

TECHNICAL EXHIBIT  
APPLICATION FOR  
MINOR CHANGE IN LICENSED FACILITY  
AURIO A. MATOS BARRETO.  
FM TRANSLATOR STATION W279BU  
SAN JUAN, PUERTO RICO  
FACILITY ID 143465

AUGUST 8, 2014

CH 279 0.250 KW 552 M AMSL

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Technical Narrative

The technical exhibit, of which this narrative is part, has been prepared on behalf of Aurio A. Matos Barreto, licensee of FM translator station W279BU, Gurabo, Puerto Rico. W279BU is currently licensed as a “fill-in” translator of FM station WNVM. By means of this application, the licensee seeks construction permit for a minor change in the license facility of W279BU requesting a Mattoon waiver to associate W279BU as a fill-in translator of AM station WCMA, 1600 kHz, Bayamon, PR, Facility ID 39145, also licensed to Aurio A. Matos. Mr. Matos is also the licensee of FM translator W279BV, currently operating as a fill-in of AM station WCMA. Simultaneously with the filing of this application, an application is being filed to relocate W279BV as a fill-in of AM station WDNO. This application to relocate W279BU seeks to substitute the service improvement currently provided by W279BV to WCMA. This application is filed contingent to a grant of the application to modify W279BV.

FM translator station W279BU presently operates on channel 279 (103.7 MHz) with an effective radiated power (ERP) of 0.250 kW (250 watts), using a directional antenna system with vertical polarization. It is proposed to move W279BU to a new site and operate with an ERP of 0.250 kW (250 Watts) using a directional antenna with horizontal polarization, at a height of 52.4 meters AGL (552.5 meters AMSL) oriented at an azimuth of 0° True.

Proposed Transmitter Location

The proposed transmitting facility would use a Scala, Model CL-FM/HRM 50N, vertical stacked, 0.5 wavelength array consisting of three horizontally polarized directional antennas (FCC Antenna ID 16150), side-mounted on an existing self-support tower. The proposed translator location is described by the following NAD27 geographic coordinates:

18° 16' 49.3" North  
66° 06' 35.3" West

### Tower Registration

The FAA is not being notified of the proposed construction, as it is proposed to side-mount an FM antenna on an existing 55.5 meter (182 foot) self-support tower belonging to FM station WNVN that according to the TOWAIR program does not require registration.

### Quiet Zone Notification

As required by FCC rules pertaining to radio Quiet Zones, Section 73.1030(a), the National Astronomy and Ionosphere Center (NAIC) in Arecibo, Puerto Rico is being notified of this application. A copy of the notification letter to the Arecibo Observatory of the proposed facility is included herein as Appendix 1.

### FCC Monitoring Stations

FCC rules pertaining to FCC monitoring stations, Section 73.1030(c), requires that the proposed facility does not produce a field strength greater than 10 mV/m at the FCC stations. The closest FCC monitoring station to the proposed operation is located at Santa Isabel, PR, at a distance of 41 kilometers on a bearing of 223° True. The proposed operation will produce field strengths much lower than 10 mV/m at the FCC Santa Isabel, PR station.

### Environmental Considerations

The proposal is excluded from environmental processing, as an existing tower is to be employed and the proposal complies with the FCC Rules concerning human exposure to radio frequency (RF) energy. The proposal would not exceed 1% of the RF exposure limit for general population/uncontrolled environments for the frequency proposed. The calculation of RF energy at 2-m above ground was made under the procedures of OET Bulletin No. 65.\* The formula employed is as follows:

$$S = \frac{(33.4)F^2P}{R^2}$$

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\* Federal Communications Commission OET Bulletin No. 65, Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields (Edition 97-01, August 1997).

where,  $S$  = power density in  $\mu\text{W}/\text{cm}^2$ ,  $F$  = relative field factor at the angle to the calculation point,  $P$  = the total effective radiated power relative to a dipole in watts, and  $R$  = distance from the antenna radiation center to the calculation point in meters.

Based on the vertical radiation pattern of the proposed antenna, (Appendix 2), a relative field factor of 0.3 or less for any depression angle equal or greater than 30 degrees below horizon, a total effective radiated power of 250 watts and an antenna radiation center height above ground of 52 m, the calculated power density will not exceed  $0.3 \mu\text{W}/\text{cm}^2$ . Therefore, the calculated RF exposure at 2 m above ground will not exceed 0.15% of the limit of  $200 \mu\text{W}/\text{cm}^2$  for the general population and uncontrolled environments.

The antenna system shall be restricted from access and appropriate warning signs posted. In the event that personnel are required to climb the structure, the proposed FM translator transmissions shall be reduced or terminated as necessary to prevent RF exposure above the FCC recommended limits.

#### Allocation Considerations and Predicted Coverage Contour

Figure 2 summarizes the allocation study for the proposed facility. As indicated in Figure 2, the spacing requirements with respect to IF related facilities are met. The tabulation in Figure 2 also lists the results of a numerical analysis of the potential for contour overlap for all nearby co-channel and first-, second-, and third-adjacent-channel facilities. For the purposes of the numerical study, the maximum HAAT and maximum ERP values were used in determining the maximum distance in any direction to the predicted coverage and interfering contours.<sup>†</sup>

The predicted 60 dBu coverage contour was calculated in accordance with Section 73.313 of the FCC Rules. The average terrain elevations from 3 to 16 km from the proposed site were computed using the USGS 3-second terrain database. The distances to the predicted 60 dBu coverage contour for the proposed facilities were determined using the average elevations of radials spaced every 5-degrees of azimuth. The antenna radiation center height above average terrain and the ERP in each radial direction were used in conjunction with the propagation prediction curves of Section 73.333 to determine the distances to the contour.

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<sup>†</sup> Where the maximum HAAT figure was not available the radiation center height above mean sea level was employed as a worst-case estimate.

Waiver of Section 74.1233: as shown in Figure 3, there will not be 60 dBu contour overlap between the licensed and proposed W279BU operations. Therefore, a waiver of section 74.1233(a) is requested based on the waiver criteria (Mattoon waiver) established by the FCC in the letter dated September 2, 2011 (DA 11-1495) from Peter Doyle, Chief, Audio Division, Media Bureau to John Garziglia, Esq. concerning the application of W263AQ at Mattoon, Illinois (The Cromwell Group, Inc. of Illinois, BPFT-20101025ABR, Facility ID No. 85639). Specifically, in accordance with Mattoon waiver criteria, (1) W279BU has no history of filing serial modification applications to change markets, (2) will not preclude future licensing opportunities in the LPFM service and (3) its licensed and proposed operations will be mutually exclusive with one another. Figure 3 shows that the licensed and proposed W279BV operations are mutually exclusive.

Figure 3 shows the predicted 60 dBu coverage contour of the proposed translator facility and the licensed 2 mV/m coverage contour of station WCMA. As shown in Figure 3, the predicted 60 dBu coverage contour of the proposed translator facility is well within the 2 mV/m daytime contour of WCMA, the primary station to be retransmitted, and within a 25-mile radius of the WCMA transmitter site.

Figure 4, Sheets A to C is a depiction of the allocation situation with respect to the predicted protected contours of those stations close enough to warrant further study. This is based on the analysis in Figure 2, where there is an indication of the potential for prohibited overlapping contours. As shown in Figure 4A, the proposed facility does not involve prohibited contour overlap with the proposed facilities of W279BV

Figure 4B shows that there is no prohibitive overlap with respect to station WXLX. As shown in Figure 4C, while the predicted 54 dBu contour of stations WERR and WVJP-FM encompass the proposed transmitter site of W279BU, booster stations WERR-FM1, WVJP-FM1 and WVJP-FM2 will be properly protected.

With respect to WVJP-FM, processing pursuant to Section 73.1204(d) of the FCC Rules is requested. Specifically, it is demonstrated herein that the proposed translator facility will cause no harmful interference to WVJP-FM.

W279BU operates on Channel 279, second adjacent channel to WVJP-FM. The protection requirements of the undesired signal from W279BU is 40 dB higher than the desired signal of WVJP-FM. The proposed translator site is located 27.2 kilometers, at a bearing of 271 degrees true from station WVJP-FM, which operates on channel 277B with an omnidirectional antenna having an ERP of 26 kW and an HAAT of 596 meters along radial 271°. The predicted WVJP-FM F(50,50) field strength at the proposed site is 83.1dBu. Using the U/D ratio of 40 db contained in Section 74.1204, the proposed F(50,10) interfering signal is

123.1 dBu.<sup>‡</sup> The 123.1 dBu contour thus defines the maximum extent of predicted interference to WVJP-FM from the proposed translator facility.

Since an ERP of 250-watts is proposed, the 123.1 dBu signal contour is calculated by means of a free-space calculation. Based on free-space calculations, at no point anywhere near the proposed site would the 123.1 dBu contour reach a height less than 118 feet above ground level. This is graphically depicted in Figure 5B. Therefore, no predicted harmful interference to WVJP-FM will result as a result of the proposed translator facility.

Figure 5A is a table and Figure 5B a graphic representation showing the computed distances to the predicted 123.1 dBu contour under these assumptions. For these calculations, a non-directional horizontal antenna pattern and the antenna radiation center height above ground was used, though it should be noted that the proposed antenna is highly directional and given the complex topography of the terrain surrounding the site, the antenna height to the potentially affected inhabited structures is always significantly higher than the value used in these calculations. Appendix 2 shows the vertical antenna pattern data used for these calculations.

With respect to WERR, processing pursuant to Section 73.1204(d) of the FCC Rules is also requested. Specifically, it is demonstrated herein that the proposed translator facility will cause no harmful interference to WERR.

W279Bu operates on Channel 279, second adjacent channel to WERR. The protection requirements of the undesired signal from W279Bu is 40 dB higher than the desired signal of WERR. The proposed translator site is located 58.2 kilometers, at a bearing of 91 degrees true from station WERR, which operates on channel 281B with an omni directional antenna having an ERP of 50 kW and an HAAT of 303.3 meters along radial 91°. The predicted WERR F(50,50) field strength at the proposed site is 63.3 dBu. Using the U/D ratio of 40 db contained in Section 74.1204, the proposed F(50,10) interfering signal is 103.3 dBu. The 103.3 dBu contour thus defines the maximum extent of predicted interference to WERR from the proposed translator facility.

Since an ERP of 250-watts is proposed, the 103.3 dBu signal contour is calculated by means of a free-space calculation. Given the complex topography of the terrain surrounding the site, for the WERR interference calculations the directional horizontal antenna pattern and the antenna radiation center height relative to the potentially affected inhabited structures have been used. Figure 6 shows the area of the proposed site, WNVM at Cerro

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<sup>‡</sup> See In re Application of Living Way Ministries, Inc. for a Construction Permit for a New NCE FM Translator Station at Sun Valley, CA, File No. BPFT-19981001TA, FCC 02-244, Released: September 9, 2002

Marquesa, a well-known communication site housing several TV, FM and communication towers.

Seven distinct areas or locations are identified in Figure 6. Zone “A” in Figure 6 correspond to the area where the various communications facilities are housed. There are no residences or office structures within this area, but only structures which house TV, FM, and other communication equipment and towers belonging to broadcast stations and telecommunication companies which are occasionally visited by maintenance personnel. The Cerro Marquesa site is a secluded radio transmission area.

Zone “B” in Figure 6 consist of an arc of land where any residences located within this area will be located between a bearing of  $50^{\circ}$  and  $310^{\circ}$  true from the proposed W279BU horizontal antenna pattern. Along this arc, the maximum horizontal field value of the antenna is 0.25 at  $\pm 50^{\circ}$  from main lobe ( $0^{\circ}$ ), and significantly lower at greater azimuth deviations. The highest terrain elevation within this arc is 472 meters AMSL at a distance of 615 feet (the closest inhabited house) from the site, gradually decreasing with increasing distance from the site. Given that the proposed antenna radiation center will be at a height of 552.5 meters AMSL, the delta height for the calculations of field intensity from the proposed facility is 80.5 meters or 264 feet. Figure 7A is a table and Figure 7B a graphic representation showing the computed distances to the predicted 103.3 dBu contour under these assumptions. Appendix 2 shows the antenna pattern data used in the calculations. Based on these free-space calculations, at no point near the proposed site within the Zone B arc where inhabited structures could be present would the 103.3 dBu contour reach a height less than 132 feet above ground level. This is graphically depicted in Figure 7B.

Point “C” to Point “G” in Figure 6 represent the closest potentially inhabited locations closer to the main horizontal radiation lobe of the proposed antenna; to these locations correspond different terrain elevations and horizontal field values of the proposed antenna system, thus each location will be separately treated.

Point “C” in Figure 6 is located at a bearing of no less than  $10^{\circ}$  true from the proposed W279BU horizontal antenna pattern, corresponding to a horizontal field value of 0.95, at a distance of approximately 1,800 feet. The highest terrain elevation near this point is 382 meters AMSL, gradually decreasing with increasing distance from the site along this radial. Given that the proposed antenna radiation center will be at a height of 552.5 meters AMSL, the delta height for the calculations of field intensity from the proposed facility is 170.5 meters or 559 feet. Figure 8A is a table and Figure 8B a graphic representation showing the computed distances to the predicted 103.3 dBu contour under these assumptions based on



the antenna pattern data shown in Appendix 2. Based on these free-space calculations, at no point near Point “C” or along this radial where inhabited structures could be present would the 103.3 dBu contour reach a height less than 59 feet above ground level. This is graphically depicted in Figure 8B.

Point “D” in Figure 6 is located at a bearing of no less than 17° true from the proposed W279BU horizontal antenna pattern, corresponding to a horizontal field value of 0.865, at a distance of approximately 1,710 feet. The highest terrain elevation near this point is 408 meters AMSL, gradually decreasing with increasing distance from the site along this radial. Given that the proposed antenna radiation center will be at a height of 552.5 meters AMSL, the delta height for the calculations of field intensity from the proposed facility is 144.5 meters or 474 feet. Figure 9A is a table and Figure 9B a graphic representation showing the computed distances to the predicted 103.3 dBu contour under these assumptions based on the antenna pattern data shown in Appendix 2. Based on these free-space calculations, at no point near Point “D” or along this radial where inhabited structures could be present would the 103.3 dBu contour reach a height less than 53 feet above ground level. This is shown in Figure 9A and graphically depicted in Figure 9B.

Point “E” in Figure 6 is located at a bearing of no less than 20° true from the proposed W279BU horizontal antenna pattern, corresponding to a horizontal field value of 0.82, at a distance of approximately 1,750 feet. The highest terrain elevation near this point is 411 meters AMSL, gradually decreasing with increasing distance from the site along this radial. Given that the proposed antenna radiation center will be at a height of 552.5 meters AMSL, the delta height for the calculations of field intensity from the proposed facility is 141.5 meters or 464 feet. Figure 10A is a table and Figure 10B a graphic representation showing the computed distances to the predicted 103.3 dBu contour under these assumptions based on the antenna pattern data shown in Appendix 2. Based on these free-space calculations, at no point near Point “E” or along this radial where inhabited structures could be present would the 103.3 dBu contour reach a height less than 98 feet above ground level. This is shown in Figure 10A and graphically depicted in Figure 10B.

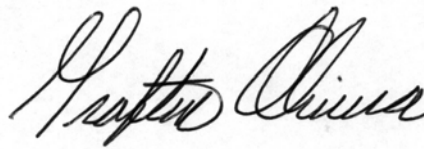
Point “F” in Figure 6 is located at a bearing of no less than 25° true from the proposed W279BU horizontal antenna pattern, corresponding to a horizontal field value of 0.735, at a distance of approximately 1,700 feet. The highest terrain elevation near this point is 400 meters AMSL, gradually decreasing with increasing distance from the site along this radial. Given that the proposed antenna radiation center will be at a height of 552.5 meters AMSL, the delta height for the calculations of field intensity from the proposed facility is 172.5 meters or 500 feet. Figure 11A is a table and Figure 11B a graphic representation showing the computed distances to the predicted 103.3 dBu contour under these assumptions based on the antenna pattern data shown in Appendix 2. Based on these free-space

calculations, at no point near Point “F” or along this radial where inhabited structures could be present would the 103.3 dBu contour reach a height less than 113 feet above ground level. This is shown in Figure 11A and graphically depicted in Figure 11B.

Point “G” in Figure 6 is located at a bearing of no less than  $41^{\circ}$  true from the proposed W279BU horizontal antenna pattern, corresponding to a horizontal field value of 0.470, at a distance of approximately 1,600 feet. The highest terrain elevation near this point is 410 meters AMSL, gradually decreasing with increasing distance from the site along this radial. Given that the proposed antenna radiation center will be at a height of 552.5 meters AMSL, the delta height for the calculations of field intensity from the proposed facility is 142.5 meters or 467 feet. Figure 12A is a table and Figure 12B a graphic representation showing the computed distances to the predicted 103.3 dBu contour under these assumptions based on the antenna pattern data shown in Appendix 2. Based on these free-space calculations, at no point near Point “G” or along this radial where inhabited structures could be present would the 103.3 dBu contour reach a height less than 220 feet above ground level. This is shown in Figure 12A and graphically depicted in Figure 12B.

