



ENGINEERING STATEMENT
OF
JOHN F.X. BROWNE, P.E.
IN SUPPORT OF AN APPLICATION FOR
MINOR MODIFICATION OF A POST-TRANSITION CONSTRUCTION PERMIT
WXYZ-DT
DETROIT, MI

Background

Channel 7 of Detroit, Inc. is the licensee of WXYZ which has been authorized to operate its post-transition DTV facility on Channel 41 (BPCDT-20080228AAC) at Detroit, MI, with an ERP of 985 kW at an HAAT of 305m. The tower is located at the following coordinates:

(NAD27)
42° 28' 14" N
83° 15' 01" W

WXYZ now wishes to "maximize" the post-transition facility ERP to 1000 kW. All other facility parameters will remain the same.



Site

The proposed facility is located within the Canadian border zone and coordination with the Canadian government is requested to the extent necessary in light of the FCC's ongoing negotiations with the Canadian administration.

Antenna System and Tower

WXYZ proposes to use the directional digital antenna specified in its recently granted post-transition construction permit (March, 2008), a Dielectric TFU-26GTH-R 6C140 (specifications attached hereto as Figure 1a - Figure 1e), for the proposed maximized facility. The antenna will be installed on a tower (ASR#1002464) after the existing analog antenna is removed. The tower will have a new overall height of 523.8m AMSL (with appurtenances) which is 5.8m lower than the present overall tower height of 529.6m AMSL and the antenna will have a center of radiation of 516.1m AMSL (with a calculated HAAT of 305m). The FAA will be notified of the decrease in height of the overall structure and the ASR will be amended accordingly.

Coverage

The entire principal community of Detroit, MI is well within the predicted F(50,90) 48 dBu contour based on the proposed 1000 kW ERP.

Interference

Studies were conducted with the proposed parameters using software that emulates the software used by the FCC (OET-69 analysis). The results of the study indicate that there are no post-transition domestic stations that would receive more than the 0.5% new interference.



Environmental/RFR

The proposed construction does not require preparation of an Environmental Assessment as it does not involve any of the factors listed in Section 1.1306.

The additional ground level RFR contributed to the site by this proposal in public areas is calculated to be 0.003371 mW/cm^2 which is less than 5% of the MPE for public exposure (0.423 mW/cm^2) at the proposed frequency and, therefore, the proposal is excluded from further consideration.

WXYZ agrees to comply with the Commission's requirements regarding power adjustments or cessation of operation as may be necessary to ensure a compliant environment for worker access. Workers will be encouraged to wear personal RFR monitors when on the structure. The tower base is enclosed by a locked security fence and appropriate signage warning of RFR hazards is posted.

Certification

I hereby certify that the foregoing report or statement was prepared by me but may include work performed by others under my supervision or direction. The statements of fact contained therein are believed to be true and correct based on personal knowledge, information and belief unless otherwise stated; with respect to facts not known of my own personal knowledge, I believe them to be true and correct based on their origin from sources known to me to be generally reliable and accurate. I have prepared this document with due care and in accordance with applicable standards of professional practice.

