consideration. It is believed that the instant proposal is in compliance with all the Rules governing domestic interference issues.

The allocation concerns with respect to Mexico are reviewed in great detail in the accompanying Appendix. The Appendix demonstrates that the operation now proposed for KDOC-DT is configured to avoid increasing radiation toward the Tijuana, BC, Channel 32, DTV allotment in the Memorandum of Understanding. As indicated in an earlier paragraph, the Appendix may be used as a package for notification purposes to Mexico, if desired.

Environmental impact issues have been addressed in the pending application. Radio-frequency radiation (rfr) measurements are contemplated at the site and vicinity as part of the construction process to ascertain if radiation exceeding the maximum permissible level (MPL) prevails at any location accessible to the public. Appropriate corrective measures will be taken if it develops that excessive radiation levels are present.

BERNARD R. SEGAL, P. E.
CONSULTING ENGINEER
KENSINGTON, MARYLAND

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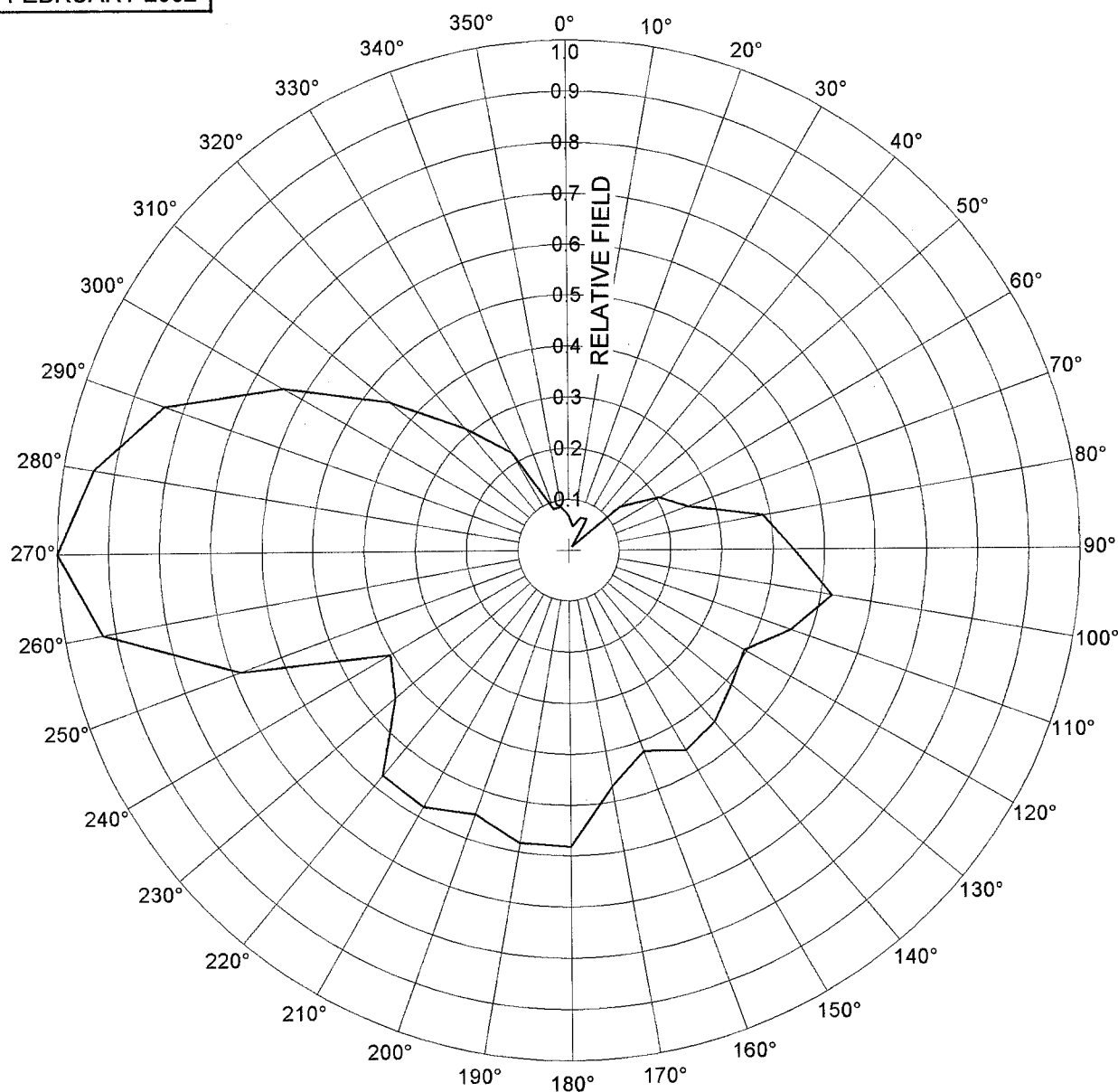
The tower will be located within a fence-enclosed area. Access within the fence will be available only to authorized personnel. Radiation hazard warning signs will be placed on the fence. In concert with other site users, protocols will be developed for the termination of excitation to the antenna when the prospect for overexposure to a worker might occur.