Based on the preceding analysis, no harmful interference to WERR will result as a result of the proposed translator facility.

For all the reasons stated above, it is believed that the proposed facility is in compliance with applicable FCC Rules and Regulations.



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Engineering Specifications

|                                    |  |
|------------------------------------|--|
| Channel / Frequency                | 279A / 103.7 MHz   |
| Site Coordinates (NAD27)           | 18° 16' 49.3" North Latitude<br>66° 06' 35.3" West Longitude |
| Antenna structure Registration     | N/A  |
| Height of antenna radiation center | 52.4 m AGL / 552.5 AMSL                                      |
| Antenna radiation center HAAT      | 333 m  |
| Transmitter                        | RVR, PJ-50 M   |
| Transmitter power output           | 0.024 kW   |
| Transmission line                  | Andrew, LDF5-50A   |
| Transmission line length           | 60 m   |
| Transmission line efficiency       | 84.3 %   |
| Antenna                            | Scala CL-FM/HRM Custom Array                                 |
| Polarization                       | Horizontal   |
| Power gain                         | 12.3   |
| Antenna input power                | 0.02 kW  |
| Effective radiated power           | 0.25 kW (Vert. MAX-DA)                                       |

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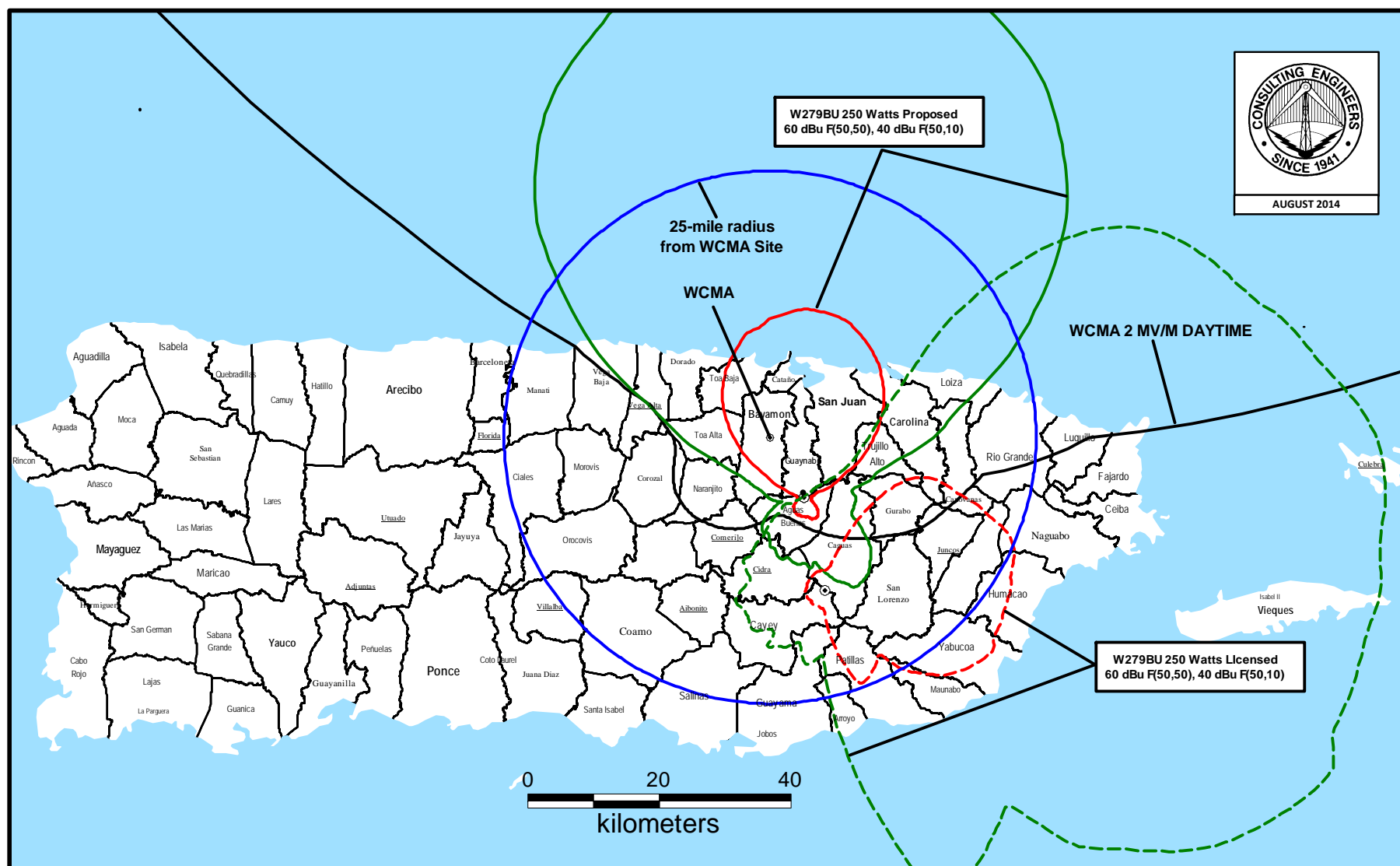
Summary of Allocation Analysis

Channel: 279 Coordinates: 018-16-49.3 066-06-35.3 (NAD 27)  
Class: A Buffer Distance: 50 km

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| Callsign | Status | Chan.    | Serv. | Freq. | City      |         | State   | Latitude  | Dist.(km)   | Sep.(km)   | Spacing(km) |         |
|----------|--------|----------|-------|-------|-----------|---------|---------|-----------|-------------|------------|-------------|---------|
| Fac. ID  | ARN    |          |       | Class | DA        | Ant. ID | ERP(kW) | HAAT(m)   | Longitude   | Bear.(deg) | 73.215      | Comment |
| W225AY   | LIC    | 225      | FX    | 92.9  | ARROYO    |         | PR      | 018-00-36 | 31.25       |            |             |         |
| 157296   | BLFT   | 20071228 | ABO   | D     | C         | 67340   | 0.05    |           | 066-01-28.4 | 163.31     |             | INFO    |
| WYQE     | LIC    | 225      | FM    | 92.9  | NAGUABO   |         | PR      | 018-16-50 | 46.47       | 10         | 36.47       |         |
| 19056    | BLH    | 19950106 | KB    | A     | N         |         | 3.9     | 229       | 065-40-13   | 89.9       |             | CLEAR   |
| W276AI   | LIC    | 276      | FX    | 103.1 | PONCE     |         | PR      | 018-00-00 | 62.32       |            |             |         |
| 53553    | BLFT   | 19860609 | TH    | D     | D         | 13702   | 0.004   |           | 066-37-14   | 240.07     |             | INFO    |
| WVJP-FM  | CP     | 277      | FM    | 103.3 | CAGUAS    |         | PR      | 018-16-41 | 27.12       | 69         | -41.88      |         |
| 6441     | BPH    | 20140521 | AGV   | B     | N         |         | 26      | 592       | 065-51-12   | 90.5       | 63 N        | SHORT   |
| WVJP-FM  | LIC    | 277      | FM    | 103.3 | CAGUAS    |         | PR      | 018-16-41 | 27.21       | 69         | -41.79      |         |
| 6441     | BLH    | 19890331 | KI    | B     |           |         | 28      | 581       | 065-51-09   | 90.5       | 63 N        | SHORT   |
| W279BV   | LIC    | 279      | FX    | 103.7 | SAN JUAN  |         | PR      | 018-17-42 | 6.11        |            |             |         |
| 26656    | BLFT   | 20140507 | ACX   | D     | D         | 16150   | 0.225   |           | 066-09-56   | 285.47     |             | INFO    |
| W279BU   | LIC    | 279      | FX    | 103.7 | GURABO    |         | PR      | 018-09-17 | 14.25       |            |             |         |
| 143465   | BLFT   | 20140303 | AEF   | D     | D         | 16151   | 0.25    |           | 066-04-50   | 167.53     |             | INFO    |
| WXLX     | LIC    | 279      | FM    | 103.7 | LAJAS     |         | PR      | 017-59-37 | 118.21      | 178        | -59.79      |         |
| 55065    | BLH    | 19940113 | KE    | B     | N         |         | 50      | 139       | 067-11-09   | 254.5      | 143 N       | SHORT   |
| WERR     | LIC    | 281      | FM    | 104.1 | VEGA ALTA |         | PR      | 018-17-29 | 58.28       | 69         | -10.72      |         |
| 54750    | BLH    | 20080708 | AJO   | B     | N         |         | 50      | 301       | 066-39-39   | 271.29     | 63 N        | SHORT   |

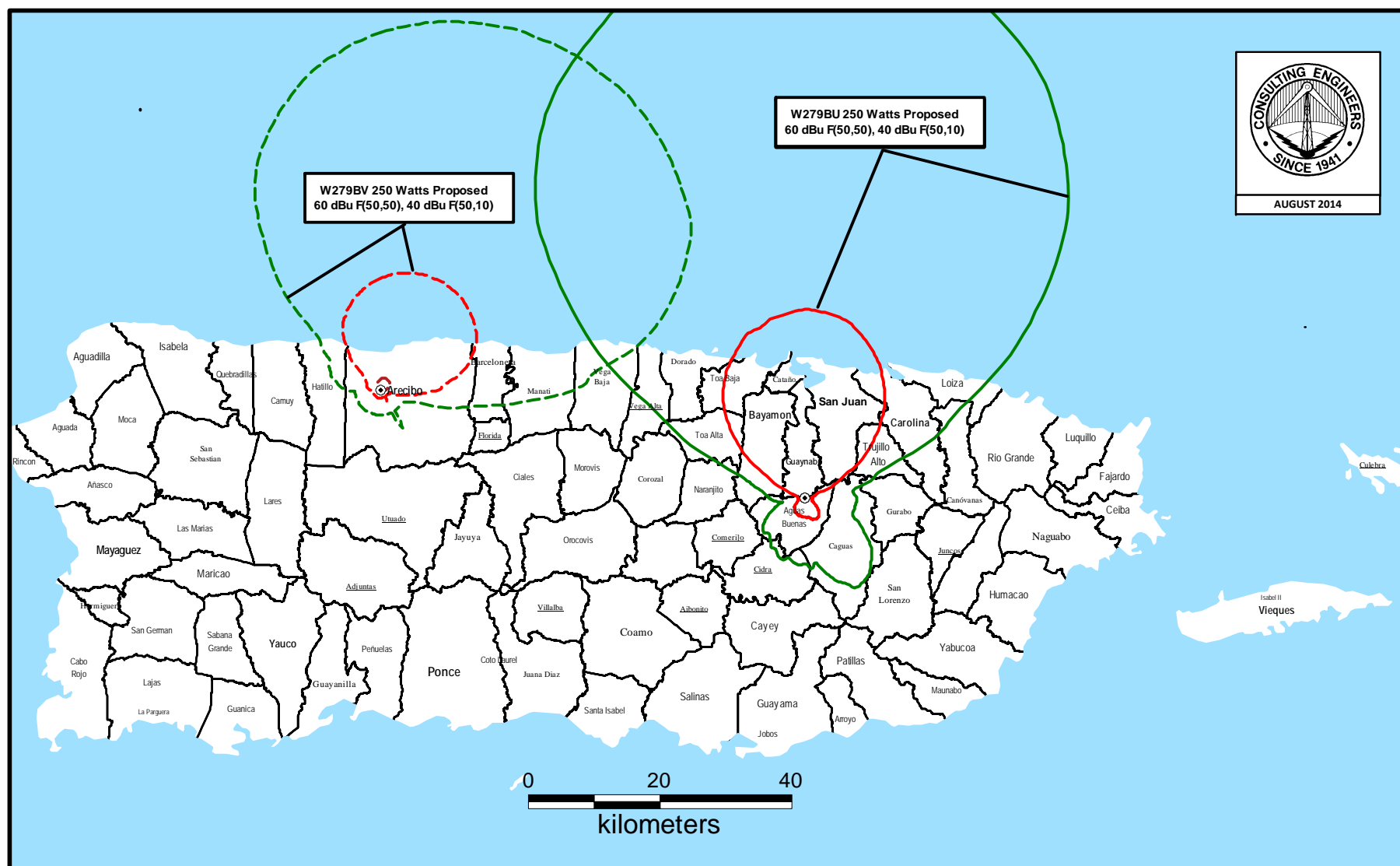
Figure 3



### **PREDICTED COVERAGE CONTOURS**

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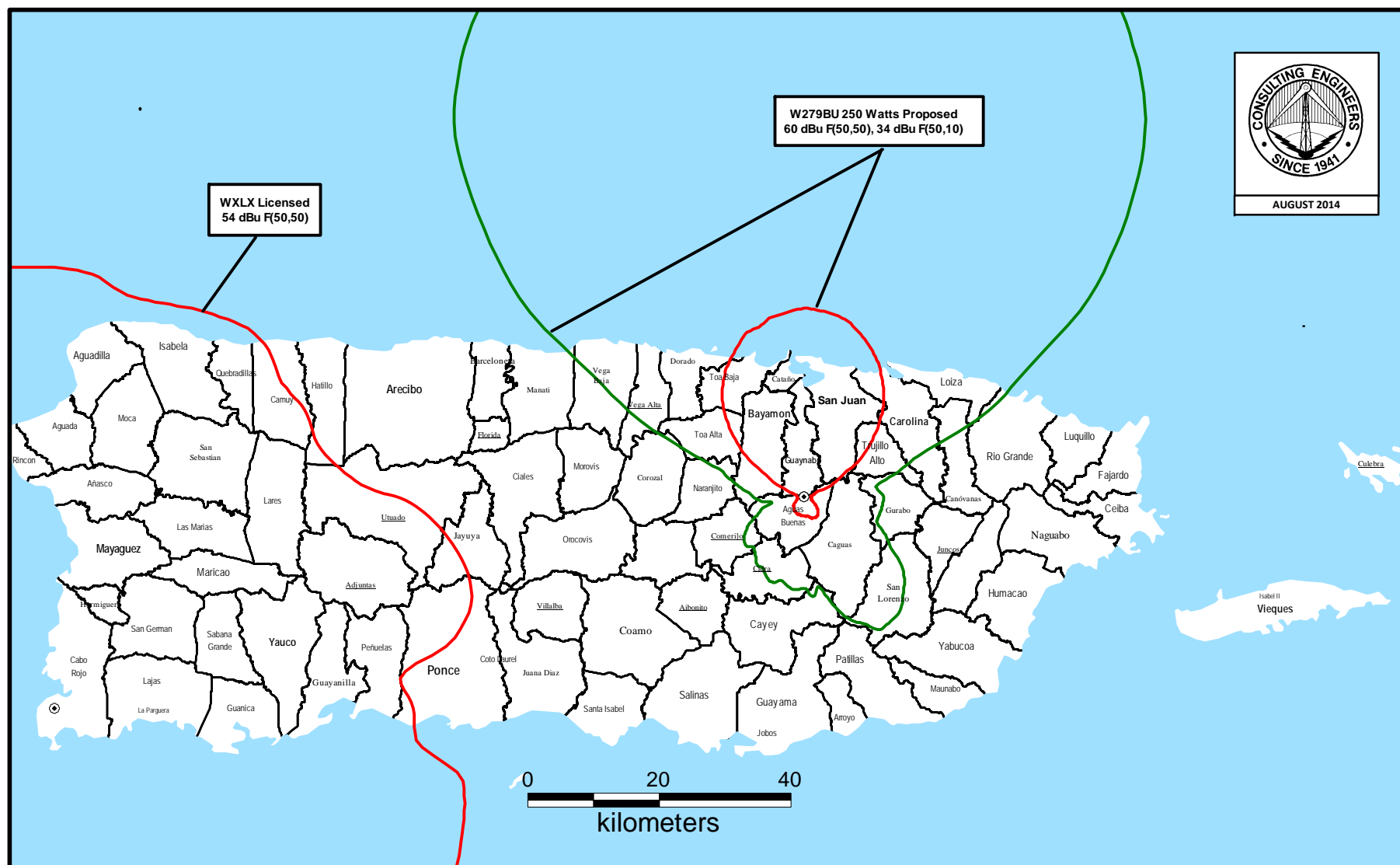
Figure 4A