John F. X. Browne, P.E.
June 11, 2008

DIRECTIONAL ANTENNA DATA
WXYZ-DT
dBk Table

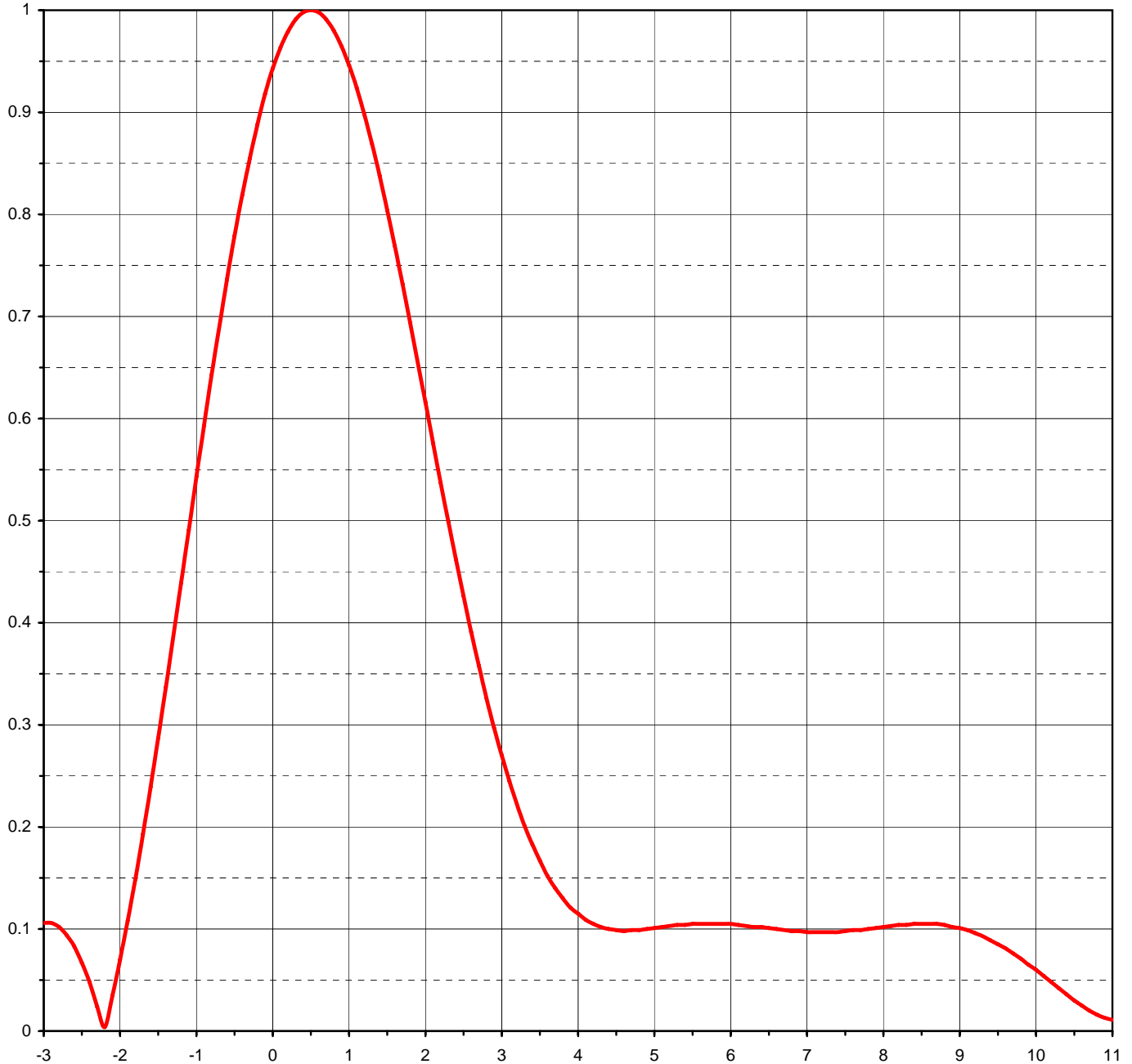
| Actual Bearing | Pattern Azimuth | Relative Field | ERP (dBk) | CONTOURS(km) | |
|----------------|-----------------|----------------|-----------|--------------|--------|
| | | | | 48 dBu | 41 dBu |
| N000E | 0.00 | 0.883 | 28.92 | 78.0 | 90.1 |
| | 10.00 | 0.858 | 28.67 | | |
| | 20.00 | 0.853 | 28.62 | | |
| | 30.00 | 0.848 | 28.57 | | |
| | 40.00 | 0.814 | 28.21 | | |
| N045E | 45.00 | 0.787 | 27.92 | 80.5 | 92.8 |
| | 50.00 | 0.759 | 27.60 | | |
| | 60.00 | 0.725 | 27.21 | | |
| | 70.00 | 0.741 | 27.40 | | |
| | 80.00 | 0.782 | 27.86 | | |
| N090E | 90.00 | 0.810 | 28.17 | 82.0 | 94.5 |
| | 100.00 | 0.815 | 28.22 | | |
| | 110.00 | 0.813 | 28.20 | | |
| | 120.00 | 0.817 | 28.24 | | |
| | 130.00 | 0.825 | 28.33 | | |
| N135E | 135.00 | 0.828 | 28.36 | 82.3 | 94.9 |
| | 140.00 | 0.829 | 28.37 | | |
| | 150.00 | 0.825 | 28.33 | | |
| | 160.00 | 0.817 | 28.24 | | |
| | 170.00 | 0.813 | 28.20 | | |
| N180E | 180.00 | 0.815 | 28.22 | 83.3 | 95.7 |
| | 190.00 | 0.810 | 28.17 | | |
| | 200.00 | 0.782 | 27.86 | | |
| | 210.00 | 0.741 | 27.40 | | |
| | 220.00 | 0.725 | 27.21 | | |
| N225E | 225.00 | 0.737 | 27.35 | 81.1 | 93.3 |
| | 230.00 | 0.759 | 27.60 | | |
| | 240.00 | 0.814 | 28.21 | | |
| | 250.00 | 0.848 | 28.57 | | |
| | 260.00 | 0.853 | 28.62 | | |
| N270E | 270.00 | 0.858 | 28.67 | 79.6 | 92.0 |
| | 280.00 | 0.883 | 28.92 | | |
| | 290.00 | 0.924 | 29.31 | | |
| | 300.00 | 0.965 | 29.69 | | |
| | 310.00 | 0.991 | 29.92 | | |
| N315E | 315.00 | 0.998 | 29.98 | 78.4 | 90.9 |
| | 320.00 | 1.000 | 30.00 | | |
| | 330.00 | 0.991 | 29.92 | | |
| | 340.00 | 0.965 | 29.69 | | |
| | 350.00 | 0.924 | 29.31 | | |