The instant amendment will not alter the conclusion that no significant impact on the environment will result in the event the instant proposal is implemented. An environmental assessment is not required for the instant proposal.

I declare under penalty of perjury that the foregoing is true and correct. Executed on March 12, 2002.

Bernard R. Segal, P.E.
Bernard R. Segal, P. E.

FEBRUARY 2002



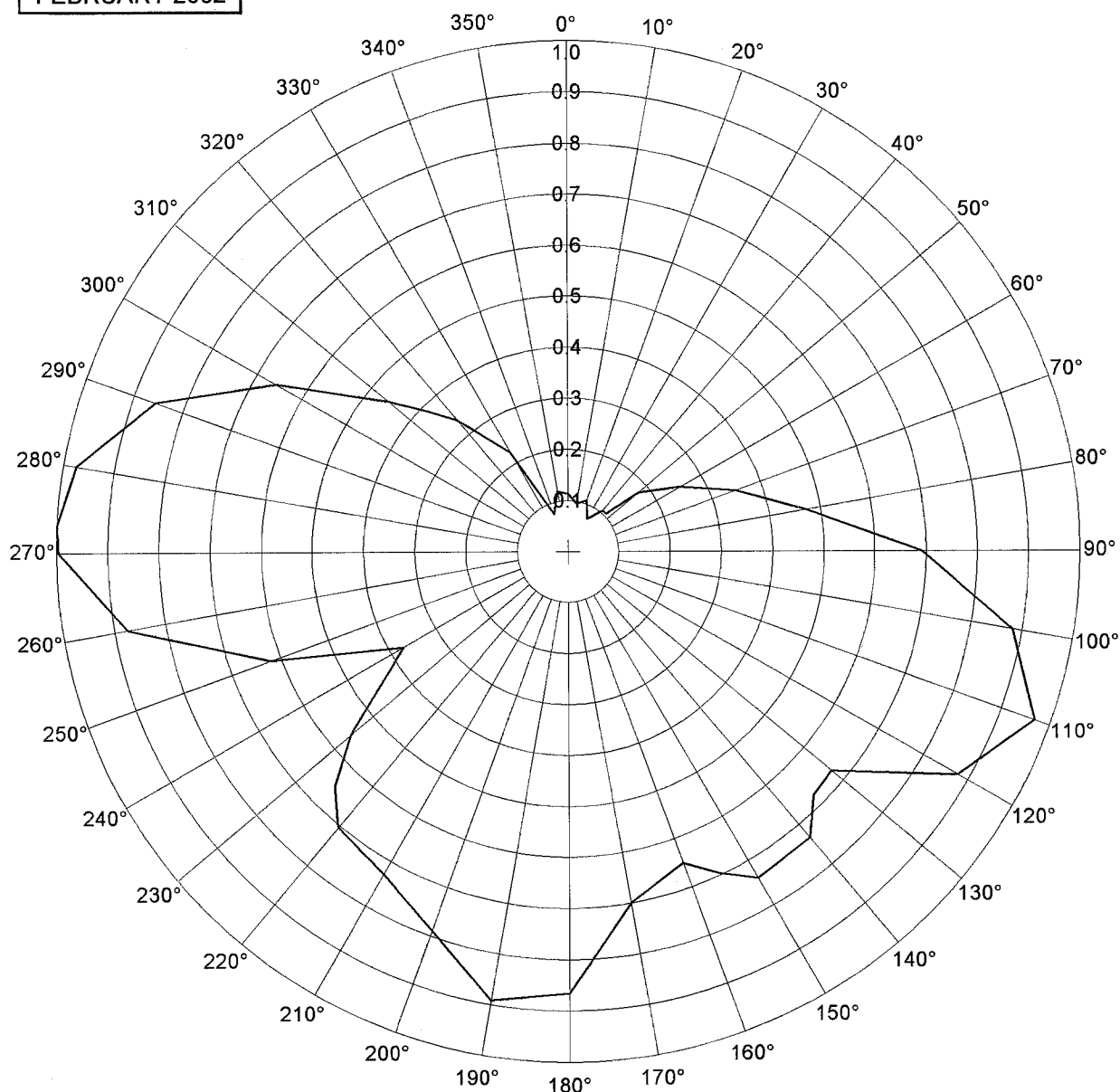
Note: Composite pattern maximum ERP = 778 kW