# **PROPOSED ALLOCATION SITUATION**

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Figure 4B



## PROPOSED ALLOCATION SITUATION

LICENSE MOD. APPLICATION

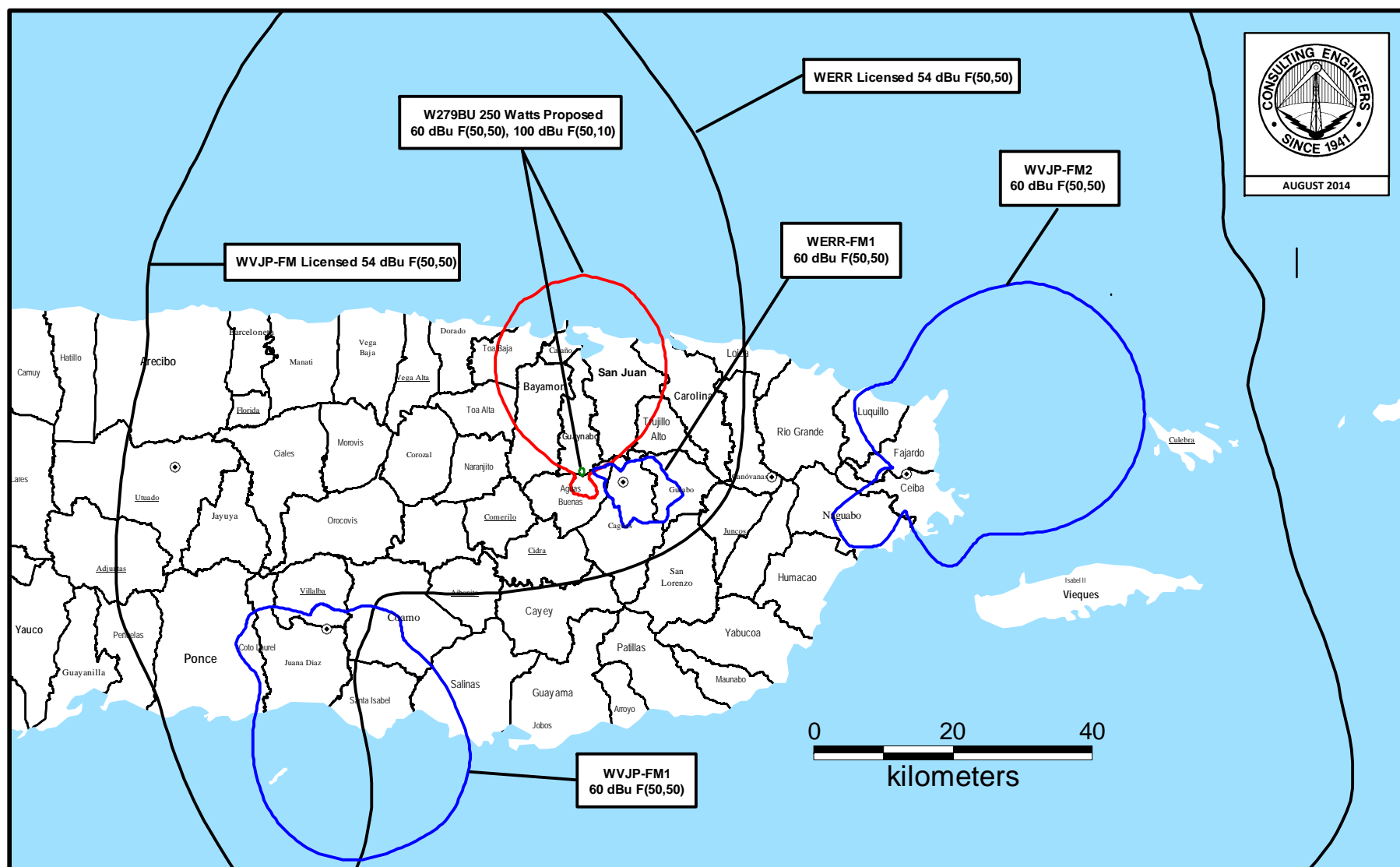
FM TRANSLATOR W279BU

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Figure 4C



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du Treil, Lundin & Rackley, Inc. Sarasota, Florida



Figure 5A

## Interfering Field Strength Vs. Distance Graph - W279BU to WVJP-FM

|                     |   |  |     |                 |  |  |  |
|---------------------|---|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelenth |  |     |                 |  |  |  |
| RCAGL               | 172 feet  |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 123.1 dBu   |  |     | -6.02059991 dBk |  |  |  |

172'+0'=172'

500 MTS AMSL TERRAIN ELEV.

| Depression Angle | VRF   | HRF  | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 0                   | 169               |
| 89               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 0                   | 169               |
| 88               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 0                   | 169               |
| 87               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 0                   | 169               |
| 86               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 0                   | 169               |
| 85               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 0                   | 169               |
| 84               | 0.011 | 1.00 | -45.2     | 0.9                       | 3                            | 0                   | 169               |
| 83               | 0.013 | 1.00 | -43.7     | 1.0                       | 3                            | 0                   | 169               |
| 82               | 0.014 | 1.00 | -43.1     | 1.1                       | 4                            | 1                   | 168               |
| 81               | 0.015 | 1.00 | -42.5     | 1.2                       | 4                            | 1                   | 168               |
| 80               | 0.017 | 1.00 | -41.4     | 1.4                       | 4                            | 1                   | 168               |
| 79               | 0.021 | 1.00 | -39.6     | 1.7                       | 6                            | 1                   | 167               |
| 78               | 0.025 | 1.00 | -38.1     | 2.0                       | 7                            | 1                   | 166               |
| 77               | 0.028 | 1.00 | -37.1     | 2.2                       | 7                            | 2                   | 165               |
| 76               | 0.032 | 1.00 | -35.9     | 2.6                       | 8                            | 2                   | 164               |
| 75               | 0.036 | 1.00 | -34.9     | 2.9                       | 9                            | 2                   | 163               |
| 74               | 0.041 | 1.00 | -33.8     | 3.3                       | 11                           | 3                   | 162               |
| 73               | 0.046 | 1.00 | -32.8     | 3.7                       | 12                           | 4                   | 160               |
| 72               | 0.051 | 1.00 | -31.9     | 4.1                       | 13                           | 4                   | 159               |
| 71               | 0.056 | 1.00 | -31.1     | 4.5                       | 15                           | 5                   | 158               |
| 70               | 0.061 | 1.00 | -30.3     | 4.9                       | 16                           | 5                   | 157               |
| 69               | 0.068 | 1.00 | -29.4     | 5.5                       | 18                           | 6                   | 155               |
| 68               | 0.074 | 1.00 | -28.6     | 5.9                       | 19                           | 7                   | 154               |
| 67               | 0.08  | 1.00 | -28.0     | 6.4                       | 21                           | 8                   | 153               |
| 66               | 0.086 | 1.00 | -27.3     | 6.9                       | 23                           | 9                   | 151               |
| 65               | 0.091 | 1.00 | -26.8     | 7.3                       | 24                           | 10                  | 150               |
| 64               | 0.095 | 1.00 | -26.5     | 7.6                       | 25                           | 11                  | 150               |
| 63               | 0.099 | 1.00 | -26.1     | 7.9                       | 26                           | 12                  | 149               |
| 62               | 0.102 | 1.00 | -25.8     | 8.2                       | 27                           | 13                  | 148               |
| 61               | 0.105 | 1.00 | -25.6     | 8.4                       | 28                           | 13                  | 148               |
| 60               | 0.107 | 1.00 | -25.4     | 8.6                       | 28                           | 14                  | 148               |
| 59               | 0.108 | 1.00 | -25.4     | 8.7                       | 28                           | 15                  | 148               |
| 58               | 0.109 | 1.00 | -25.3     | 8.7                       | 29                           | 15                  | 148               |
| 57               | 0.109 | 1.00 | -25.3     | 8.7                       | 29                           | 16                  | 148               |
| 56               | 0.108 | 1.00 | -25.4     | 8.7                       | 28                           | 16                  | 148               |
| 55               | 0.107 | 1.00 | -25.4     | 8.6                       | 28                           | 16                  | 149               |
| 54               | 0.105 | 1.00 | -25.6     | 8.4                       | 28                           | 16                  | 150               |
| 53               | 0.102 | 1.00 | -25.8     | 8.2                       | 27                           | 16                  | 151               |
| 52               | 0.098 | 1.00 | -26.2     | 7.9                       | 26                           | 16                  | 152               |
| 51               | 0.093 | 1.00 | -26.7     | 7.5                       | 24                           | 15                  | 153               |
| 50               | 0.088 | 1.00 | -27.1     | 7.1                       | 23                           | 15                  | 154               |
| 49               | 0.081 | 1.00 | -27.9     | 6.5                       | 21                           | 14                  | 156               |
| 48               | 0.073 | 1.00 | -28.8     | 5.9                       | 19                           | 13                  | 158               |
| 47               | 0.064 | 1.00 | -29.9     | 5.1                       | 17                           | 11                  | 160               |

| Depression Angle | VRF   | HRF  | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 1.00 | -31.2     | 4.4                       | 14                           | 10                  | 162               |
| 45               | 0.043 | 1.00 | -33.4     | 3.4                       | 11                           | 8                   | 164               |
| 44               | 0.031 | 1.00 | -36.2     | 2.5                       | 8                            | 6                   | 166               |
| 43               | 0.018 | 1.00 | -40.9     | 1.4                       | 5                            | 3                   | 169               |
| 42               | 0.01  | 1.00 | -46.0     | 0.8                       | 3                            | 2                   | 170               |
| 41               | 0.013 | 1.00 | -43.7     | 1.0                       | 3                            | 3                   | 170               |
| 40               | 0.031 | 1.00 | -36.2     | 2.5                       | 8                            | 6                   | 167               |
| 39               | 0.049 | 1.00 | -32.2     | 3.9                       | 13                           | 10                  | 164               |
| 38               | 0.069 | 1.00 | -29.2     | 5.5                       | 18                           | 14                  | 161               |
| 37               | 0.09  | 1.00 | -26.9     | 7.2                       | 24                           | 19                  | 158               |
| 36               | 0.113 | 1.00 | -25.0     | 9.1                       | 30                           | 24                  | 155               |
| 35               | 0.136 | 1.00 | -23.3     | 10.9                      | 36                           | 29                  | 151               |
| 34               | 0.161 | 1.00 | -21.9     | 12.9                      | 42                           | 35                  | 148               |
| 33               | 0.187 | 1.00 | -20.6     | 15.0                      | 49                           | 41                  | 145               |
| 32               | 0.215 | 1.00 | -19.4     | 17.2                      | 57                           | 48                  | 142               |
| 31               | 0.243 | 1.00 | -18.3     | 19.5                      | 64                           | 55                  | 139               |
| 30               | 0.273 | 1.00 | -17.3     | 21.9                      | 72                           | 62                  | 136               |
| 29               | 0.303 | 1.00 | -16.4     | 24.3                      | 80                           | 70                  | 133               |
| 28               | 0.333 | 1.00 | -15.6     | 26.7                      | 88                           | 77                  | 131               |
| 27               | 0.365 | 1.00 | -14.8     | 29.3                      | 96                           | 86                  | 128               |
| 26               | 0.398 | 1.00 | -14.0     | 31.9                      | 105                          | 94                  | 126               |
| 25               | 0.431 | 1.00 | -13.3     | 34.5                      | 113                          | 103                 | 124               |
| 24               | 0.464 | 1.00 | -12.7     | 37.2                      | 122                          | 111                 | 122               |
| 23               | 0.496 | 1.00 | -12.1     | 39.8                      | 130                          | 120                 | 121               |
| 22               | 0.53  | 1.00 | -11.5     | 42.5                      | 139                          | 129                 | 120               |
| 21               | 0.563 | 1.00 | -11.0     | 45.1                      | 148                          | 138                 | 119               |
| 20               | 0.596 | 1.00 | -10.5     | 47.8                      | 157                          | 147                 | 118               |
| 19               | 0.629 | 1.00 | -10.0     | 50.4                      | 165                          | 156                 | 118               |
| 18               | 0.661 | 1.00 | -9.6      | 53.0                      | 174                          | 165                 | 118               |
| 17               | 0.692 | 1.00 | -9.2      | 55.5                      | 182                          | 174                 | 119               |
| 16               | 0.724 | 1.00 | -8.8      | 58.0                      | 190                          | 183                 | 120               |
| 15               | 0.754 | 1.00 | -8.5      | 60.4                      | 198                          | 192                 | 121               |
| 14               | 0.782 | 1.00 | -8.2      | 62.7                      | 206                          | 200                 | 122               |
| 13               | 0.81  | 1.00 | -7.9      | 64.9                      | 213                          | 208                 | 124               |
| 12               | 0.836 | 1.00 | -7.6      | 67.0                      | 220                          | 215                 | 126               |
| 11               | 0.861 | 1.00 | -7.3      | 69.0                      | 226                          | 222                 | 129               |
| 10               | 0.885 | 1.00 | -7.1      | 70.9                      | 233                          | 229                 | 132               |
| 9                | 0.905 | 1.00 | -6.9      | 72.5                      | 238                          | 235                 | 135               |
| 8                | 0.924 | 1.00 | -6.7      | 74.1                      | 243                          | 241                 | 138               |
| 7                | 0.94  | 1.00 | -6.6      | 75.4                      | 247                          | 245                 | 142               |
| 6                | 0.956 | 1.00 | -6.4      | 76.6                      | 251                          | 250                 | 146               |
| 5                | 0.969 | 1.00 | -6.3      | 77.7                      | 255                          | 254                 | 150               |
| 4                | 0.979 | 1.00 | -6.2      | 78.5                      | 257                          | 257                 | 154               |
| 3                | 0.987 | 1.00 | -6.1      | 79.1                      | 260                          | 259                 | 158               |
| 2                | 0.994 | 1.00 | -6.1      | 79.7                      | 261                          | 261                 | 163               |
| 1                | 0.997 | 1.00 | -6.0      | 79.9                      | 262                          | 262                 | 167               |
| 0                | 1     | 1.00 | -6.0      | 80.2                      | 263                          | 263                 | 172               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 118