Maximum: N320E 30.00 dBk

Minima: N060E 27.21 dBk
N220E 27.21 dBk

ELEVATION PATTERN

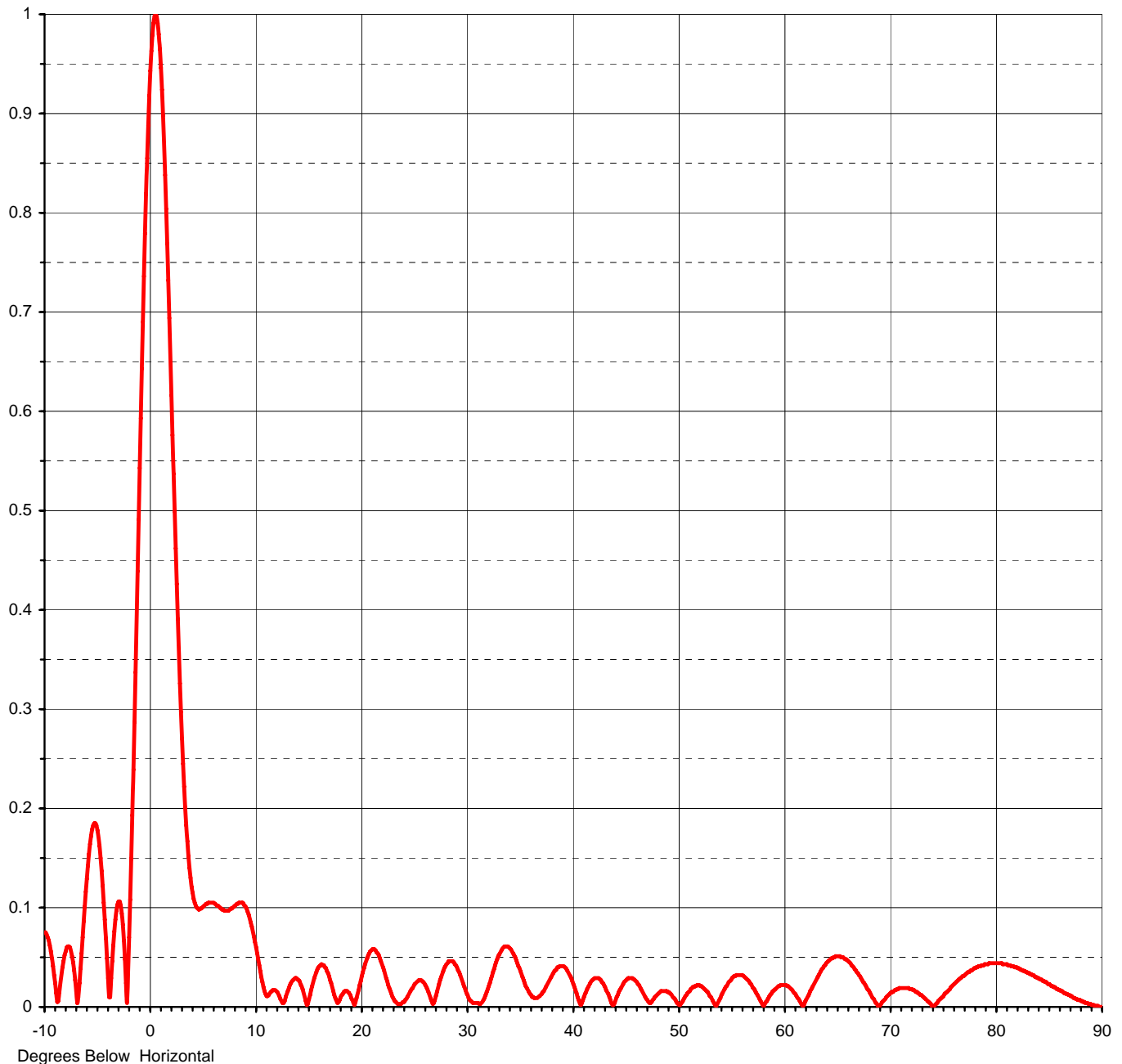
| | | | |
|------------------------|---------------------------|-----------|-------------------|
| RMS Gain at Main Lobe | 24.00 (13.80 dB) | Beam Tilt | 0.50 deg |
| RMS Gain at Horizontal | 21.30 (13.28 dB) | Frequency | 635.00 MHz |
| Calculated / Measured | Calculated | Drawing # | 26G240050 |