**COMPOSITE AZIMUTH PATTERN AT
DEPRESSION ANGLES TO THE RADIO HORIZON**

**GOLDEN ORANGE BROADCASTING CO., INC.
STATION KDOC-DT ANAHEIM, CALIFORNIA
CH. 32 1000 KW (MAX-DA) 938 METERS**

Bernard R. Segal, P. E. Consulting Engineer

FEBRUARY 2002



Note: Composite pattern maximum ERP = 1000 kW

**COMPOSITE AZIMUTH PATTERN USING
MAXIMUM VERTICAL PLANE RADIATION VALUES**

GOLDEN ORANGE BROADCASTING CO., INC.
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Bernard R. Segal, P. E. Consulting Engineer

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CONSULTING ENGINEER
KENSINGTON, MARYLAND

FIGURE 2
Sheet 1 of 2

TABULATION OF DATA FOR KDOC-DT AZIMUTH PATTERNS

Azimuth (Deg. T)	Rad. Center Above 3.2-16.1 km Terrain Avg. (meters)	Depr. Angle To Radio Horizon (Deg.)	Rel. Field At R.H. Depr. Angle	Fig.1 Sheet 1 Normal- ized Value	Depr. Angle For Max. Radiation (Deg.)	Fig.1, Sht.2 Rel. Field At Depr. Angle For Max. Rad
0	421	0.6	0.0603	0.068	2.5	0.1125
10	497	0.6	0.0425	0.048	2.6	0.0955
20	351	0.5	0.0595	0.067	2.3	0.1067
30	316	0.5	0.0618	0.070	2.1	0.0743
40	372	0.5	0.0096	0.011	3.1	0.1803
50	425	0.6	0.1156	0.131	2.5	0.2505
60	687	0.7	0.1803	0.204	2.6	0.3481
70	797	0.8	0.2191	0.248	2.7	0.4767
80	998	0.9	0.3395	0.385	2.7	0.6901
90	659	0.7	0.3881	0.440	2.7	0.8800
100	768	0.8	0.4597	0.521	2.7	0.9677
110	924	0.8	0.4062	0.460	2.7	0.8757
120	1122	0.9	0.3478	0.394	2.7	0.6689
130	1345	1.0	0.3631	0.412	2.6	0.6128
135	1403	1.0	0.3811	0.432	2.6	0.6741
140	1440	1.1	0.3878	0.440	2.7	0.7319
145	1465	1.1	0.4132	0.468	2.7	0.7561
150	1492	1.1	0.3997	0.453	2.8	0.7384
155	1520	1.1	0.3843	0.436	2.8	0.6953
160	1544	1.1	0.3699	0.419	2.7	0.6490
170	1519	1.1	0.4143	0.470	2.7	0.6966
180	1522	1.1	0.5120	0.580	2.7	0.8650
190	1536	1.1	0.5130	0.581	2.7	0.8905
200	1518	1.1	0.4841	0.549	2.7	0.7892
210	1503	1.1	0.5102	0.578	2.5	0.7277
220	1491	1.1	0.5051	0.572	2.4	0.6481
230	1439	1.1	0.3939	0.446	2.4	0.5559
240	1335	1.0	0.3578	0.406	1.4	0.3718
250	1279	1.0	0.6033	0.684	1.3	0.6191
260	1190	1.0	0.8166	0.926	1.6	0.8737
270	1009	0.9	0.8823	1.000	1.7	0.9960
273 (max)					1.7	1.0000
280	741	0.8	0.8302	0.941	1.7	0.9752
290	789	0.8	0.7394	0.838	1.6	0.8563
300	689	0.7	0.5651	0.640	1.6	0.6575
310	564	0.7	0.4014	0.455	1.5	0.4589
320	509	0.6	0.2765	0.313	1.3	0.3366