Figure 5B

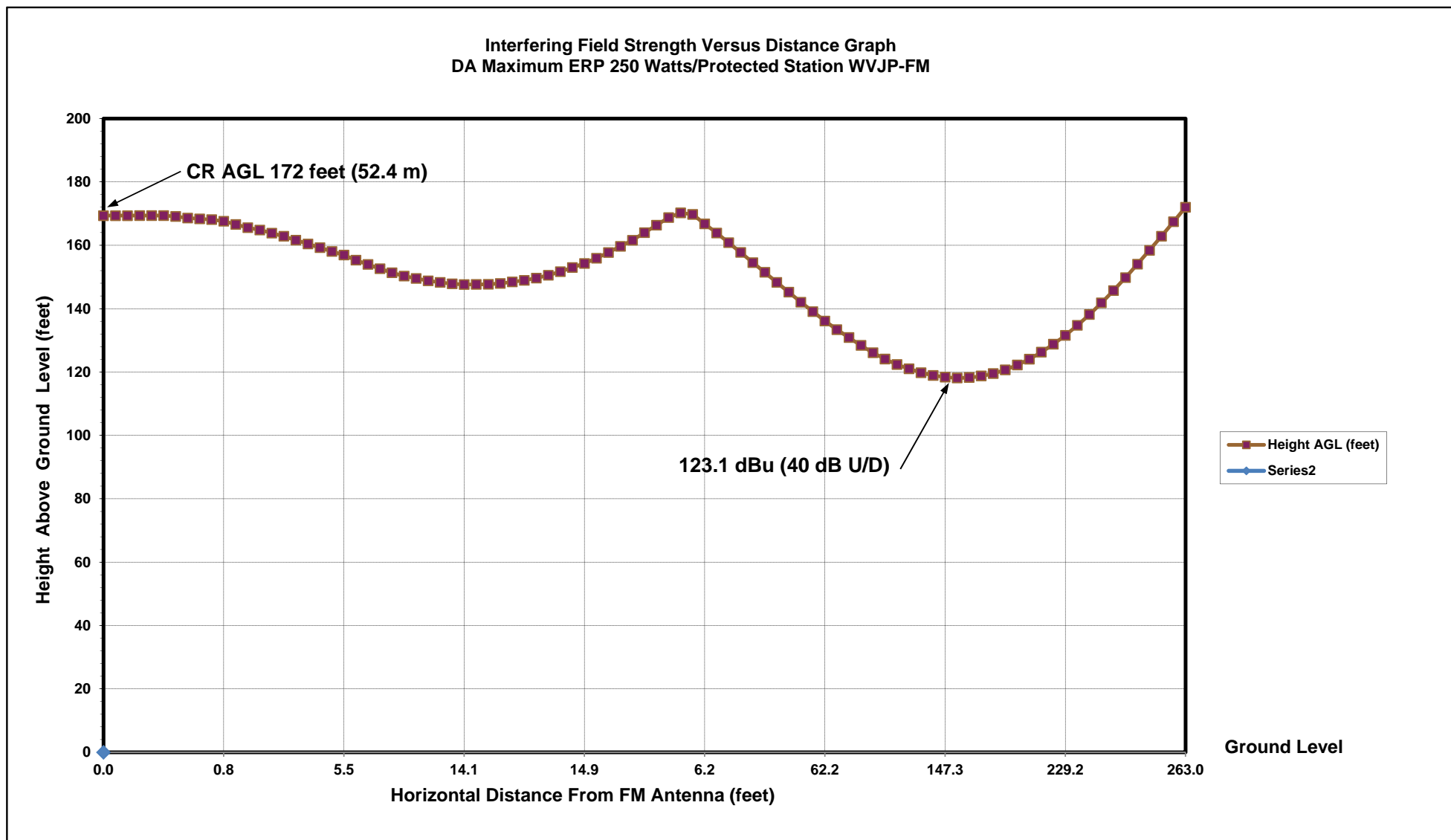
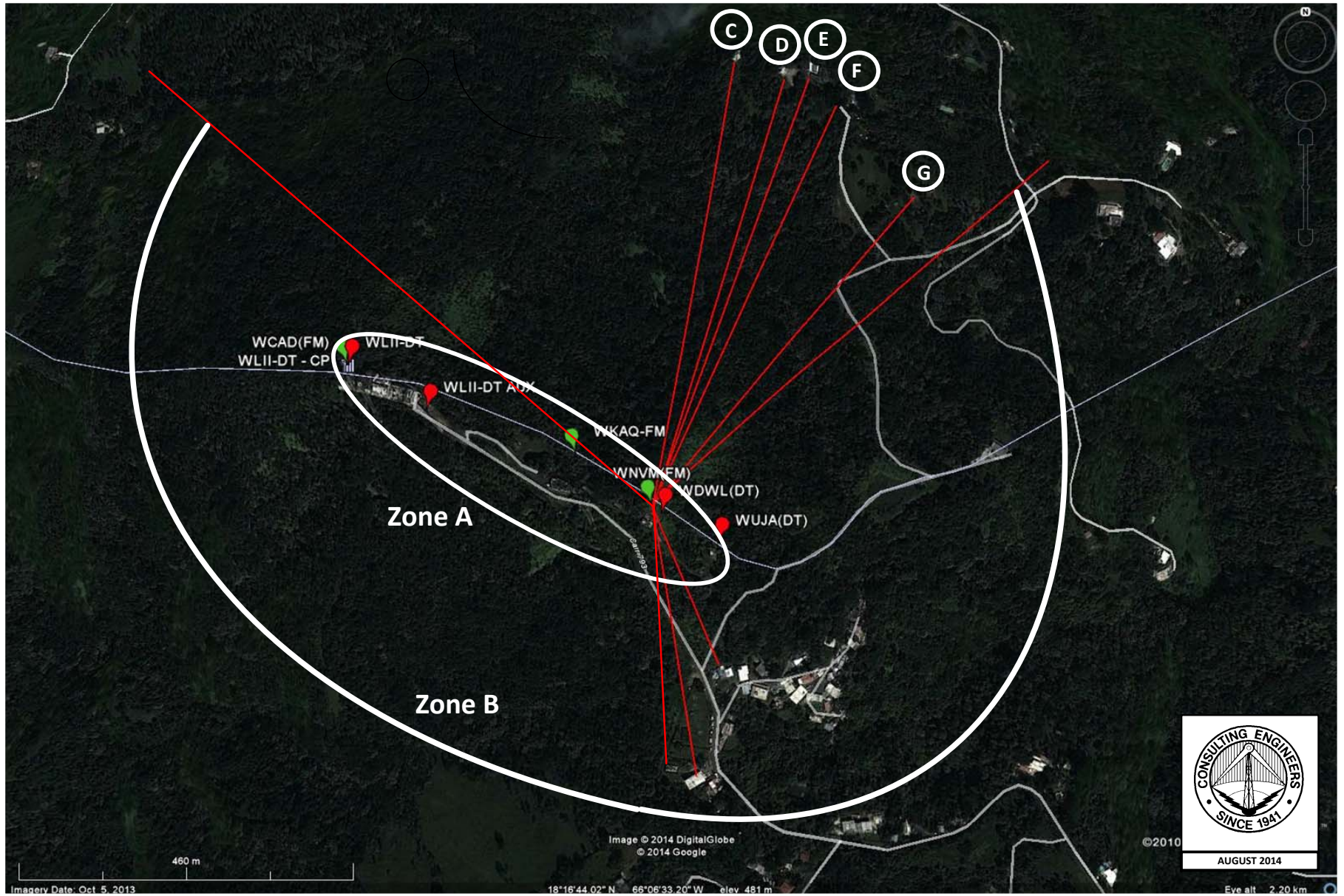


Figure 6



**PROPOSED SITE – CERRO MARQUESA**  
LICENSE MOD. APPLICATION  
FM TRANSLATOR W279BU - SAN JUAN, PUERTO RICO  
CH 279 0.25 KW 552.5 M AMSL  
du Treil, Lundin & Rackley, Inc. Sarasota, Florida

Figure 7A

## Interfering Field Strength Vs. Distance Graph - W279BU to WERR (FM) - Zone B of Figure 6

|                     |  |  |     |                 |  |  |  |
|---------------------|--|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelength |  |     |                 |  |  |  |
| RCAGL               | 264 feet   |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 103.3 dBu  |  |     | -6.02059991 dBk |  |  |  |

172'+92'=264'

472 MTS AMSL TERRAIN ELEV.

| Depression Angle | VRF   | HRF  | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 0                   | 258               |
| 89               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 0                   | 258               |
| 88               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 0                   | 258               |
| 87               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 0                   | 258               |
| 86               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 0                   | 258               |
| 85               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 1                   | 258               |
| 84               | 0.011 | 0.25 | -57.2     | 2.2                       | 7                            | 1                   | 257               |
| 83               | 0.013 | 0.25 | -55.8     | 2.5                       | 8                            | 1                   | 256               |
| 82               | 0.014 | 0.25 | -55.1     | 2.7                       | 9                            | 1                   | 255               |
| 81               | 0.015 | 0.25 | -54.5     | 2.9                       | 10                           | 2                   | 254               |
| 80               | 0.017 | 0.25 | -53.5     | 3.3                       | 11                           | 2                   | 253               |
| 79               | 0.021 | 0.25 | -51.6     | 4.1                       | 13                           | 3                   | 251               |
| 78               | 0.025 | 0.25 | -50.1     | 4.9                       | 16                           | 3                   | 248               |
| 77               | 0.028 | 0.25 | -49.1     | 5.5                       | 18                           | 4                   | 246               |
| 76               | 0.032 | 0.25 | -48.0     | 6.3                       | 21                           | 5                   | 244               |
| 75               | 0.036 | 0.25 | -46.9     | 7.1                       | 23                           | 6                   | 242               |
| 74               | 0.041 | 0.25 | -45.8     | 8.0                       | 26                           | 7                   | 239               |
| 73               | 0.046 | 0.25 | -44.8     | 9.0                       | 30                           | 9                   | 236               |
| 72               | 0.051 | 0.25 | -43.9     | 10.0                      | 33                           | 10                  | 233               |
| 71               | 0.056 | 0.25 | -43.1     | 11.0                      | 36                           | 12                  | 230               |
| 70               | 0.061 | 0.25 | -42.4     | 11.9                      | 39                           | 13                  | 227               |
| 69               | 0.068 | 0.25 | -41.4     | 13.3                      | 44                           | 16                  | 223               |
| 68               | 0.074 | 0.25 | -40.7     | 14.5                      | 48                           | 18                  | 220               |
| 67               | 0.080 | 0.25 | -40.0     | 15.7                      | 51                           | 20                  | 217               |
| 66               | 0.086 | 0.25 | -39.4     | 16.8                      | 55                           | 22                  | 214               |
| 65               | 0.091 | 0.25 | -38.9     | 17.8                      | 58                           | 25                  | 211               |
| 64               | 0.095 | 0.25 | -38.5     | 18.6                      | 61                           | 27                  | 209               |
| 63               | 0.099 | 0.25 | -38.1     | 19.4                      | 64                           | 29                  | 207               |
| 62               | 0.102 | 0.25 | -37.9     | 20.0                      | 66                           | 31                  | 206               |
| 61               | 0.105 | 0.25 | -37.6     | 20.6                      | 67                           | 33                  | 205               |
| 60               | 0.107 | 0.25 | -37.5     | 21.0                      | 69                           | 34                  | 204               |
| 59               | 0.108 | 0.25 | -37.4     | 21.2                      | 69                           | 36                  | 205               |
| 58               | 0.109 | 0.25 | -37.3     | 21.3                      | 70                           | 37                  | 205               |
| 57               | 0.109 | 0.25 | -37.3     | 21.3                      | 70                           | 38                  | 205               |
| 56               | 0.108 | 0.25 | -37.4     | 21.2                      | 69                           | 39                  | 206               |
| 55               | 0.107 | 0.25 | -37.5     | 21.0                      | 69                           | 39                  | 208               |
| 54               | 0.105 | 0.25 | -37.6     | 20.6                      | 67                           | 40                  | 209               |
| 53               | 0.102 | 0.25 | -37.9     | 20.0                      | 66                           | 39                  | 212               |
| 52               | 0.098 | 0.25 | -38.2     | 19.2                      | 63                           | 39                  | 214               |
| 51               | 0.093 | 0.25 | -38.7     | 18.2                      | 60                           | 38                  | 218               |
| 50               | 0.088 | 0.25 | -39.2     | 17.2                      | 57                           | 36                  | 221               |
| 49               | 0.081 | 0.25 | -39.9     | 15.9                      | 52                           | 34                  | 225               |
| 48               | 0.073 | 0.25 | -40.8     | 14.3                      | 47                           | 31                  | 229               |
| 47               | 0.064 | 0.25 | -41.9     | 12.5                      | 41                           | 28                  | 234               |



| Depression Angle | VRF   | HRF  | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 0.25 | -43.3     | 10.8                      | 35                           | 25                  | 239               |
| 45               | 0.043 | 0.25 | -45.4     | 8.4                       | 28                           | 20                  | 244               |
| 44               | 0.031 | 0.25 | -48.2     | 6.1                       | 20                           | 14                  | 250               |
| 43               | 0.018 | 0.25 | -53.0     | 3.5                       | 12                           | 8                   | 256               |
| 42               | 0.010 | 0.25 | -58.1     | 2.0                       | 6                            | 5                   | 260               |
| 41               | 0.013 | 0.25 | -55.8     | 2.5                       | 8                            | 6                   | 259               |
| 40               | 0.031 | 0.25 | -48.2     | 6.1                       | 20                           | 15                  | 251               |
| 39               | 0.049 | 0.25 | -44.3     | 9.6                       | 31                           | 24                  | 244               |
| 38               | 0.069 | 0.25 | -41.3     | 13.5                      | 44                           | 35                  | 237               |
| 37               | 0.090 | 0.25 | -39.0     | 17.6                      | 58                           | 46                  | 229               |
| 36               | 0.113 | 0.25 | -37.0     | 22.1                      | 73                           | 59                  | 221               |
| 35               | 0.136 | 0.25 | -35.4     | 26.6                      | 87                           | 72                  | 214               |
| 34               | 0.161 | 0.25 | -33.9     | 31.5                      | 103                          | 86                  | 206               |
| 33               | 0.187 | 0.25 | -32.6     | 36.6                      | 120                          | 101                 | 199               |
| 32               | 0.215 | 0.25 | -31.4     | 42.1                      | 138                          | 117                 | 191               |
| 31               | 0.243 | 0.25 | -30.3     | 47.6                      | 156                          | 134                 | 184               |
| 30               | 0.273 | 0.25 | -29.3     | 53.5                      | 175                          | 152                 | 176               |
| 29               | 0.303 | 0.25 | -28.4     | 59.3                      | 195                          | 170                 | 170               |
| 28               | 0.333 | 0.25 | -27.6     | 65.2                      | 214                          | 189                 | 164               |
| 27               | 0.365 | 0.25 | -26.8     | 71.5                      | 235                          | 209                 | 158               |
| 26               | 0.398 | 0.25 | -26.1     | 77.9                      | 256                          | 230                 | 152               |
| 25               | 0.431 | 0.25 | -25.4     | 84.4                      | 277                          | 251                 | 147               |
| 24               | 0.464 | 0.25 | -24.7     | 90.9                      | 298                          | 272                 | 143               |
| 23               | 0.496 | 0.25 | -24.2     | 97.1                      | 319                          | 293                 | 139               |
| 22               | 0.530 | 0.25 | -23.6     | 103.8                     | 341                          | 316                 | 136               |
| 21               | 0.563 | 0.25 | -23.1     | 110.3                     | 362                          | 338                 | 134               |
| 20               | 0.596 | 0.25 | -22.6     | 116.7                     | 383                          | 360                 | 133               |
| 19               | 0.629 | 0.25 | -22.1     | 123.2                     | 404                          | 382                 | 132               |
| 18               | 0.661 | 0.25 | -21.7     | 129.5                     | 425                          | 404                 | 133               |
| 17               | 0.692 | 0.25 | -21.3     | 135.5                     | 445                          | 425                 | 134               |
| 16               | 0.724 | 0.25 | -20.9     | 141.8                     | 465                          | 447                 | 136               |
| 15               | 0.754 | 0.25 | -20.5     | 147.7                     | 484                          | 468                 | 139               |
| 14               | 0.782 | 0.25 | -20.2     | 153.1                     | 502                          | 488                 | 142               |
| 13               | 0.810 | 0.25 | -19.9     | 158.6                     | 520                          | 507                 | 147               |
| 12               | 0.836 | 0.25 | -19.6     | 163.7                     | 537                          | 525                 | 152               |
| 11               | 0.861 | 0.25 | -19.4     | 168.6                     | 553                          | 543                 | 158               |
| 10               | 0.885 | 0.25 | -19.1     | 173.3                     | 569                          | 560                 | 165               |
| 9                | 0.905 | 0.25 | -18.9     | 177.2                     | 581                          | 574                 | 173               |
| 8                | 0.924 | 0.25 | -18.7     | 181.0                     | 594                          | 588                 | 181               |
| 7                | 0.940 | 0.25 | -18.6     | 184.1                     | 604                          | 599                 | 190               |
| 6                | 0.956 | 0.25 | -18.5     | 187.2                     | 614                          | 611                 | 200               |
| 5                | 0.969 | 0.25 | -18.3     | 189.8                     | 623                          | 620                 | 210               |
| 4                | 0.979 | 0.25 | -18.2     | 191.7                     | 629                          | 628                 | 220               |
| 3                | 0.987 | 0.25 | -18.2     | 193.3                     | 634                          | 633                 | 231               |
| 2                | 0.994 | 0.25 | -18.1     | 194.7                     | 639                          | 638                 | 242               |
| 1                | 0.997 | 0.25 | -18.1     | 195.3                     | 641                          | 641                 | 253               |
| 0                | 1.000 | 0.25 | -18.1     | 195.8                     | 643                          | 643                 | 264               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 132

Figure 7B

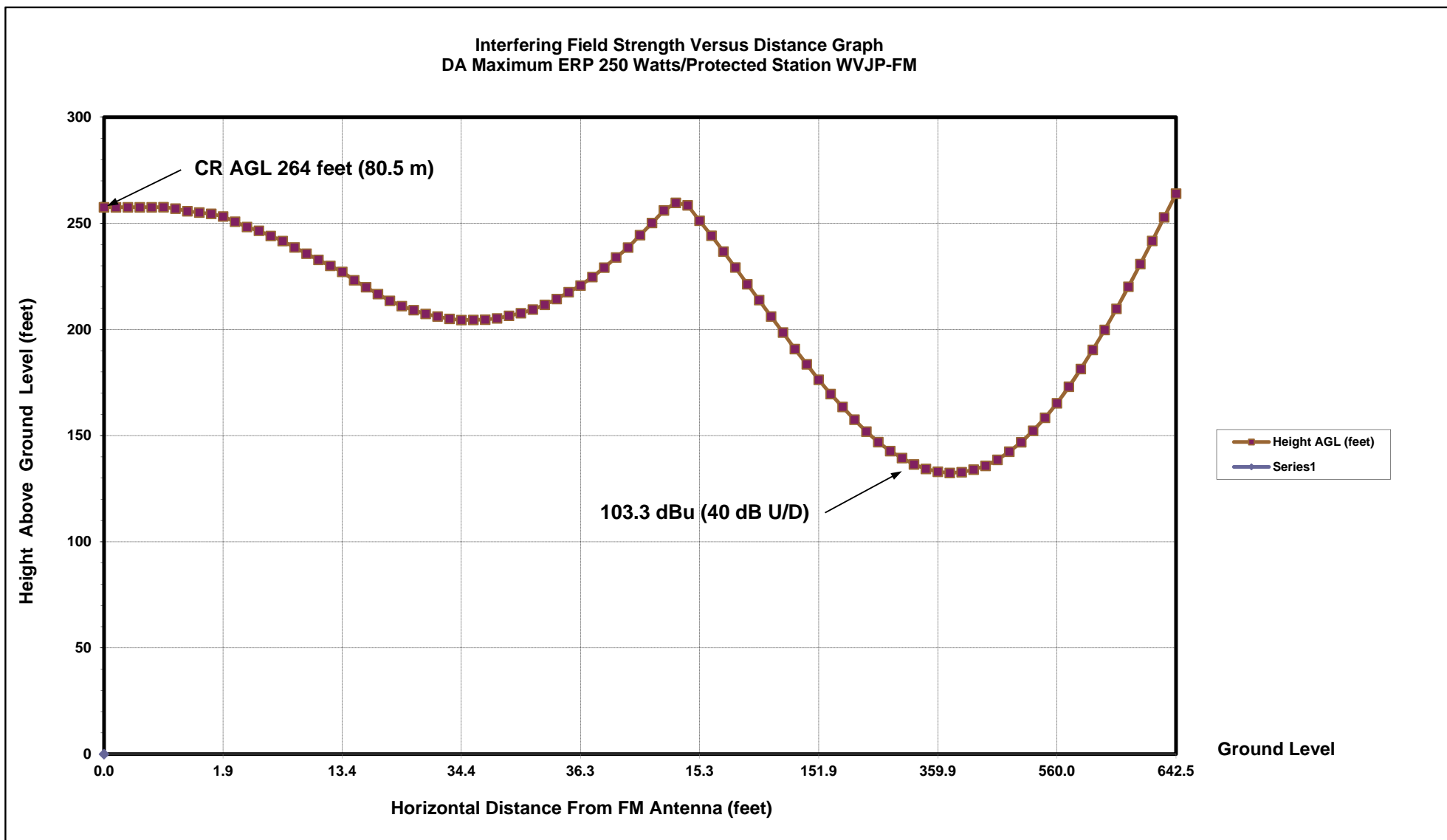


Figure 8A

## Interfering Field Strength Vs. Distance Graph - W279BU to WERR (FM) - Point "C", Figure 6

|                     |  |  |     |                 |  |  |  |
|---------------------|--|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelength |  |     |                 |  |  |  |
| RCAGL               | 559 feet   |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 103.3 dBu  |  |     | -6.02059991 dBk |  |  |  |