Degrees Below Horizontal

ELEVATION PATTERN

| | | | | |
|------------------------|-------------------|---------------------|-----------|---------------------|
| RMS Gain at Main Lobe | 24.00 | (13.80 dB) | Beam Tilt | 0.50 deg |
| RMS Gain at Horizontal | 21.30 | (13.28 dB) | Frequency | 635.00 MHz |
| Calculated / Measured | Calculated | | Drawing # | 26G240050-90 |



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Proposal Number **C-01305** Revision: **2**
 Date **28-Aug-07**
 Call Letters **WXYZ-DT** Channel **41**
 Location **Detroit, MI**
 Customer **Scripps Howard**
 Antenna Type **TFU-26GTH-R 6C140**

TABULATION OF ELEVATION PATTERN

Elevation Pattern Drawing #: **26G240050-90**

| Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -10.0 | 0.075 | 2.4 | 0.462 | 10.6 | 0.030 | 30.5 | 0.005 | 51.0 | 0.015 | 71.5 | 0.019 |
| -9.5 | 0.062 | 2.6 | 0.391 | 10.8 | 0.020 | 31.0 | 0.004 | 51.5 | 0.020 | 72.0 | 0.018 |
| -9.0 | 0.024 | 2.8 | 0.326 | 11.0 | 0.013 | 31.5 | 0.005 | 52.0 | 0.022 | 72.5 | 0.015 |
| -8.5 | 0.024 | 3.0 | 0.270 | 11.5 | 0.015 | 32.0 | 0.018 | 52.5 | 0.018 | 73.0 | 0.011 |
| -8.0 | 0.056 | 3.2 | 0.222 | 12.0 | 0.016 | 32.5 | 0.035 | 53.0 | 0.011 | 73.5 | 0.006 |
| -7.5 | 0.056 | 3.4 | 0.183 | 12.5 | 0.006 | 33.0 | 0.051 | 53.5 | 0.002 | 74.0 | 0.000 |
| -7.0 | 0.016 | 3.6 | 0.152 | 13.0 | 0.013 | 33.5 | 0.060 | 54.0 | 0.009 | 74.5 | 0.006 |
| -6.5 | 0.054 | 3.8 | 0.130 | 13.5 | 0.026 | 34.0 | 0.060 | 54.5 | 0.020 | 75.0 | 0.011 |
| -6.0 | 0.129 | 4.0 | 0.115 | 14.0 | 0.028 | 34.5 | 0.052 | 55.0 | 0.027 | 75.5 | 0.017 |
| -5.5 | 0.179 | 4.2 | 0.105 | 14.5 | 0.018 | 35.0 | 0.039 | 55.5 | 0.032 | 76.0 | 0.023 |
| -5.0 | 0.178 | 4.4 | 0.100 | 15.0 | 0.003 | 35.5 | 0.024 | 56.0 | 0.032 | 76.5 | 0.028 |
| -4.5 | 0.122 | 4.6 | 0.098 | 15.5 | 0.025 | 36.0 | 0.013 | 56.5 | 0.028 | 77.0 | 0.032 |
| -4.0 | 0.029 | 4.8 | 0.099 | 16.0 | 0.040 | 36.5 | 0.009 | 57.0 | 0.021 | 77.5 | 0.036 |
| -3.5 | 0.062 | 5.0 | 0.101 | 16.5 | 0.042 | 37.0 | 0.012 | 57.5 | 0.012 | 78.0 | 0.039 |
| -3.0 | 0.106 | 5.2 | 0.103 | 17.0 | 0.031 | 37.5 | 0.020 | 58.0 | 0.002 | 78.5 | 0.041 |
| -2.8 | 0.102 | 5.4 | 0.104 | 17.5 | 0.012 | 38.0 | 0.030 | 58.5 | 0.008 | 79.0 | 0.043 |