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CONSULTING ENGINEER
KENSINGTON, MARYLAND

FIGURE 2
Sheet 2 of 2

TABULATION OF DATA FOR KDOC-DT AZIMUTH PATTERNS

Azimuth	Rad. Center Above 3.2-16.1 km Terrain Avg.	Depr. Angle To Radio Horizon	Rel. Field At R.H. Depr. Angle	Fig.1 Sheet 1 Normal- ized Value	Depr. Angle For Max. Radiation	Fig.1, Sht.2 Rel. Field At Depr. Angle For Max. Rad
(Deg. T)	(meters)	(Deg.)			(Deg.)	
330	597	0.7	0.1954	0.221	1.6	0.2248
340	632	0.7	0.0761	0.086	1.0	0.0777
350	563	0.7	0.0761	0.086	2.2	0.1200

TABULATION OF KDOC-DT VERTICAL PLANE RELATIVE FIELD DATA
(MAXIMUM ERP = 1000 KW)

VERTICAL ANGLE	AZIMUTH - DEGREES TRUE						
	0	10	20	30	40	45	50
-5	0.0165	0.0105	0.0124	0.0188	0.0128	0.0105	0.0202
-4.9	0.0157	0.0097	0.012	0.0186	0.0118	0.0083	0.0183
-4.8	0.015	0.009	0.0119	0.0184	0.0107	0.0062	0.0169
-4.7	0.0145	0.0085	0.012	0.0181	0.0094	0.0047	0.0165
-4.6	0.0143	0.0083	0.0123	0.018	0.0081	0.0044	0.017
-4.5	0.0143	0.0085	0.0129	0.0178	0.0066	0.0055	0.0183
-4.4	0.0147	0.0089	0.0136	0.0178	0.0051	0.0073	0.0204
-4.3	0.0153	0.0096	0.0145	0.0179	0.0036	0.0095	0.0228
-4.2	0.0161	0.0105	0.0154	0.0182	0.0023	0.0116	0.0254
-4.1	0.0171	0.0114	0.0163	0.0185	0.0018	0.0137	0.0281
-4	0.0182	0.0124	0.0173	0.019	0.0025	0.0156	0.0306
-3.9	0.0193	0.0134	0.0181	0.0195	0.0039	0.0174	0.033
-3.8	0.0204	0.0144	0.0189	0.0202	0.0053	0.0189	0.0351
-3.7	0.0215	0.0153	0.0197	0.0209	0.0067	0.0202	0.0369
-3.6	0.0225	0.016	0.0203	0.0217	0.008	0.0212	0.0384
-3.5	0.0234	0.0166	0.0208	0.0225	0.0092	0.0219	0.0395
-3.4	0.0242	0.0172	0.0211	0.0232	0.0103	0.0223	0.0402
-3.3	0.0248	0.0175	0.0214	0.024	0.0112	0.0225	0.0406
-3.2	0.0253	0.0178	0.0216	0.0247	0.012	0.0223	0.0407
-3.1	0.0256	0.0178	0.0216	0.0254	0.0126	0.0219	0.0405
-3	0.0259	0.0178	0.0217	0.0261	0.013	0.0213	0.04
-2.9	0.0259	0.0177	0.0216	0.0266	0.0131	0.0205	0.0393
-2.8	0.0259	0.0175	0.0216	0.0271	0.0131	0.0195	0.0385
-2.7	0.0259	0.0172	0.0215	0.0275	0.0129	0.0184	0.0376
-2.6	0.0257	0.0169	0.0215	0.0278	0.0125	0.0173	0.0368
-2.5	0.0256	0.0167	0.0216	0.0281	0.012	0.0164	0.0363
-2.4	0.0256	0.0165	0.0218	0.0284	0.0113	0.0157	0.036
-2.3	0.0256	0.0164	0.0221	0.0286	0.0104	0.0153	0.0362
-2.2	0.0257	0.0164	0.0225	0.0289	0.0095	0.0154	0.0368
-2.1	0.0259	0.0166	0.0231	0.0291	0.0085	0.016	0.0378
-2	0.0264	0.017	0.0238	0.0294	0.0076	0.0171	0.0393
-1.9	0.0269	0.0175	0.0246	0.0298	0.0068	0.0185	0.0411
-1.8	0.0277	0.0182	0.0254	0.0302	0.0062	0.0201	0.0432
-1.7	0.0286	0.019	0.0264	0.0307	0.006	0.0218	0.0455
-1.6	0.0297	0.0199	0.0274	0.0314	0.0063	0.0235	0.0479
-1.5	0.0308	0.0209	0.0284	0.0321	0.0069	0.0251	0.0503
-1.4	0.032	0.0218	0.0293	0.0331	0.0078	0.0266	0.0525
-1.3	0.0333	0.0228	0.0303	0.0341	0.0088	0.0279	0.0546
-1.2	0.0346	0.0237	0.0317	0.0353	0.0098	0.029	0.0565
-1.1	0.0358	0.0245	0.0322	0.0366	0.0108	0.0298	0.0582
-1	0.0371	0.0253	0.0331	0.038	0.0117	0.0303	0.0596