172'+387'=559'

382 MTS ELEV. TERR

10° AZIM

| Depression Angle | VRF   | HRF  | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 0                   | 535               |
| 89               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 0                   | 535               |
| 88               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 1                   | 535               |
| 87               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 1                   | 535               |
| 86               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 2                   | 535               |
| 85               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 2                   | 535               |
| 84               | 0.011 | 0.95 | -45.6     | 8.2                       | 27                           | 3                   | 532               |
| 83               | 0.013 | 0.95 | -44.2     | 9.7                       | 32                           | 4                   | 527               |
| 82               | 0.014 | 0.95 | -43.5     | 10.4                      | 34                           | 5                   | 525               |
| 81               | 0.015 | 0.95 | -42.9     | 11.2                      | 37                           | 6                   | 523               |
| 80               | 0.017 | 0.95 | -41.9     | 12.7                      | 42                           | 7                   | 518               |
| 79               | 0.021 | 0.95 | -40.0     | 15.6                      | 51                           | 10                  | 509               |
| 78               | 0.025 | 0.95 | -38.5     | 18.6                      | 61                           | 13                  | 499               |
| 77               | 0.028 | 0.95 | -37.5     | 20.8                      | 68                           | 15                  | 492               |
| 76               | 0.032 | 0.95 | -36.4     | 23.8                      | 78                           | 19                  | 483               |
| 75               | 0.036 | 0.95 | -35.3     | 26.8                      | 88                           | 23                  | 474               |
| 74               | 0.041 | 0.95 | -34.2     | 30.5                      | 100                          | 28                  | 463               |
| 73               | 0.046 | 0.95 | -33.2     | 34.2                      | 112                          | 33                  | 452               |
| 72               | 0.051 | 0.95 | -32.3     | 38.0                      | 125                          | 38                  | 441               |
| 71               | 0.056 | 0.95 | -31.5     | 41.7                      | 137                          | 45                  | 430               |
| 70               | 0.061 | 0.95 | -30.8     | 45.4                      | 149                          | 51                  | 419               |
| 69               | 0.068 | 0.95 | -29.8     | 50.6                      | 166                          | 59                  | 404               |
| 68               | 0.074 | 0.95 | -29.1     | 55.1                      | 181                          | 68                  | 391               |
| 67               | 0.080 | 0.95 | -28.4     | 59.5                      | 195                          | 76                  | 379               |
| 66               | 0.086 | 0.95 | -27.8     | 64.0                      | 210                          | 85                  | 367               |
| 65               | 0.091 | 0.95 | -27.3     | 67.7                      | 222                          | 94                  | 358               |
| 64               | 0.095 | 0.95 | -26.9     | 70.7                      | 232                          | 102                 | 351               |
| 63               | 0.099 | 0.95 | -26.6     | 73.7                      | 242                          | 110                 | 344               |
| 62               | 0.102 | 0.95 | -26.3     | 75.9                      | 249                          | 117                 | 339               |
| 61               | 0.105 | 0.95 | -26.0     | 78.1                      | 256                          | 124                 | 335               |
| 60               | 0.107 | 0.95 | -25.9     | 79.6                      | 261                          | 131                 | 333               |
| 59               | 0.108 | 0.95 | -25.8     | 80.4                      | 264                          | 136                 | 333               |
| 58               | 0.109 | 0.95 | -25.7     | 81.1                      | 266                          | 141                 | 333               |
| 57               | 0.109 | 0.95 | -25.7     | 81.1                      | 266                          | 145                 | 336               |
| 56               | 0.108 | 0.95 | -25.8     | 80.4                      | 264                          | 147                 | 340               |
| 55               | 0.107 | 0.95 | -25.9     | 79.6                      | 261                          | 150                 | 345               |
| 54               | 0.105 | 0.95 | -26.0     | 78.1                      | 256                          | 151                 | 352               |
| 53               | 0.102 | 0.95 | -26.3     | 75.9                      | 249                          | 150                 | 360               |
| 52               | 0.098 | 0.95 | -26.6     | 72.9                      | 239                          | 147                 | 370               |
| 51               | 0.093 | 0.95 | -27.1     | 69.2                      | 227                          | 143                 | 383               |
| 50               | 0.088 | 0.95 | -27.6     | 65.5                      | 215                          | 138                 | 394               |
| 49               | 0.081 | 0.95 | -28.3     | 60.3                      | 198                          | 130                 | 410               |
| 48               | 0.073 | 0.95 | -29.2     | 54.3                      | 178                          | 119                 | 427               |
| 47               | 0.064 | 0.95 | -30.3     | 47.6                      | 156                          | 107                 | 445               |



| Depression Angle | VRF   | HRF  | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 0.95 | -31.7     | 40.9                      | 134                          | 93                  | 462               |
| 45               | 0.043 | 0.95 | -33.8     | 32.0                      | 105                          | 74                  | 485               |
| 44               | 0.031 | 0.95 | -36.6     | 23.1                      | 76                           | 54                  | 506               |
| 43               | 0.018 | 0.95 | -41.4     | 13.4                      | 44                           | 32                  | 529               |
| 42               | 0.010 | 0.95 | -46.5     | 7.4                       | 24                           | 18                  | 543               |
| 41               | 0.013 | 0.95 | -44.2     | 9.7                       | 32                           | 24                  | 538               |
| 40               | 0.031 | 0.95 | -36.6     | 23.1                      | 76                           | 58                  | 510               |
| 39               | 0.049 | 0.95 | -32.7     | 36.5                      | 120                          | 93                  | 484               |
| 38               | 0.069 | 0.95 | -29.7     | 51.4                      | 168                          | 133                 | 455               |
| 37               | 0.090 | 0.95 | -27.4     | 67.0                      | 220                          | 175                 | 427               |
| 36               | 0.113 | 0.95 | -25.4     | 84.1                      | 276                          | 223                 | 397               |
| 35               | 0.136 | 0.95 | -23.8     | 101.2                     | 332                          | 272                 | 369               |
| 34               | 0.161 | 0.95 | -22.3     | 119.8                     | 393                          | 326                 | 339               |
| 33               | 0.187 | 0.95 | -21.0     | 139.2                     | 457                          | 383                 | 310               |
| 32               | 0.215 | 0.95 | -19.8     | 160.0                     | 525                          | 445                 | 281               |
| 31               | 0.243 | 0.95 | -18.8     | 180.8                     | 593                          | 509                 | 253               |
| 30               | 0.273 | 0.95 | -17.7     | 203.2                     | 667                          | 577                 | 226               |
| 29               | 0.303 | 0.95 | -16.8     | 225.5                     | 740                          | 647                 | 200               |
| 28               | 0.333 | 0.95 | -16.0     | 247.8                     | 813                          | 718                 | 177               |
| 27               | 0.365 | 0.95 | -15.2     | 271.6                     | 891                          | 794                 | 154               |
| 26               | 0.398 | 0.95 | -14.5     | 296.2                     | 972                          | 873                 | 133               |
| 25               | 0.431 | 0.95 | -13.8     | 320.8                     | 1052                         | 954                 | 114               |
| 24               | 0.464 | 0.95 | -13.1     | 345.3                     | 1133                         | 1035                | 98                |
| 23               | 0.496 | 0.95 | -12.6     | 369.1                     | 1211                         | 1115                | 86                |
| 22               | 0.530 | 0.95 | -12.0     | 394.4                     | 1294                         | 1200                | 74                |
| 21               | 0.563 | 0.95 | -11.5     | 419.0                     | 1375                         | 1283                | 66                |
| 20               | 0.596 | 0.95 | -11.0     | 443.5                     | 1455                         | 1367                | 61                |
| 19               | 0.629 | 0.95 | -10.5     | 468.1                     | 1536                         | 1452                | 59                |
| 18               | 0.661 | 0.95 | -10.1     | 491.9                     | 1614                         | 1535                | 60                |
| 17               | 0.692 | 0.95 | -9.7      | 515.0                     | 1690                         | 1616                | 65                |
| 16               | 0.724 | 0.95 | -9.3      | 538.8                     | 1768                         | 1699                | 72                |
| 15               | 0.754 | 0.95 | -8.9      | 561.1                     | 1841                         | 1778                | 83                |
| 14               | 0.782 | 0.95 | -8.6      | 582.0                     | 1909                         | 1853                | 97                |
| 13               | 0.810 | 0.95 | -8.3      | 602.8                     | 1978                         | 1927                | 114               |
| 12               | 0.836 | 0.95 | -8.0      | 622.2                     | 2041                         | 1997                | 135               |
| 11               | 0.861 | 0.95 | -7.8      | 640.8                     | 2102                         | 2064                | 158               |
| 10               | 0.885 | 0.95 | -7.5      | 658.6                     | 2161                         | 2128                | 184               |
| 9                | 0.905 | 0.95 | -7.3      | 673.5                     | 2210                         | 2182                | 213               |
| 8                | 0.924 | 0.95 | -7.2      | 687.6                     | 2256                         | 2234                | 245               |
| 7                | 0.940 | 0.95 | -7.0      | 699.6                     | 2295                         | 2278                | 279               |
| 6                | 0.956 | 0.95 | -6.9      | 711.5                     | 2334                         | 2321                | 315               |
| 5                | 0.969 | 0.95 | -6.7      | 721.1                     | 2366                         | 2357                | 353               |
| 4                | 0.979 | 0.95 | -6.7      | 728.6                     | 2390                         | 2385                | 392               |
| 3                | 0.987 | 0.95 | -6.6      | 734.5                     | 2410                         | 2407                | 433               |
| 2                | 0.994 | 0.95 | -6.5      | 739.7                     | 2427                         | 2425                | 474               |
| 1                | 0.997 | 0.95 | -6.5      | 742.0                     | 2434                         | 2434                | 517               |
| 0                | 1.000 | 0.95 | -6.5      | 744.2                     | 2442                         | 2442                | 559               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 59

Figure 8B

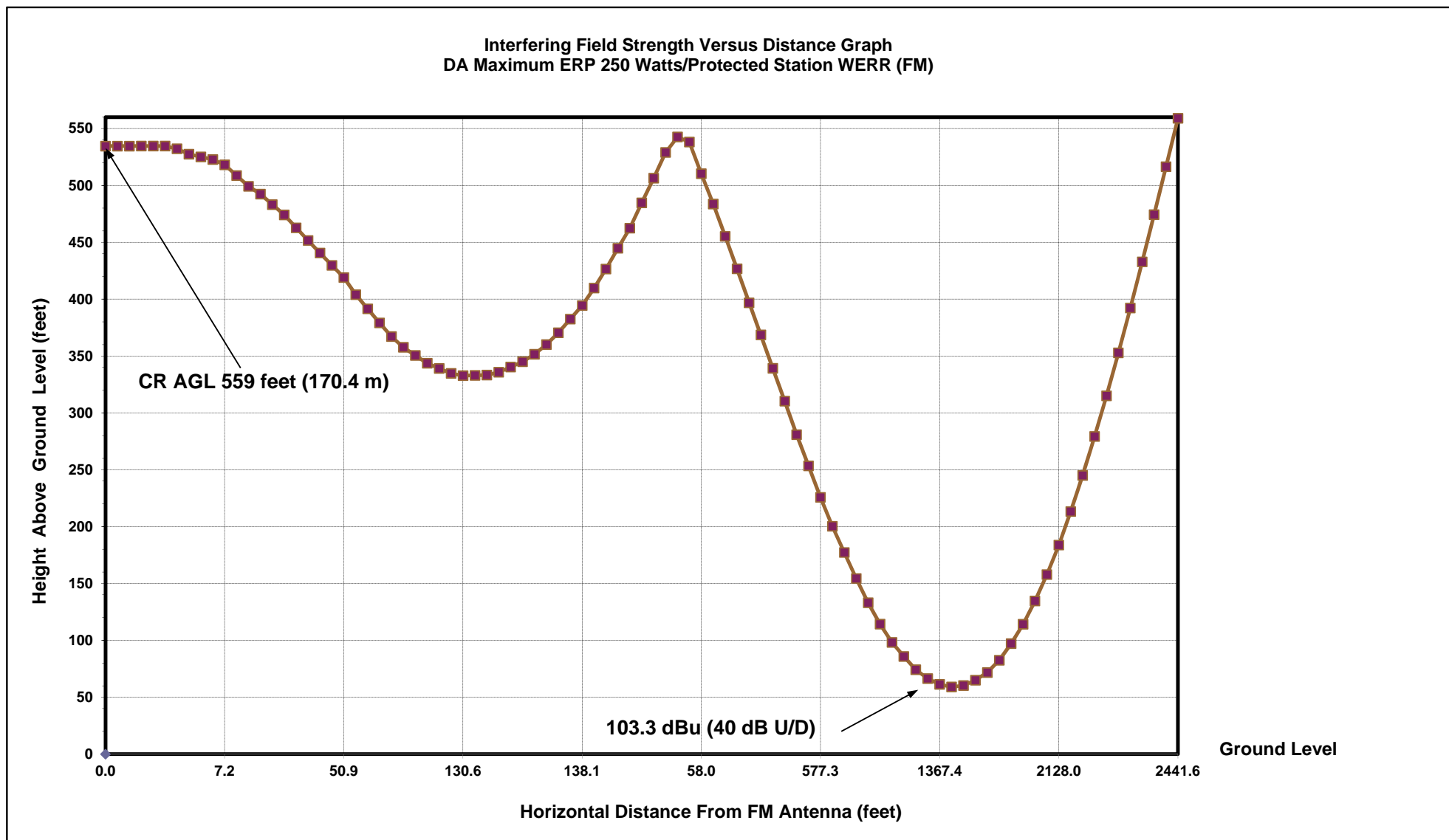


Figure 9A

## Interfering Field Strength Vs. Distance Graph - W279BU to WERR (FM) - Point "D", Figure 6

|                     |  |  |     |                 |  |  |  |
|---------------------|--|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelength |  |     |                 |  |  |  |
| RCAGL               | 474 feet   |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 103.3 dBu  |  |     | -6.02059991 dBk |  |  |  |

172'+302'=474'