| -2.6 | 0.083 | 5.6 | 0.105 | 18.0 | 0.007 | 38.5 | 0.038 | 59.0 | 0.016 | 79.5 | 0.044 |
| -2.4 | 0.048 | 5.8 | 0.105 | 18.5 | 0.016 | 39.0 | 0.041 | 59.5 | 0.021 | 80.0 | 0.044 |
| -2.2 | 0.004 | 6.0 | 0.105 | 19.0 | 0.012 | 39.5 | 0.037 | 60.0 | 0.022 | 80.5 | 0.044 |
| -2.0 | 0.070 | 6.2 | 0.103 | 19.5 | 0.005 | 40.0 | 0.026 | 60.5 | 0.020 | 81.0 | 0.043 |
| -1.8 | 0.149 | 6.4 | 0.102 | 20.0 | 0.026 | 40.5 | 0.010 | 61.0 | 0.014 | 81.5 | 0.041 |
| -1.6 | 0.239 | 6.6 | 0.100 | 20.5 | 0.046 | 41.0 | 0.007 | 61.5 | 0.006 | 82.0 | 0.039 |
| -1.4 | 0.337 | 6.8 | 0.098 | 21.0 | 0.057 | 41.5 | 0.020 | 62.0 | 0.005 | 82.5 | 0.037 |
| -1.2 | 0.439 | 7.0 | 0.097 | 21.5 | 0.055 | 42.0 | 0.028 | 62.5 | 0.016 | 83.0 | 0.034 |
| -1.0 | 0.543 | 7.2 | 0.097 | 22.0 | 0.043 | 42.5 | 0.029 | 63.0 | 0.026 | 83.5 | 0.032 |
| -0.8 | 0.643 | 7.4 | 0.097 | 22.5 | 0.026 | 43.0 | 0.022 | 63.5 | 0.036 | 84.0 | 0.029 |
| -0.6 | 0.736 | 7.6 | 0.099 | 23.0 | 0.010 | 43.5 | 0.010 | 64.0 | 0.044 | 84.5 | 0.026 |
| -0.4 | 0.819 | 7.8 | 0.100 | 23.5 | 0.003 | 44.0 | 0.004 | 64.5 | 0.049 | 85.0 | 0.023 |
| -0.2 | 0.888 | 8.0 | 0.102 | 24.0 | 0.005 | 44.5 | 0.017 | 65.0 | 0.051 | 85.5 | 0.020 |
| 0.0 | 0.943 | 8.2 | 0.104 | 24.5 | 0.012 | 45.0 | 0.026 | 65.5 | 0.050 | 86.0 | 0.017 |
| 0.2 | 0.979 | 8.4 | 0.105 | 25.0 | 0.021 | 45.5 | 0.029 | 66.0 | 0.046 | 86.5 | 0.014 |
| 0.4 | 0.998 | 8.6 | 0.105 | 25.5 | 0.027 | 46.0 | 0.026 | 66.5 | 0.040 | 87.0 | 0.011 |
| 0.6 | 0.998 | 8.8 | 0.104 | 26.0 | 0.024 | 46.5 | 0.018 | 67.0 | 0.032 | 87.5 | 0.008 |
| 0.8 | 0.980 | 9.0 | 0.101 | 26.5 | 0.012 | 47.0 | 0.008 | 67.5 | 0.024 | 88.0 | 0.006 |
| 1.0 | 0.946 | 9.2 | 0.096 | 27.0 | 0.007 | 47.5 | 0.005 | 68.0 | 0.015 | 88.5 | 0.004 |
| 1.2 | 0.898 | 9.4 | 0.089 | 27.5 | 0.027 | 48.0 | 0.012 | 68.5 | 0.006 | 89.0 | 0.002 |
| 1.4 | 0.838 | 9.6 | 0.081 | 28.0 | 0.041 | 48.5 | 0.016 | 69.0 | 0.002 | 89.5 | 0.001 |
| 1.6 | 0.769 | 9.8 | 0.076 | 28.5 | 0.046 | 49.0 | 0.015 | 69.5 | 0.008 | 90.0 | 0.000 |
| 1.8 | 0.694 | 10.0 | 0.065 | 29.0 | 0.042 | 49.5 | 0.010 | 70.0 | 0.014 | | |
| 2.0 | 0.616 | 10.2 | 0.054 | 29.5 | 0.029 | 50.0 | 0.003 | 70.5 | 0.017 | | |
| 2.2 | 0.537 | 10.4 | 0.042 | 30.0 | 0.014 | 50.5 | 0.007 | 71.0 | 0.019 | | |