TABULATION OF KDOC-DT VERTICAL PLANE RELATIVE FIELD DATA
(MAXIMUM ERP = 1000 KW)

VERTICAL ANGLE	AZIMUTH - DEGREES TRUE						
	0	10	20	30	40	45	50
-0.9	0.0382	0.0259	0.034	0.0395	0.0124	0.0305	0.0608
-0.8	0.0393	0.0265	0.0349	0.0411	0.0129	0.0304	0.0617
-0.7	0.0404	0.027	0.0358	0.0427	0.0132	0.0302	0.0626
-0.6	0.0414	0.0274	0.0367	0.0444	0.0132	0.0298	0.0634
-0.5	0.0424	0.0278	0.0378	0.0461	0.0129	0.0294	0.0643
-0.4	0.0433	0.0281	0.039	0.0478	0.0124	0.0292	0.0654
-0.3	0.0443	0.0286	0.0403	0.0495	0.0115	0.0294	0.0669
-0.2	0.0454	0.0291	0.0419	0.0511	0.0104	0.0302	0.069
-0.1	0.0465	0.0298	0.0437	0.0528	0.0089	0.0318	0.0718
0	0.0478	0.0307	0.0457	0.0544	0.0072	0.0343	0.0755
0.1	0.0493	0.0319	0.048	0.056	0.0055	0.0377	0.08
0.2	0.051	0.0333	0.0505	0.0575	0.0041	0.042	0.0855
0.3	0.0529	0.0351	0.0533	0.059	0.0043	0.0472	0.0918
0.4	0.0551	0.0373	0.0563	0.0604	0.0065	0.053	0.099
0.5	0.0576	0.0397	0.0595	0.0618	0.0096	0.0595	0.107
0.6	0.0603	0.0425	0.0629	0.0631	0.0132	0.0665	0.1156
0.7	0.0633	0.0455	0.0665	0.0644	0.0173	0.0738	0.1248
0.8	0.0665	0.0488	0.0701	0.0656	0.0216	0.0814	0.1343
0.9	0.0699	0.0522	0.0737	0.0668	0.0261	0.0892	0.1441
1	0.0734	0.0558	0.0774	0.0679	0.0309	0.0971	0.1541
1.1	0.0771	0.0595	0.081	0.0689	0.0358	0.105	0.1641
1.2	0.0807	0.0632	0.0845	0.0699	0.0408	0.1128	0.1739
1.3	0.0844	0.0668	0.0879	0.0707	0.0458	0.1205	0.1836
1.4	0.0881	0.0704	0.0911	0.0715	0.0509	0.128	0.1929
1.5	0.0916	0.0739	0.0941	0.0723	0.056	0.1353	0.2018
1.6	0.095	0.0773	0.0968	0.0729	0.061	0.1421	0.2103
1.7	0.0982	0.0805	0.0993	0.0734	0.066	0.1486	0.2181
1.8	0.1012	0.0834	0.1015	0.0738	0.0708	0.1546	0.2252
1.9	0.1039	0.0861	0.1033	0.0741	0.0754	0.16	0.2316
2	0.1063	0.0885	0.1048	0.0743	0.0798	0.165	0.2371
2.1	0.1083	0.0906	0.1058	0.0743	0.084	0.1692	0.2417
2.2	0.11	0.0923	0.1065	0.0741	0.0878	0.1728	0.2454
2.3	0.1112	0.0937	0.1067	0.0738	0.0913	0.1757	0.2481
2.4	0.1121	0.0947	0.1066	0.0733	0.0945	0.1779	0.2498
2.5	0.1125	0.0953	0.106	0.0726	0.0973	0.1795	0.2505
2.6	0.1124	0.0955	0.105	0.0718	0.0997	0.1803	0.2502
2.7	0.1119	0.0954	0.1036	0.0707	0.1017	0.1803	0.2489
2.8	0.111	0.0948	0.1018	0.0695	0.1032	0.1797	0.2466
2.9	0.1096	0.0939	0.0997	0.068	0.1043	0.1784	0.2434
3	0.1078	0.0926	0.0971	0.0664	0.105	0.1764	0.2392
3.1	0.1056	0.0909	0.0942	0.0645	0.1052	0.1737	0.2341