408 MTS ELEV. TERR

17° AZIM

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 0                   | 452               |
| 89               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 0                   | 452               |
| 88               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 1                   | 452               |
| 87               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 1                   | 452               |
| 86               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 2                   | 452               |
| 85               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 2                   | 452               |
| 84               | 0.011 | 0.865 | -46.5     | 7.5                       | 24                           | 3                   | 450               |
| 83               | 0.013 | 0.865 | -45.0     | 8.8                       | 29                           | 4                   | 445               |
| 82               | 0.014 | 0.865 | -44.4     | 9.5                       | 31                           | 4                   | 443               |
| 81               | 0.015 | 0.865 | -43.8     | 10.2                      | 33                           | 5                   | 441               |
| 80               | 0.017 | 0.865 | -42.7     | 11.5                      | 38                           | 7                   | 437               |
| 79               | 0.021 | 0.865 | -40.8     | 14.2                      | 47                           | 9                   | 428               |
| 78               | 0.025 | 0.865 | -39.3     | 16.9                      | 56                           | 12                  | 420               |
| 77               | 0.028 | 0.865 | -38.3     | 19.0                      | 62                           | 14                  | 413               |
| 76               | 0.032 | 0.865 | -37.2     | 21.7                      | 71                           | 17                  | 405               |
| 75               | 0.036 | 0.865 | -36.2     | 24.4                      | 80                           | 21                  | 397               |
| 74               | 0.041 | 0.865 | -35.0     | 27.8                      | 91                           | 25                  | 386               |
| 73               | 0.046 | 0.865 | -34.0     | 31.2                      | 102                          | 30                  | 376               |
| 72               | 0.051 | 0.865 | -33.1     | 34.6                      | 113                          | 35                  | 366               |
| 71               | 0.056 | 0.865 | -32.3     | 37.9                      | 124                          | 41                  | 356               |
| 70               | 0.061 | 0.865 | -31.6     | 41.3                      | 136                          | 46                  | 347               |
| 69               | 0.068 | 0.865 | -30.6     | 46.1                      | 151                          | 54                  | 333               |
| 68               | 0.074 | 0.865 | -29.9     | 50.1                      | 165                          | 62                  | 321               |
| 67               | 0.080 | 0.865 | -29.2     | 54.2                      | 178                          | 69                  | 310               |
| 66               | 0.086 | 0.865 | -28.6     | 58.3                      | 191                          | 78                  | 299               |
| 65               | 0.091 | 0.865 | -28.1     | 61.7                      | 202                          | 85                  | 291               |
| 64               | 0.095 | 0.865 | -27.7     | 64.4                      | 211                          | 93                  | 284               |
| 63               | 0.099 | 0.865 | -27.4     | 67.1                      | 220                          | 100                 | 278               |
| 62               | 0.102 | 0.865 | -27.1     | 69.1                      | 227                          | 106                 | 274               |
| 61               | 0.105 | 0.865 | -26.9     | 71.2                      | 233                          | 113                 | 270               |
| 60               | 0.107 | 0.865 | -26.7     | 72.5                      | 238                          | 119                 | 268               |
| 59               | 0.108 | 0.865 | -26.6     | 73.2                      | 240                          | 124                 | 268               |
| 58               | 0.109 | 0.865 | -26.5     | 73.9                      | 242                          | 128                 | 268               |
| 57               | 0.109 | 0.865 | -26.5     | 73.9                      | 242                          | 132                 | 271               |
| 56               | 0.108 | 0.865 | -26.6     | 73.2                      | 240                          | 134                 | 275               |
| 55               | 0.107 | 0.865 | -26.7     | 72.5                      | 238                          | 136                 | 279               |
| 54               | 0.105 | 0.865 | -26.9     | 71.2                      | 233                          | 137                 | 285               |
| 53               | 0.102 | 0.865 | -27.1     | 69.1                      | 227                          | 136                 | 293               |
| 52               | 0.098 | 0.865 | -27.5     | 66.4                      | 218                          | 134                 | 302               |
| 51               | 0.093 | 0.865 | -27.9     | 63.0                      | 207                          | 130                 | 313               |
| 50               | 0.088 | 0.865 | -28.4     | 59.6                      | 196                          | 126                 | 324               |
| 49               | 0.081 | 0.865 | -29.1     | 54.9                      | 180                          | 118                 | 338               |
| 48               | 0.073 | 0.865 | -30.0     | 49.5                      | 162                          | 109                 | 353               |
| 47               | 0.064 | 0.865 | -31.2     | 43.4                      | 142                          | 97                  | 370               |

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 0.865 | -32.5     | 37.3                      | 122                          | 85                  | 386               |
| 45               | 0.043 | 0.865 | -34.6     | 29.1                      | 96                           | 68                  | 406               |
| 44               | 0.031 | 0.865 | -37.5     | 21.0                      | 69                           | 50                  | 426               |
| 43               | 0.018 | 0.865 | -42.2     | 12.2                      | 40                           | 29                  | 447               |
| 42               | 0.010 | 0.865 | -47.3     | 6.8                       | 22                           | 17                  | 459               |
| 41               | 0.013 | 0.865 | -45.0     | 8.8                       | 29                           | 22                  | 455               |
| 40               | 0.031 | 0.865 | -37.5     | 21.0                      | 69                           | 53                  | 430               |
| 39               | 0.049 | 0.865 | -33.5     | 33.2                      | 109                          | 85                  | 405               |
| 38               | 0.069 | 0.865 | -30.5     | 46.8                      | 153                          | 121                 | 380               |
| 37               | 0.090 | 0.865 | -28.2     | 61.0                      | 200                          | 160                 | 354               |
| 36               | 0.113 | 0.865 | -26.2     | 76.6                      | 251                          | 203                 | 326               |
| 35               | 0.136 | 0.865 | -24.6     | 92.2                      | 302                          | 248                 | 301               |
| 34               | 0.161 | 0.865 | -23.1     | 109.1                     | 358                          | 297                 | 274               |
| 33               | 0.187 | 0.865 | -21.8     | 126.7                     | 416                          | 349                 | 248               |
| 32               | 0.215 | 0.865 | -20.6     | 145.7                     | 478                          | 405                 | 221               |
| 31               | 0.243 | 0.865 | -19.6     | 164.7                     | 540                          | 463                 | 196               |
| 30               | 0.273 | 0.865 | -18.6     | 185.0                     | 607                          | 526                 | 171               |
| 29               | 0.303 | 0.865 | -17.7     | 205.3                     | 674                          | 589                 | 147               |
| 28               | 0.333 | 0.865 | -16.8     | 225.6                     | 740                          | 654                 | 126               |
| 27               | 0.365 | 0.865 | -16.0     | 247.3                     | 811                          | 723                 | 106               |
| 26               | 0.398 | 0.865 | -15.3     | 269.7                     | 885                          | 795                 | 86                |
| 25               | 0.431 | 0.865 | -14.6     | 292.1                     | 958                          | 868                 | 69                |
| 24               | 0.464 | 0.865 | -13.9     | 314.4                     | 1032                         | 942                 | 54                |
| 23               | 0.496 | 0.865 | -13.4     | 336.1                     | 1103                         | 1015                | 43                |
| 22               | 0.530 | 0.865 | -12.8     | 359.1                     | 1178                         | 1092                | 33                |
| 21               | 0.563 | 0.865 | -12.3     | 381.5                     | 1252                         | 1169                | 25                |
| 20               | 0.596 | 0.865 | -11.8     | 403.9                     | 1325                         | 1245                | 21                |
| 19               | 0.629 | 0.865 | -11.3     | 426.2                     | 1398                         | 1322                | 19                |
| 18               | 0.661 | 0.865 | -10.9     | 447.9                     | 1470                         | 1398                | 20                |
| 17               | 0.692 | 0.865 | -10.5     | 468.9                     | 1538                         | 1471                | 24                |
| 16               | 0.724 | 0.865 | -10.1     | 490.6                     | 1610                         | 1547                | 30                |
| 15               | 0.754 | 0.865 | -9.7      | 510.9                     | 1676                         | 1619                | 40                |
| 14               | 0.782 | 0.865 | -9.4      | 529.9                     | 1739                         | 1687                | 53                |
| 13               | 0.810 | 0.865 | -9.1      | 548.9                     | 1801                         | 1755                | 69                |
| 12               | 0.836 | 0.865 | -8.8      | 566.5                     | 1859                         | 1818                | 88                |
| 11               | 0.861 | 0.865 | -8.6      | 583.4                     | 1914                         | 1879                | 109               |
| 10               | 0.885 | 0.865 | -8.3      | 599.7                     | 1967                         | 1938                | 132               |
| 9                | 0.905 | 0.865 | -8.1      | 613.2                     | 2012                         | 1987                | 159               |
| 8                | 0.924 | 0.865 | -8.0      | 626.1                     | 2054                         | 2034                | 188               |
| 7                | 0.940 | 0.865 | -7.8      | 637.0                     | 2090                         | 2074                | 219               |
| 6                | 0.956 | 0.865 | -7.7      | 647.8                     | 2125                         | 2114                | 252               |
| 5                | 0.969 | 0.865 | -7.6      | 656.6                     | 2154                         | 2146                | 286               |
| 4                | 0.979 | 0.865 | -7.5      | 663.4                     | 2176                         | 2171                | 322               |
| 3                | 0.987 | 0.865 | -7.4      | 668.8                     | 2194                         | 2191                | 359               |
| 2                | 0.994 | 0.865 | -7.3      | 673.6                     | 2210                         | 2208                | 397               |
| 1                | 0.997 | 0.865 | -7.3      | 675.6                     | 2216                         | 2216                | 435               |
| 0                | 1.000 | 0.865 | -7.3      | 677.6                     | 2223                         | 2223                | 474               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 19

Figure 9B

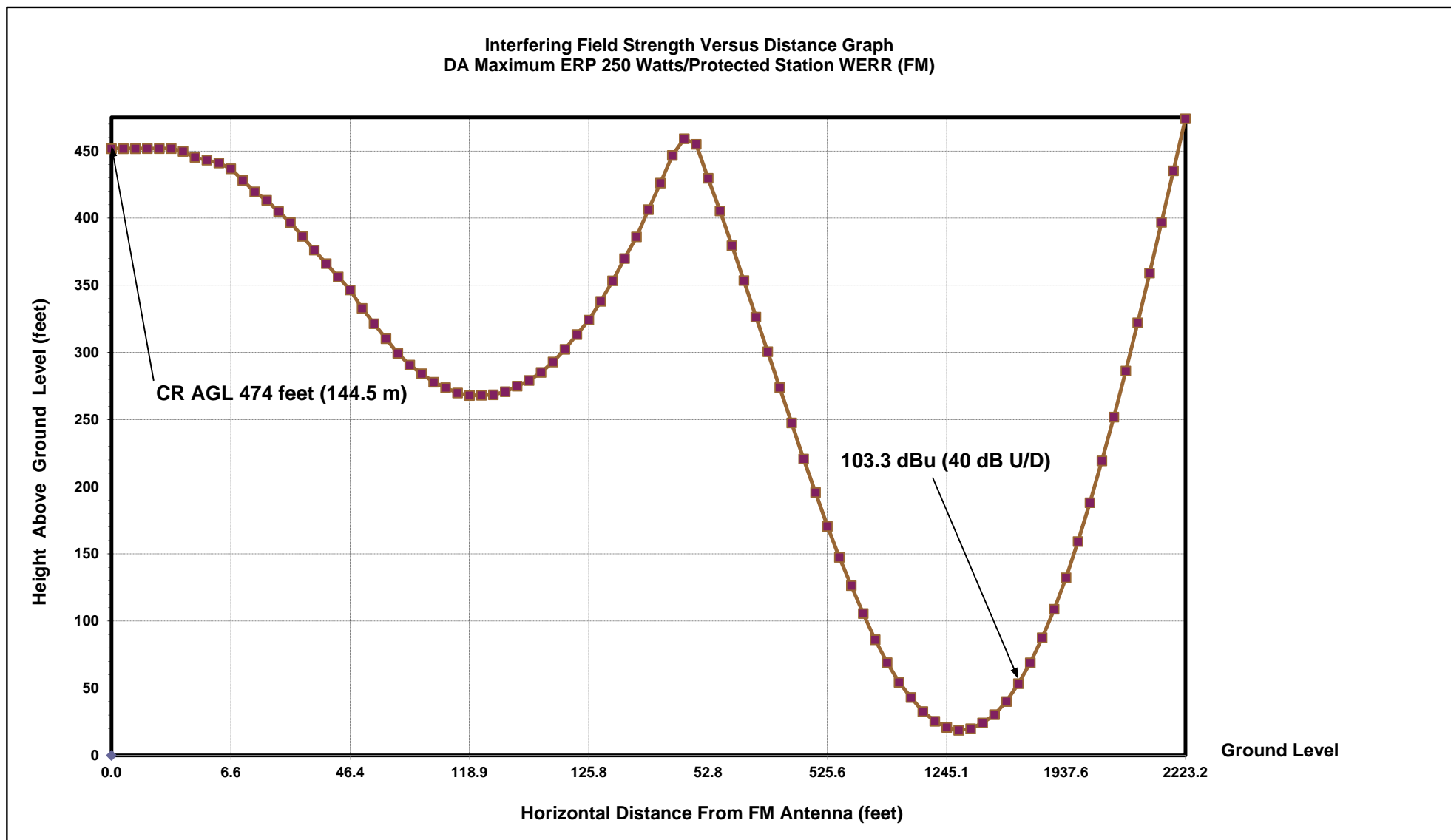


Figure 10A

## Interfering Field Strength Vs. Distance Graph - W279BU to WERR (FM) - Point "E", Figure 6

|                     |  |  |     |                 |  |  |  |
|---------------------|--|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelength |  |     |                 |  |  |  |
| RCAGL               | 464 feet   |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 103.3 dBu  |  |     | -6.02059991 dBk |  |  |  |

172'+292'=464'

411 MTS ELEV. TERR

20° AZIM

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 0                   | 443               |
| 89               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 0                   | 443               |
| 88               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 1                   | 443               |
| 87               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 1                   | 443               |
| 86               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 1                   | 443               |
| 85               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 2                   | 443               |
| 84               | 0.011 | 0.820 | -46.9     | 7.1                       | 23                           | 2                   | 441               |
| 83               | 0.013 | 0.820 | -45.5     | 8.4                       | 27                           | 3                   | 437               |
| 82               | 0.014 | 0.820 | -44.8     | 9.0                       | 30                           | 4                   | 435               |
| 81               | 0.015 | 0.820 | -44.2     | 9.6                       | 32                           | 5                   | 433               |
| 80               | 0.017 | 0.820 | -43.1     | 10.9                      | 36                           | 6                   | 429               |
| 79               | 0.021 | 0.820 | -41.3     | 13.5                      | 44                           | 8                   | 421               |
| 78               | 0.025 | 0.820 | -39.8     | 16.1                      | 53                           | 11                  | 412               |
| 77               | 0.028 | 0.820 | -38.8     | 18.0                      | 59                           | 13                  | 407               |
| 76               | 0.032 | 0.820 | -37.6     | 20.6                      | 67                           | 16                  | 399               |
| 75               | 0.036 | 0.820 | -36.6     | 23.1                      | 76                           | 20                  | 391               |
| 74               | 0.041 | 0.820 | -35.5     | 26.3                      | 86                           | 24                  | 381               |
| 73               | 0.046 | 0.820 | -34.5     | 29.5                      | 97                           | 28                  | 371               |
| 72               | 0.051 | 0.820 | -33.6     | 32.8                      | 107                          | 33                  | 362               |
| 71               | 0.056 | 0.820 | -32.8     | 36.0                      | 118                          | 38                  | 352               |
| 70               | 0.061 | 0.820 | -32.0     | 39.2                      | 129                          | 44                  | 343               |
| 69               | 0.068 | 0.820 | -31.1     | 43.7                      | 143                          | 51                  | 330               |
| 68               | 0.074 | 0.820 | -30.4     | 47.5                      | 156                          | 58                  | 319               |
| 67               | 0.080 | 0.820 | -29.7     | 51.4                      | 169                          | 66                  | 309               |
| 66               | 0.086 | 0.820 | -29.1     | 55.2                      | 181                          | 74                  | 298               |
| 65               | 0.091 | 0.820 | -28.6     | 58.5                      | 192                          | 81                  | 290               |
| 64               | 0.095 | 0.820 | -28.2     | 61.0                      | 200                          | 88                  | 284               |
| 63               | 0.099 | 0.820 | -27.8     | 63.6                      | 209                          | 95                  | 278               |
| 62               | 0.102 | 0.820 | -27.6     | 65.5                      | 215                          | 101                 | 274               |
| 61               | 0.105 | 0.820 | -27.3     | 67.4                      | 221                          | 107                 | 270               |
| 60               | 0.107 | 0.820 | -27.2     | 68.7                      | 226                          | 113                 | 269               |
| 59               | 0.108 | 0.820 | -27.1     | 69.4                      | 228                          | 117                 | 269               |
| 58               | 0.109 | 0.820 | -27.0     | 70.0                      | 230                          | 122                 | 269               |
| 57               | 0.109 | 0.820 | -27.0     | 70.0                      | 230                          | 125                 | 271               |
| 56               | 0.108 | 0.820 | -27.1     | 69.4                      | 228                          | 127                 | 275               |
| 55               | 0.107 | 0.820 | -27.2     | 68.7                      | 226                          | 129                 | 279               |
| 54               | 0.105 | 0.820 | -27.3     | 67.4                      | 221                          | 130                 | 285               |
| 53               | 0.102 | 0.820 | -27.6     | 65.5                      | 215                          | 129                 | 292               |
| 52               | 0.098 | 0.820 | -27.9     | 63.0                      | 207                          | 127                 | 301               |
| 51               | 0.093 | 0.820 | -28.4     | 59.7                      | 196                          | 123                 | 312               |
| 50               | 0.088 | 0.820 | -28.9     | 56.5                      | 185                          | 119                 | 322               |
| 49               | 0.081 | 0.820 | -29.6     | 52.0                      | 171                          | 112                 | 335               |
| 48               | 0.073 | 0.820 | -30.5     | 46.9                      | 154                          | 103                 | 350               |
| 47               | 0.064 | 0.820 | -31.6     | 41.1                      | 135                          | 92                  | 365               |