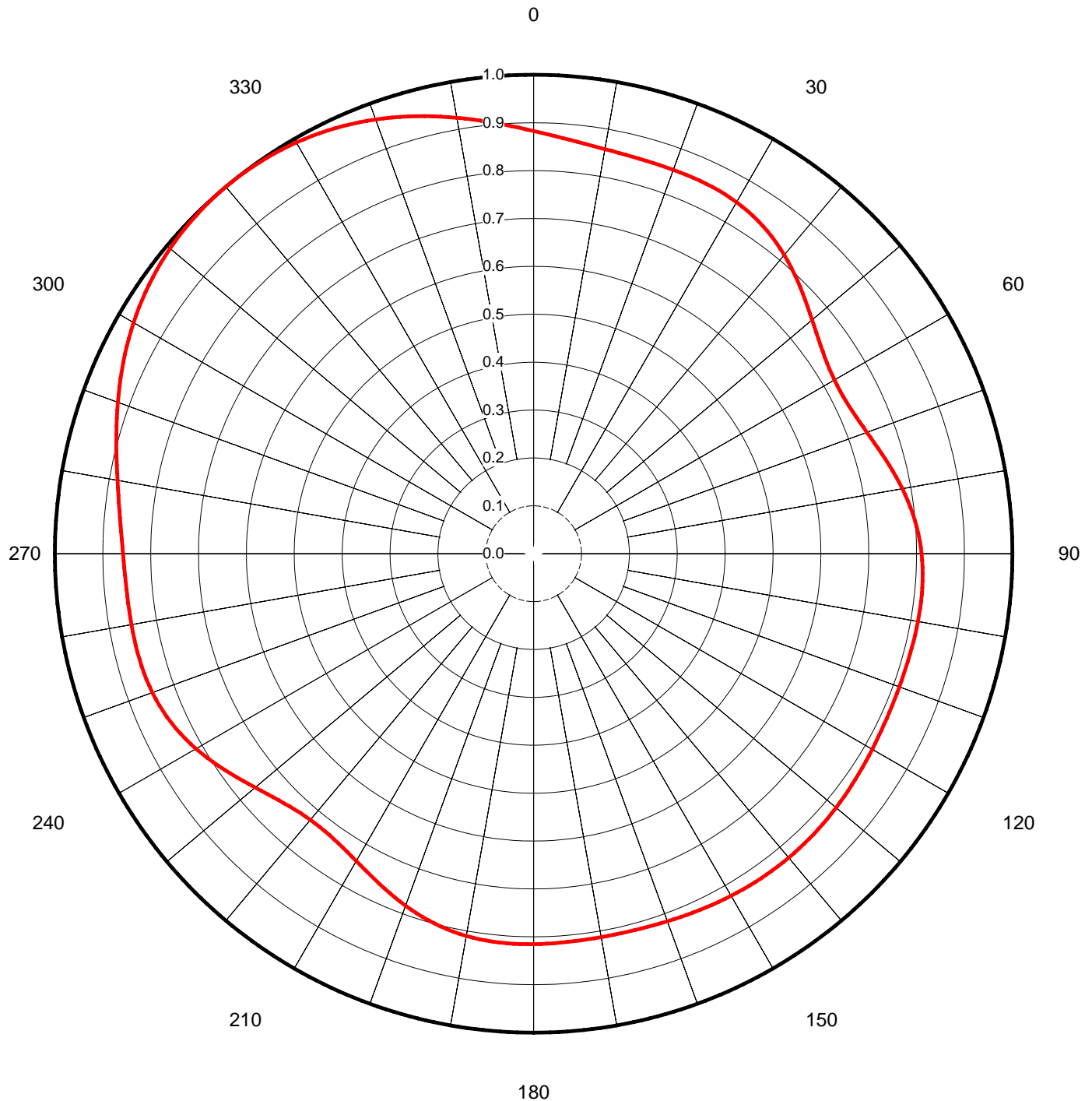
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| | | | |
|-----------------|--------------------------|-----------|-----------|
| Proposal Number | C-01305 | Revision: | 2 |
| Date | 28-Aug-07 | | |
| Call Letters | WXYZ-DT | Channel | 41 |
| Location | Detroit, MI | | |
| Customer | Scripps Howard | | |
| Antenna Type | TFU-26GTH-R 6C140 | | |

AZIMUTH PATTERN

Gain **1.40** (1.46 dB)
Calculated / Measured **Calculated**

Frequency **635.00 MHz**
Drawing # **TFU-6C140**





| | | | |
|-----------------|--------------------------|-----------|-----------|
| Proposal Number | C-01305 | Revision: | 2 |
| Date | 7-Aug-07 | | |
| Call Letters | WXYZ-DT | Channel | 41 |
| Location | Detroit, MI | | |
| Customer | Scripps Howard | | |
| Antenna Type | TFU-26GTH-R 6C140 | | |