BERNARD R. SEGAL, P. E.
CONSULTING ENGINEER
KENSINGTON, MARYLAND

FIGURE 3
SHEET 3

TABULATION OF KDOC-DT VERTICAL PLANE RELATIVE FIELD DATA
(MAXIMUM ERP = 1000 KW)

VERTICAL ANGLE	AZIMUTH - DEGREES TRUE						
	0	10	20	30	40	45	50
3.2	0.1029	0.0888	0.091	0.0625	0.105	0.1704	0.2281
3.3	0.0999	0.0864	0.0876	0.0603	0.1043	0.1665	0.2214
3.4	0.0965	0.0838	0.0838	0.0579	0.1032	0.1621	0.2141
3.5	0.0928	0.0808	0.0799	0.0553	0.1017	0.1572	0.2061
3.6	0.0889	0.0777	0.0758	0.0527	0.0998	0.1519	0.1977
3.7	0.0847	0.0743	0.0716	0.0499	0.0975	0.1463	0.1889
3.8	0.0803	0.0708	0.0674	0.0469	0.095	0.1404	0.1797
3.9	0.0758	0.0672	0.0631	0.0439	0.0921	0.1343	0.1704
4	0.0712	0.0635	0.0588	0.0409	0.089	0.128	0.161
4.1	0.0666	0.0597	0.0546	0.0378	0.0856	0.1217	0.1516
4.2	0.062	0.056	0.0506	0.0346	0.0821	0.1154	0.1424
4.3	0.0575	0.0523	0.0467	0.0315	0.0785	0.1092	0.1335
4.4	0.0531	0.0488	0.0431	0.0285	0.0748	0.1032	0.125
4.5	0.049	0.0455	0.0398	0.0255	0.0711	0.0975	0.117
4.6	0.0452	0.0424	0.0369	0.0227	0.0674	0.0921	0.1097
4.7	0.0417	0.0396	0.0343	0.0201	0.0638	0.087	0.1031
4.8	0.0386	0.0371	0.0322	0.0177	0.0603	0.0825	0.0973
4.9	0.0361	0.0349	0.0305	0.0156	0.0571	0.0784	0.0924
5	0.034	0.0332	0.0293	0.0139	0.0541	0.0748	0.0883
5.1	0.0324	0.0317	0.0284	0.0126	0.0513	0.0717	0.0849
5.2	0.0314	0.0307	0.0278	0.0119	0.0489	0.0691	0.0823
5.3	0.0307	0.0299	0.0275	0.0116	0.0468	0.0669	0.0803
5.4	0.0303	0.0293	0.0273	0.0118	0.0451	0.0651	0.0787
5.5	0.0302	0.029	0.0271	0.0122	0.0437	0.0637	0.0775
5.6	0.0302	0.0287	0.027	0.0127	0.0426	0.0624	0.0765
5.7	0.0303	0.0285	0.0268	0.0134	0.0418	0.0613	0.0755
5.8	0.0303	0.0283	0.0265	0.014	0.0411	0.0603	0.0745
5.9	0.0302	0.0281	0.0261	0.0144	0.0406	0.0593	0.0733
6	0.03	0.0277	0.0256	0.0148	0.0403	0.0583	0.072
6.1	0.0296	0.0273	0.0249	0.015	0.0399	0.0572	0.0705
6.2	0.0291	0.0267	0.0241	0.0151	0.0396	0.0559	0.0686
6.3	0.0283	0.026	0.0231	0.0149	0.0392	0.0546	0.0666
6.4	0.0274	0.0252	0.022	0.0146	0.0387	0.0532	0.0643
6.5	0.0262	0.0243	0.0208	0.0142	0.0381	0.0517	0.0619
6.6	0.025	0.0233	0.0195	0.0135	0.0374	0.0501	0.0593
6.7	0.0236	0.0222	0.0183	0.0128	0.0366	0.0484	0.0566
6.8	0.0221	0.021	0.017	0.0118	0.0357	0.0467	0.054
6.9	0.0206	0.0199	0.0158	0.0108	0.0347	0.045	0.0514
7	0.0191	0.0188	0.0148	0.0097	0.0336	0.0433	0.049
7.1	0.0177	0.0177	0.0139	0.0085	0.0324	0.0417	0.0468
7.2	0.0164	0.0168	0.0133	0.0072	0.0311	0.0403	0.045