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 0.820 | -32.9     | 35.3                      | 116                          | 81                  | 381               |
| 45               | 0.043 | 0.820 | -35.1     | 27.6                      | 91                           | 64                  | 400               |
| 44               | 0.031 | 0.820 | -37.9     | 19.9                      | 65                           | 47                  | 419               |
| 43               | 0.018 | 0.820 | -42.6     | 11.6                      | 38                           | 28                  | 438               |
| 42               | 0.010 | 0.820 | -47.7     | 6.4                       | 21                           | 16                  | 450               |
| 41               | 0.013 | 0.820 | -45.5     | 8.4                       | 27                           | 21                  | 446               |
| 40               | 0.031 | 0.820 | -37.9     | 19.9                      | 65                           | 50                  | 422               |
| 39               | 0.049 | 0.820 | -33.9     | 31.5                      | 103                          | 80                  | 399               |
| 38               | 0.069 | 0.820 | -31.0     | 44.3                      | 145                          | 115                 | 374               |
| 37               | 0.090 | 0.820 | -28.7     | 57.8                      | 190                          | 151                 | 350               |
| 36               | 0.113 | 0.820 | -26.7     | 72.6                      | 238                          | 193                 | 324               |
| 35               | 0.136 | 0.820 | -25.1     | 87.4                      | 287                          | 235                 | 300               |
| 34               | 0.161 | 0.820 | -23.6     | 103.4                     | 339                          | 281                 | 274               |
| 33               | 0.187 | 0.820 | -22.3     | 120.1                     | 394                          | 331                 | 249               |
| 32               | 0.215 | 0.820 | -21.1     | 138.1                     | 453                          | 384                 | 224               |
| 31               | 0.243 | 0.820 | -20.0     | 156.1                     | 512                          | 439                 | 200               |
| 30               | 0.273 | 0.820 | -19.0     | 175.4                     | 575                          | 498                 | 176               |
| 29               | 0.303 | 0.820 | -18.1     | 194.6                     | 639                          | 559                 | 154               |
| 28               | 0.333 | 0.820 | -17.3     | 213.9                     | 702                          | 620                 | 135               |
| 27               | 0.365 | 0.820 | -16.5     | 234.5                     | 769                          | 685                 | 115               |
| 26               | 0.398 | 0.820 | -15.7     | 255.7                     | 839                          | 754                 | 96                |
| 25               | 0.431 | 0.820 | -15.1     | 276.9                     | 908                          | 823                 | 80                |
| 24               | 0.464 | 0.820 | -14.4     | 298.1                     | 978                          | 893                 | 66                |
| 23               | 0.496 | 0.820 | -13.8     | 318.6                     | 1045                         | 962                 | 56                |
| 22               | 0.530 | 0.820 | -13.3     | 340.5                     | 1117                         | 1036                | 46                |
| 21               | 0.563 | 0.820 | -12.7     | 361.7                     | 1187                         | 1108                | 39                |
| 20               | 0.596 | 0.820 | -12.2     | 382.9                     | 1256                         | 1180                | 34                |
| 19               | 0.629 | 0.820 | -11.8     | 404.0                     | 1326                         | 1253                | 32                |
| 18               | 0.661 | 0.820 | -11.3     | 424.6                     | 1393                         | 1325                | 34                |
| 17               | 0.692 | 0.820 | -10.9     | 444.5                     | 1458                         | 1395                | 38                |
| 16               | 0.724 | 0.820 | -10.5     | 465.1                     | 1526                         | 1467                | 43                |
| 15               | 0.754 | 0.820 | -10.2     | 484.3                     | 1589                         | 1535                | 53                |
| 14               | 0.782 | 0.820 | -9.9      | 502.3                     | 1648                         | 1599                | 65                |
| 13               | 0.810 | 0.820 | -9.6      | 520.3                     | 1707                         | 1663                | 80                |
| 12               | 0.836 | 0.820 | -9.3      | 537.0                     | 1762                         | 1723                | 98                |
| 11               | 0.861 | 0.820 | -9.0      | 553.1                     | 1815                         | 1781                | 118               |
| 10               | 0.885 | 0.820 | -8.8      | 568.5                     | 1865                         | 1837                | 140               |
| 9                | 0.905 | 0.820 | -8.6      | 581.3                     | 1907                         | 1884                | 166               |
| 8                | 0.924 | 0.820 | -8.4      | 593.5                     | 1947                         | 1928                | 193               |
| 7                | 0.940 | 0.820 | -8.3      | 603.8                     | 1981                         | 1966                | 223               |
| 6                | 0.956 | 0.820 | -8.1      | 614.1                     | 2015                         | 2004                | 253               |
| 5                | 0.969 | 0.820 | -8.0      | 622.5                     | 2042                         | 2034                | 286               |
| 4                | 0.979 | 0.820 | -7.9      | 628.9                     | 2063                         | 2058                | 320               |
| 3                | 0.987 | 0.820 | -7.9      | 634.0                     | 2080                         | 2077                | 355               |
| 2                | 0.994 | 0.820 | -7.8      | 638.5                     | 2095                         | 2094                | 391               |
| 1                | 0.997 | 0.820 | -7.8      | 640.4                     | 2101                         | 2101                | 427               |
| 0                | 1.000 | 0.820 | -7.7      | 642.4                     | 2108                         | 2108                | 464               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 32

Figure 10B

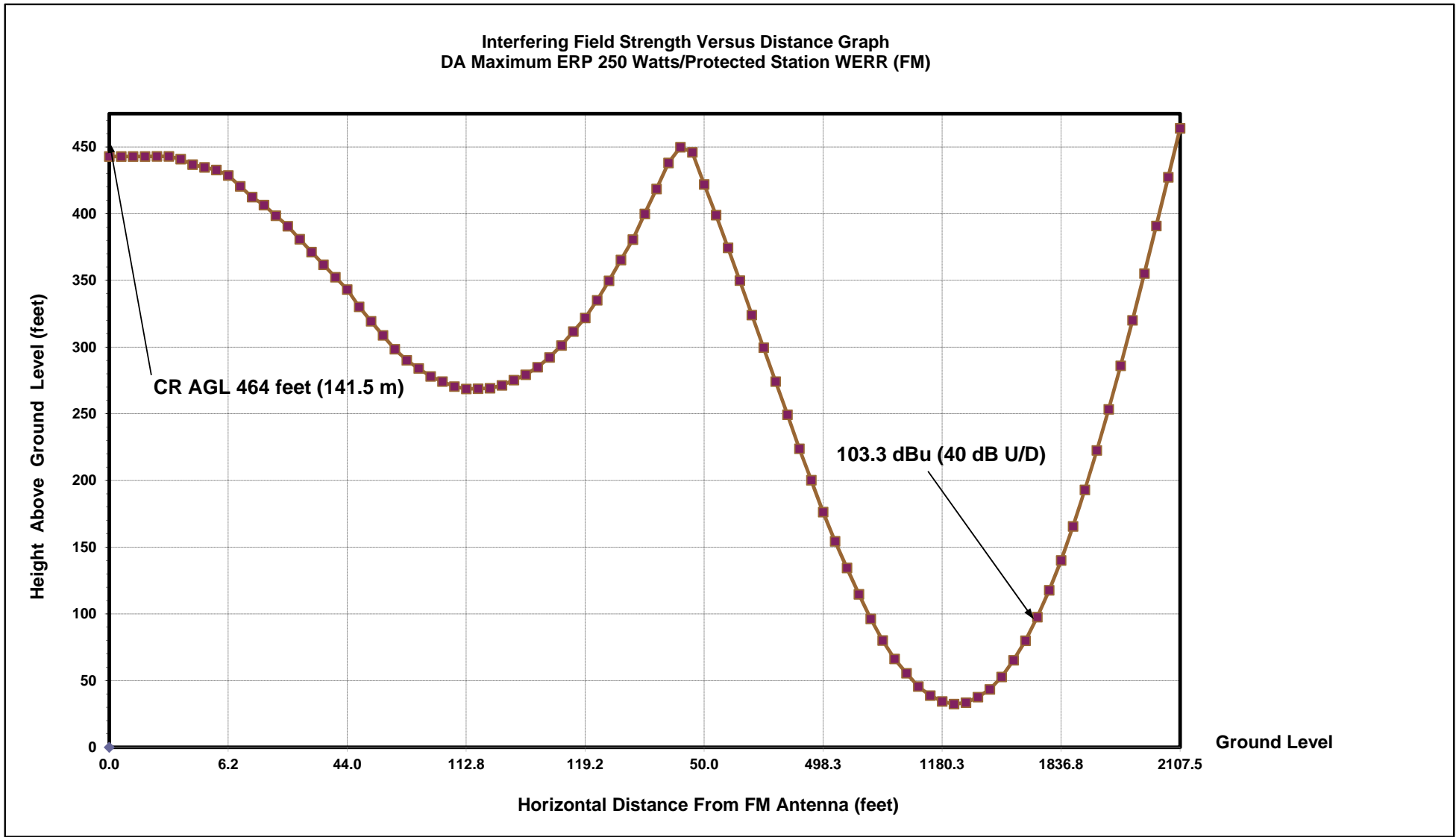




Figure 11A

## Interfering Field Strength Vs. Distance Graph - W279BU to WERR (FM) - Point "F", Figure 6

|                     |  |  |     |                 |  |  |  |
|---------------------|--|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelength |  |     |                 |  |  |  |
| RCAGL               | 500 feet   |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 103.3 dBu  |  |     | -6.02059991 dBk |  |  |  |

172'+328'=500'

400 MTS ELEV. TERR

25° AZIM

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 0                   | 481               |
| 89               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 0                   | 481               |
| 88               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 1                   | 481               |
| 87               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 1                   | 481               |
| 86               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 1                   | 481               |
| 85               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 2                   | 481               |
| 84               | 0.011 | 0.735 | -47.9     | 6.3                       | 21                           | 2                   | 479               |
| 83               | 0.013 | 0.735 | -46.4     | 7.5                       | 25                           | 3                   | 476               |
| 82               | 0.014 | 0.735 | -45.8     | 8.1                       | 26                           | 4                   | 474               |
| 81               | 0.015 | 0.735 | -45.2     | 8.6                       | 28                           | 4                   | 472               |
| 80               | 0.017 | 0.735 | -44.1     | 9.8                       | 32                           | 6                   | 468               |
| 79               | 0.021 | 0.735 | -42.3     | 12.1                      | 40                           | 8                   | 461               |
| 78               | 0.025 | 0.735 | -40.7     | 14.4                      | 47                           | 10                  | 454               |
| 77               | 0.028 | 0.735 | -39.8     | 16.1                      | 53                           | 12                  | 448               |
| 76               | 0.032 | 0.735 | -38.6     | 18.4                      | 60                           | 15                  | 441               |
| 75               | 0.036 | 0.735 | -37.6     | 20.7                      | 68                           | 18                  | 434               |
| 74               | 0.041 | 0.735 | -36.4     | 23.6                      | 77                           | 21                  | 426               |
| 73               | 0.046 | 0.735 | -35.4     | 26.5                      | 87                           | 25                  | 417               |
| 72               | 0.051 | 0.735 | -34.5     | 29.4                      | 96                           | 30                  | 408               |
| 71               | 0.056 | 0.735 | -33.7     | 32.2                      | 106                          | 34                  | 400               |
| 70               | 0.061 | 0.735 | -33.0     | 35.1                      | 115                          | 39                  | 392               |
| 69               | 0.068 | 0.735 | -32.0     | 39.2                      | 128                          | 46                  | 380               |
| 68               | 0.074 | 0.735 | -31.3     | 42.6                      | 140                          | 52                  | 370               |
| 67               | 0.080 | 0.735 | -30.6     | 46.1                      | 151                          | 59                  | 361               |
| 66               | 0.086 | 0.735 | -30.0     | 49.5                      | 162                          | 66                  | 352               |
| 65               | 0.091 | 0.735 | -29.5     | 52.4                      | 172                          | 73                  | 344               |
| 64               | 0.095 | 0.735 | -29.1     | 54.7                      | 179                          | 79                  | 339               |
| 63               | 0.099 | 0.735 | -28.8     | 57.0                      | 187                          | 85                  | 333               |
| 62               | 0.102 | 0.735 | -28.5     | 58.7                      | 193                          | 90                  | 330               |
| 61               | 0.105 | 0.735 | -28.3     | 60.5                      | 198                          | 96                  | 327               |
| 60               | 0.107 | 0.735 | -28.1     | 61.6                      | 202                          | 101                 | 325               |
| 59               | 0.108 | 0.735 | -28.0     | 62.2                      | 204                          | 105                 | 325               |
| 58               | 0.109 | 0.735 | -27.9     | 62.8                      | 206                          | 109                 | 325               |
| 57               | 0.109 | 0.735 | -27.9     | 62.8                      | 206                          | 112                 | 327               |
| 56               | 0.108 | 0.735 | -28.0     | 62.2                      | 204                          | 114                 | 331               |
| 55               | 0.107 | 0.735 | -28.1     | 61.6                      | 202                          | 116                 | 334               |
| 54               | 0.105 | 0.735 | -28.3     | 60.5                      | 198                          | 117                 | 340               |
| 53               | 0.102 | 0.735 | -28.5     | 58.7                      | 193                          | 116                 | 346               |
| 52               | 0.098 | 0.735 | -28.9     | 56.4                      | 185                          | 114                 | 354               |
| 51               | 0.093 | 0.735 | -29.3     | 53.5                      | 176                          | 111                 | 363               |
| 50               | 0.088 | 0.735 | -29.8     | 50.7                      | 166                          | 107                 | 373               |
| 49               | 0.081 | 0.735 | -30.5     | 46.6                      | 153                          | 100                 | 385               |
| 48               | 0.073 | 0.735 | -31.4     | 42.0                      | 138                          | 92                  | 398               |
| 47               | 0.064 | 0.735 | -32.6     | 36.8                      | 121                          | 82                  | 412               |