TABULATION OF AZIMUTH PATTERN

Azimuth Pattern Drawing #: **TFU-6C140**

| Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0.883 | 45 | 0.787 | 90 | 0.810 | 135 | 0.828 | 180 | 0.815 | 225 | 0.737 | 270 | 0.858 | 315 | 0.998 |
| 1 | 0.879 | 46 | 0.782 | 91 | 0.812 | 136 | 0.828 | 181 | 0.815 | 226 | 0.741 | 271 | 0.859 | 316 | 0.999 |
| 2 | 0.876 | 47 | 0.776 | 92 | 0.813 | 137 | 0.828 | 182 | 0.815 | 227 | 0.745 | 272 | 0.861 | 317 | 0.999 |
| 3 | 0.873 | 48 | 0.770 | 93 | 0.814 | 138 | 0.829 | 183 | 0.815 | 228 | 0.749 | 273 | 0.863 | 318 | 1.000 |
| 4 | 0.870 | 49 | 0.765 | 94 | 0.815 | 139 | 0.829 | 184 | 0.815 | 229 | 0.754 | 274 | 0.865 | 319 | 1.000 |
| 5 | 0.867 | 50 | 0.759 | 95 | 0.815 | 140 | 0.829 | 185 | 0.815 | 230 | 0.759 | 275 | 0.867 | 320 | 1.000 |
| 6 | 0.865 | 51 | 0.754 | 96 | 0.815 | 141 | 0.829 | 186 | 0.815 | 231 | 0.765 | 276 | 0.870 | 321 | 1.000 |
| 7 | 0.863 | 52 | 0.749 | 97 | 0.815 | 142 | 0.829 | 187 | 0.814 | 232 | 0.770 | 277 | 0.873 | 322 | 1.000 |
| 8 | 0.861 | 53 | 0.745 | 98 | 0.815 | 143 | 0.828 | 188 | 0.813 | 233 | 0.776 | 278 | 0.876 | 323 | 0.999 |
| 9 | 0.859 | 54 | 0.741 | 99 | 0.815 | 144 | 0.828 | 189 | 0.812 | 234 | 0.782 | 279 | 0.879 | 324 | 0.999 |
| 10 | 0.858 | 55 | 0.737 | 100 | 0.815 | 145 | 0.828 | 190 | 0.810 | 235 | 0.787 | 280 | 0.883 | 325 | 0.998 |
| 11 | 0.857 | 56 | 0.733 | 101 | 0.815 | 146 | 0.827 | 191 | 0.809 | 236 | 0.793 | 281 | 0.886 | 326 | 0.997 |
| 12 | 0.855 | 57 | 0.731 | 102 | 0.815 | 147 | 0.827 | 192 | 0.807 | 237 | 0.799 | 282 | 0.890 | 327 | 0.996 |
| 13 | 0.855 | 58 | 0.728 | 103 | 0.814 | 148 | 0.826 | 193 | 0.804 | 238 | 0.804 | 283 | 0.894 | 328 | 0.994 |
| 14 | 0.854 | 59 | 0.727 | 104 | 0.814 | 149 | 0.825 | 194 | 0.802 | 239 | 0.809 | 284 | 0.898 | 329 | 0.993 |
| 15 | 0.854 | 60 | 0.725 | 105 | 0.814 | 150 | 0.825 | 195 | 0.799 | 240 | 0.814 | 285 | 0.902 | 330 | 0.991 |
| 16 | 0.853 | 61 | 0.725 | 106 | 0.813 | 151 | 0.824 | 196 | 0.796 | 241 | 0.819 | 286 | 0.907 | 331 | 0.989 |
| 17 | 0.853 | 62 | 0.725 | 107 | 0.813 | 152 | 0.823 | 197 | 0.793 | 242 | 0.824 | 287 | 0.911 | 332 | 0.988 |
| 18 | 0.853 | 63 | 0.725 | 108 | 0.813 | 153 | 0.822 | 198 | 0.790 | 243 | 0.828 | 288 | 0.915 | 333 | 0.985 |
| 19 | 0.853 | 64 | 0.726 | 109 | 0.813 | 154 | 0.822 | 199 | 0.786 | 244 | 0.832 | 289 | 0.920 | 334 | 0.983 |
| 20 | 0.853 | 65 | 0.728 | 110 | 0.813 | 155 | 0.821 | 200 | 0.782 | 245 | 0.835 | 290 | 0.924 | 335 | 0.980 |
| 21 | 0.853 | 66 | 0.729 | 111 | 0.813 | 156 | 0.820 | 201 | 0.778 | 246 | 0.838 | 291 | 0.929 | 336 | 0.978 |