TABULATION OF KDOC-DT VERTICAL PLANE RELATIVE FIELD DATA
(MAXIMUM ERP = 1000 KW)

VERTICAL ANGLE	AZIMUTH - DEGREES TRUE						
	0	10	20	30	40	45	50
7.3	0.0153	0.016	0.0129	0.0059	0.0299	0.039	0.0435
7.4	0.0145	0.0154	0.0128	0.0047	0.0286	0.0379	0.0425
7.5	0.0141	0.015	0.0129	0.0036	0.0275	0.037	0.0419
7.6	0.0139	0.0149	0.0132	0.0029	0.0264	0.0363	0.0416
7.7	0.0141	0.0149	0.0137	0.0028	0.0254	0.0358	0.0417
7.8	0.0146	0.0151	0.0142	0.0033	0.0246	0.0355	0.0421
7.9	0.0152	0.0154	0.0148	0.0042	0.0239	0.0353	0.0426
8	0.0159	0.0157	0.0153	0.0052	0.0235	0.0353	0.0431
8.1	0.0166	0.0161	0.0157	0.0062	0.0231	0.0352	0.0436
8.2	0.0173	0.0165	0.016	0.0072	0.023	0.0352	0.0441
8.3	0.0179	0.0168	0.0162	0.008	0.023	0.0352	0.0443
8.4	0.0183	0.017	0.0162	0.0088	0.0231	0.035	0.0443
8.5	0.0186	0.0171	0.0161	0.0094	0.0232	0.0348	0.0441
8.6	0.0188	0.017	0.0158	0.0099	0.0234	0.0345	0.0435
8.7	0.0187	0.0169	0.0154	0.0103	0.0236	0.034	0.0427
8.8	0.0185	0.0166	0.0148	0.0105	0.0237	0.0334	0.0417
8.9	0.0181	0.0162	0.0141	0.0106	0.0238	0.0327	0.0403
9	0.0174	0.0156	0.0132	0.0105	0.0237	0.0319	0.0387
9.1	0.0166	0.015	0.0122	0.0103	0.0236	0.0309	0.0369
9.2	0.0157	0.0142	0.0111	0.01	0.0234	0.0298	0.0349
9.3	0.0146	0.0133	0.01	0.0095	0.023	0.0287	0.0328
9.4	0.0133	0.0123	0.0089	0.0089	0.0225	0.0275	0.0306
9.5	0.012	0.0114	0.0077	0.0082	0.022	0.0263	0.0286
9.6	0.0106	0.0104	0.0067	0.0074	0.0213	0.0252	0.0267
9.7	0.0092	0.0095	0.0059	0.0066	0.0205	0.0242	0.025
9.8	0.0079	0.0086	0.0054	0.0056	0.0197	0.0233	0.0238
9.9	0.0068	0.008	0.0054	0.0046	0.0188	0.0226	0.023
10	0.006	0.0076	0.0058	0.0037	0.0179	0.0221	0.0228