| 22 | 0.853 | 67 | 0.732 | 112 | 0.813 | 157 | 0.819 | 202 | 0.774 | 247 | 0.841 | 292 | 0.933 | 337 | 0.975 |
| 23 | 0.853 | 68 | 0.734 | 113 | 0.813 | 158 | 0.818 | 203 | 0.770 | 248 | 0.844 | 293 | 0.937 | 338 | 0.972 |
| 24 | 0.853 | 69 | 0.738 | 114 | 0.813 | 159 | 0.817 | 204 | 0.765 | 249 | 0.846 | 294 | 0.942 | 339 | 0.968 |
| 25 | 0.852 | 70 | 0.741 | 115 | 0.814 | 160 | 0.817 | 205 | 0.761 | 250 | 0.848 | 295 | 0.946 | 340 | 0.965 |
| 26 | 0.852 | 71 | 0.745 | 116 | 0.814 | 161 | 0.816 | 206 | 0.757 | 251 | 0.849 | 296 | 0.950 | 341 | 0.961 |
| 27 | 0.851 | 72 | 0.748 | 117 | 0.815 | 162 | 0.815 | 207 | 0.753 | 252 | 0.850 | 297 | 0.954 | 342 | 0.958 |
| 28 | 0.850 | 73 | 0.753 | 118 | 0.815 | 163 | 0.815 | 208 | 0.748 | 253 | 0.851 | 298 | 0.958 | 343 | 0.954 |
| 29 | 0.849 | 74 | 0.757 | 119 | 0.816 | 164 | 0.814 | 209 | 0.745 | 254 | 0.852 | 299 | 0.961 | 344 | 0.950 |
| 30 | 0.848 | 75 | 0.761 | 120 | 0.817 | 165 | 0.814 | 210 | 0.741 | 255 | 0.852 | 300 | 0.965 | 345 | 0.946 |
| 31 | 0.846 | 76 | 0.765 | 121 | 0.817 | 166 | 0.813 | 211 | 0.738 | 256 | 0.853 | 301 | 0.968 | 346 | 0.942 |
| 32 | 0.844 | 77 | 0.770 | 122 | 0.818 | 167 | 0.813 | 212 | 0.734 | 257 | 0.853 | 302 | 0.972 | 347 | 0.937 |
| 33 | 0.841 | 78 | 0.774 | 123 | 0.819 | 168 | 0.813 | 213 | 0.732 | 258 | 0.853 | 303 | 0.975 | 348 | 0.933 |
| 34 | 0.838 | 79 | 0.778 | 124 | 0.820 | 169 | 0.813 | 214 | 0.729 | 259 | 0.853 | 304 | 0.978 | 349 | 0.929 |
| 35 | 0.835 | 80 | 0.782 | 125 | 0.821 | 170 | 0.813 | 215 | 0.728 | 260 | 0.853 | 305 | 0.980 | 350 | 0.924 |
| 36 | 0.832 | 81 | 0.786 | 126 | 0.822 | 171 | 0.813 | 216 | 0.726 | 261 | 0.853 | 306 | 0.983 | 351 | 0.920 |
| 37 | 0.828 | 82 | 0.790 | 127 | 0.822 | 172 | 0.813 | 217 | 0.725 | 262 | 0.853 | 307 | 0.985 | 352 | 0.915 |
| 38 | 0.824 | 83 | 0.793 | 128 | 0.823 | 173 | 0.813 | 218 | 0.725 | 263 | 0.853 | 308 | 0.988 | 353 | 0.911 |
| 39 | 0.819 | 84 | 0.796 | 129 | 0.824 | 174 | 0.813 | 219 | 0.725 | 264 | 0.853 | 309 | 0.989 | 354 | 0.907 |
| 40 | 0.814 | 85 | 0.799 | 130 | 0.825 | 175 | 0.814 | 220 | 0.725 | 265 | 0.854 | 310 | 0.991 | 355 | 0.902 |
| 41 | 0.809 | 86 | 0.802 | 131 | 0.825 | 176 | 0.814 | 221 | 0.727 | 266 | 0.854 | 311 | 0.993 | 356 | 0.898 |
| 42 | 0.804 | 87 | 0.804 | 132 | 0.826 | 177 | 0.814 | 222 | 0.728 | 267 | 0.855 | 312 | 0.994 | 357 | 0.894 |
| 43 | 0.799 | 88 | 0.807 | 133 | 0.827 | 178 | 0.815 | 223 | 0.731 | 268 | 0.855 | 313 | 0.996 | 358 | 0.890 |
| 44 | 0.793 | 89 | 0.809 | 134 | 0.827 | 179 | 0.815 | 224 | 0.733 | 269 | 0.857 | 314 | 0.997 | 359 | 0.886 |

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