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 0.735 | -33.9     | 31.7                      | 104                          | 72                  | 425               |
| 45               | 0.043 | 0.735 | -36.0     | 24.8                      | 81                           | 57                  | 443               |
| 44               | 0.031 | 0.735 | -38.9     | 17.8                      | 59                           | 42                  | 459               |
| 43               | 0.018 | 0.735 | -43.6     | 10.4                      | 34                           | 25                  | 477               |
| 42               | 0.010 | 0.735 | -48.7     | 5.8                       | 19                           | 14                  | 487               |
| 41               | 0.013 | 0.735 | -46.4     | 7.5                       | 25                           | 19                  | 484               |
| 40               | 0.031 | 0.735 | -38.9     | 17.8                      | 59                           | 45                  | 462               |
| 39               | 0.049 | 0.735 | -34.9     | 28.2                      | 93                           | 72                  | 442               |
| 38               | 0.069 | 0.735 | -31.9     | 39.7                      | 130                          | 103                 | 420               |
| 37               | 0.090 | 0.735 | -29.6     | 51.8                      | 170                          | 136                 | 398               |
| 36               | 0.113 | 0.735 | -27.6     | 65.1                      | 213                          | 173                 | 375               |
| 35               | 0.136 | 0.735 | -26.0     | 78.3                      | 257                          | 210                 | 353               |
| 34               | 0.161 | 0.735 | -24.6     | 92.7                      | 304                          | 252                 | 330               |
| 33               | 0.187 | 0.735 | -23.3     | 107.7                     | 353                          | 296                 | 308               |
| 32               | 0.215 | 0.735 | -22.0     | 123.8                     | 406                          | 344                 | 285               |
| 31               | 0.243 | 0.735 | -21.0     | 139.9                     | 459                          | 393                 | 264               |
| 30               | 0.273 | 0.735 | -20.0     | 157.2                     | 516                          | 447                 | 242               |
| 29               | 0.303 | 0.735 | -19.1     | 174.5                     | 572                          | 501                 | 223               |
| 28               | 0.333 | 0.735 | -18.2     | 191.7                     | 629                          | 555                 | 205               |
| 27               | 0.365 | 0.735 | -17.4     | 210.2                     | 690                          | 614                 | 187               |
| 26               | 0.398 | 0.735 | -16.7     | 229.2                     | 752                          | 676                 | 170               |
| 25               | 0.431 | 0.735 | -16.0     | 248.2                     | 814                          | 738                 | 156               |
| 24               | 0.464 | 0.735 | -15.4     | 267.2                     | 877                          | 801                 | 143               |
| 23               | 0.496 | 0.735 | -14.8     | 285.6                     | 937                          | 862                 | 134               |
| 22               | 0.530 | 0.735 | -14.2     | 305.2                     | 1001                         | 928                 | 125               |
| 21               | 0.563 | 0.735 | -13.7     | 324.2                     | 1064                         | 993                 | 119               |
| 20               | 0.596 | 0.735 | -13.2     | 343.2                     | 1126                         | 1058                | 115               |
| 19               | 0.629 | 0.735 | -12.7     | 362.2                     | 1188                         | 1123                | 113               |
| 18               | 0.661 | 0.735 | -12.3     | 380.6                     | 1249                         | 1188                | 114               |
| 17               | 0.692 | 0.735 | -11.9     | 398.4                     | 1307                         | 1250                | 118               |
| 16               | 0.724 | 0.735 | -11.5     | 416.9                     | 1368                         | 1315                | 123               |
| 15               | 0.754 | 0.735 | -11.1     | 434.1                     | 1424                         | 1376                | 131               |
| 14               | 0.782 | 0.735 | -10.8     | 450.3                     | 1477                         | 1433                | 143               |
| 13               | 0.810 | 0.735 | -10.5     | 466.4                     | 1530                         | 1491                | 156               |
| 12               | 0.836 | 0.735 | -10.3     | 481.4                     | 1579                         | 1545                | 172               |
| 11               | 0.861 | 0.735 | -10.0     | 495.7                     | 1626                         | 1597                | 190               |
| 10               | 0.885 | 0.735 | -9.8      | 509.6                     | 1672                         | 1646                | 210               |
| 9                | 0.905 | 0.735 | -9.6      | 521.1                     | 1710                         | 1689                | 233               |
| 8                | 0.924 | 0.735 | -9.4      | 532.0                     | 1745                         | 1728                | 257               |
| 7                | 0.940 | 0.735 | -9.2      | 541.2                     | 1776                         | 1762                | 284               |
| 6                | 0.956 | 0.735 | -9.1      | 550.4                     | 1806                         | 1796                | 311               |
| 5                | 0.969 | 0.735 | -9.0      | 557.9                     | 1830                         | 1824                | 340               |
| 4                | 0.979 | 0.735 | -8.9      | 563.7                     | 1849                         | 1845                | 371               |
| 3                | 0.987 | 0.735 | -8.8      | 568.3                     | 1864                         | 1862                | 402               |
| 2                | 0.994 | 0.735 | -8.7      | 572.3                     | 1878                         | 1877                | 434               |
| 1                | 0.997 | 0.735 | -8.7      | 574.1                     | 1883                         | 1883                | 467               |
| 0                | 1.000 | 0.735 | -8.7      | 575.8                     | 1889                         | 1889                | 500               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 113

Figure 11B

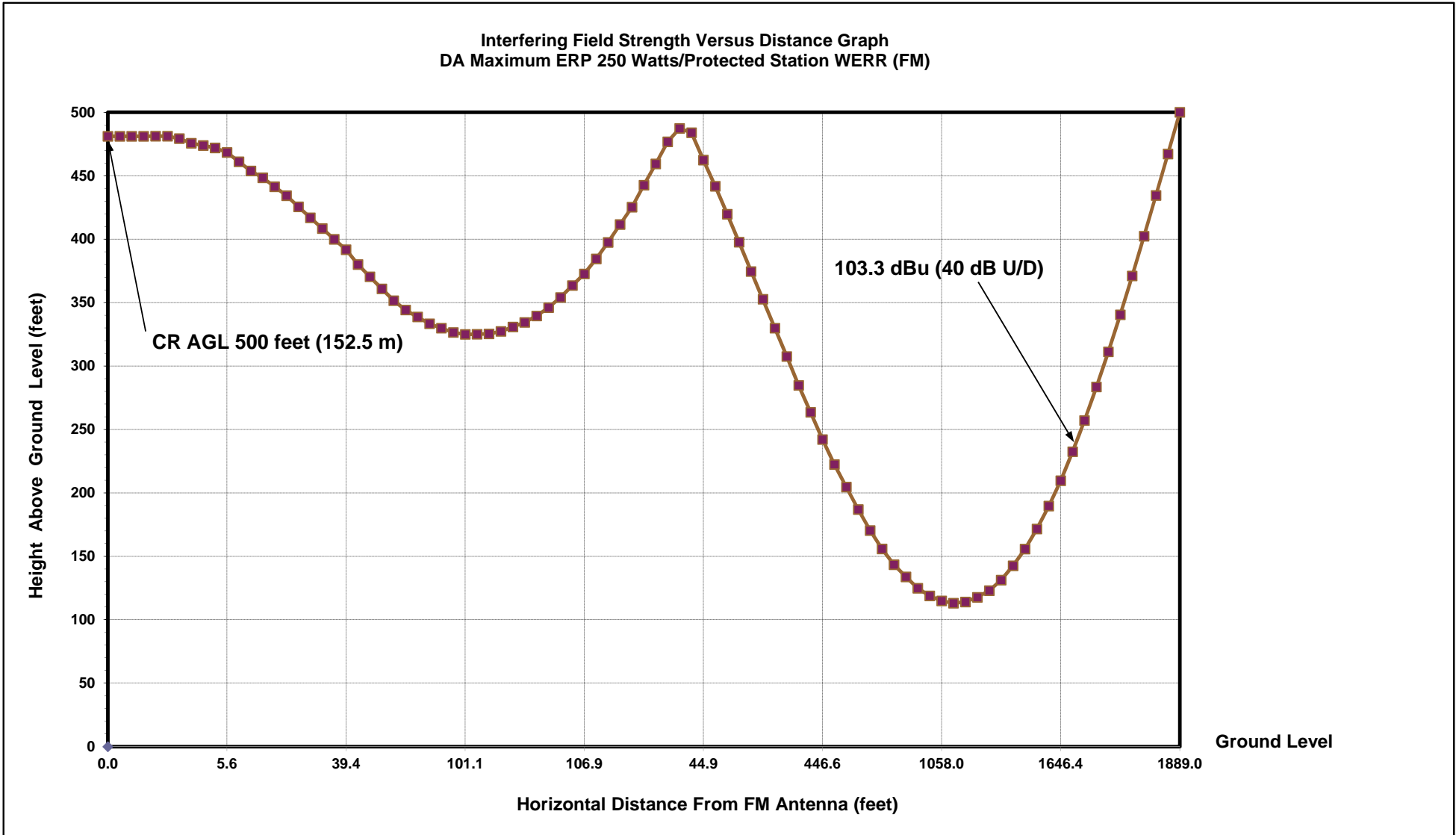


Figure 12A

## Interfering Field Strength Vs. Distance Graph - W279BU to WERR (FM) - Point "G", Figure 6

|                     |  |  |     |                 |  |  |  |
|---------------------|--|--|-----|-----------------|--|--|--|
| Antenna             | SCA: 3 X CL-FM/HRM/50N Lod-periodic Array, vertical stacked 0.5 wavelength |  |     |                 |  |  |  |
| RCAGL               | 467 feet   |  | ERP | 0.25 kW         |  |  |  |
| Interfering Contour | 103.3 dBu  |  |     | -6.02059991 dBk |  |  |  |

172'+295'=467'

410 MTS ELEV. TERR

41° AZIM

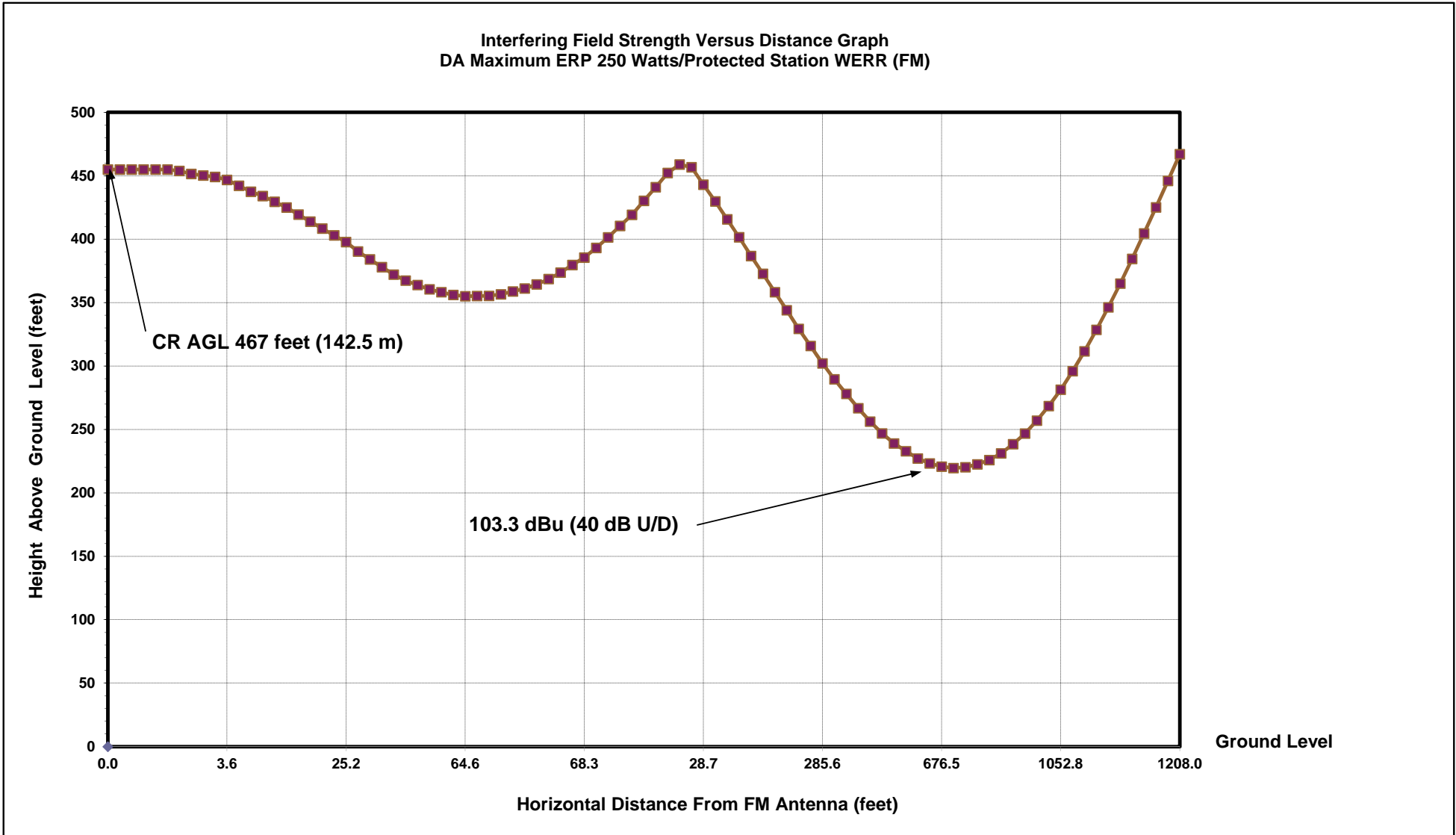
| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 90               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 0                   | 455               |
| 89               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 0                   | 455               |
| 88               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 0                   | 455               |
| 87               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 1                   | 455               |
| 86               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 1                   | 455               |
| 85               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 1                   | 455               |
| 84               | 0.011 | 0.470 | -51.8     | 4.1                       | 13                           | 1                   | 454               |
| 83               | 0.013 | 0.470 | -50.3     | 4.8                       | 16                           | 2                   | 451               |
| 82               | 0.014 | 0.470 | -49.7     | 5.2                       | 17                           | 2                   | 450               |
| 81               | 0.015 | 0.470 | -49.1     | 5.5                       | 18                           | 3                   | 449               |
| 80               | 0.017 | 0.470 | -48.0     | 6.3                       | 21                           | 4                   | 447               |
| 79               | 0.021 | 0.470 | -46.1     | 7.7                       | 25                           | 5                   | 442               |
| 78               | 0.025 | 0.470 | -44.6     | 9.2                       | 30                           | 6                   | 437               |
| 77               | 0.028 | 0.470 | -43.6     | 10.3                      | 34                           | 8                   | 434               |
| 76               | 0.032 | 0.470 | -42.5     | 11.8                      | 39                           | 9                   | 429               |
| 75               | 0.036 | 0.470 | -41.5     | 13.3                      | 43                           | 11                  | 425               |
| 74               | 0.041 | 0.470 | -40.3     | 15.1                      | 50                           | 14                  | 419               |
| 73               | 0.046 | 0.470 | -39.3     | 16.9                      | 56                           | 16                  | 414               |
| 72               | 0.051 | 0.470 | -38.4     | 18.8                      | 62                           | 19                  | 408               |
| 71               | 0.056 | 0.470 | -37.6     | 20.6                      | 68                           | 22                  | 403               |
| 70               | 0.061 | 0.470 | -36.9     | 22.5                      | 74                           | 25                  | 398               |
| 69               | 0.068 | 0.470 | -35.9     | 25.0                      | 82                           | 29                  | 390               |
| 68               | 0.074 | 0.470 | -35.2     | 27.2                      | 89                           | 33                  | 384               |
| 67               | 0.080 | 0.470 | -34.5     | 29.5                      | 97                           | 38                  | 378               |
| 66               | 0.086 | 0.470 | -33.9     | 31.7                      | 104                          | 42                  | 372               |
| 65               | 0.091 | 0.470 | -33.4     | 33.5                      | 110                          | 46                  | 367               |
| 64               | 0.095 | 0.470 | -33.0     | 35.0                      | 115                          | 50                  | 364               |
| 63               | 0.099 | 0.470 | -32.7     | 36.5                      | 120                          | 54                  | 360               |
| 62               | 0.102 | 0.470 | -32.4     | 37.6                      | 123                          | 58                  | 358               |
| 61               | 0.105 | 0.470 | -32.2     | 38.7                      | 127                          | 61                  | 356               |
| 60               | 0.107 | 0.470 | -32.0     | 39.4                      | 129                          | 65                  | 355               |
| 59               | 0.108 | 0.470 | -31.9     | 39.8                      | 130                          | 67                  | 355               |
| 58               | 0.109 | 0.470 | -31.8     | 40.1                      | 132                          | 70                  | 355               |
| 57               | 0.109 | 0.470 | -31.8     | 40.1                      | 132                          | 72                  | 357               |
| 56               | 0.108 | 0.470 | -31.9     | 39.8                      | 130                          | 73                  | 359               |
| 55               | 0.107 | 0.470 | -32.0     | 39.4                      | 129                          | 74                  | 361               |
| 54               | 0.105 | 0.470 | -32.2     | 38.7                      | 127                          | 75                  | 364               |
| 53               | 0.102 | 0.470 | -32.4     | 37.6                      | 123                          | 74                  | 369               |
| 52               | 0.098 | 0.470 | -32.8     | 36.1                      | 118                          | 73                  | 374               |
| 51               | 0.093 | 0.470 | -33.2     | 34.2                      | 112                          | 71                  | 380               |
| 50               | 0.088 | 0.470 | -33.7     | 32.4                      | 106                          | 68                  | 386               |
| 49               | 0.081 | 0.470 | -34.4     | 29.8                      | 98                           | 64                  | 393               |
| 48               | 0.073 | 0.470 | -35.3     | 26.9                      | 88                           | 59                  | 401               |
| 47               | 0.064 | 0.470 | -36.5     | 23.6                      | 77                           | 53                  | 410               |

| Depression Angle | VRF   | HRF   | ERP (dBk) | Distance to Contour (m)** | Distance to Contour (feet)** | Horiz. Dist. (feet) | Height AGL (feet) |
|------------------|-------|-------|-----------|---------------------------|------------------------------|---------------------|-------------------|
| 46               | 0.055 | 0.470 | -37.8     | 20.3                      | 66                           | 46                  | 419               |
| 45               | 0.043 | 0.470 | -39.9     | 15.8                      | 52                           | 37                  | 430               |
| 44               | 0.031 | 0.470 | -42.8     | 11.4                      | 37                           | 27                  | 441               |
| 43               | 0.018 | 0.470 | -47.5     | 6.6                       | 22                           | 16                  | 452               |
| 42               | 0.010 | 0.470 | -52.6     | 3.7                       | 12                           | 9                   | 459               |
| 41               | 0.013 | 0.470 | -50.3     | 4.8                       | 16                           | 12                  | 457               |
| 40               | 0.031 | 0.470 | -42.8     | 11.4                      | 37                           | 29                  | 443               |
| 39               | 0.049 | 0.470 | -38.8     | 18.0                      | 59                           | 46                  | 430               |
| 38               | 0.069 | 0.470 | -35.8     | 25.4                      | 83                           | 66                  | 416               |
| 37               | 0.090 | 0.470 | -33.5     | 33.1                      | 109                          | 87                  | 402               |
| 36               | 0.113 | 0.470 | -31.5     | 41.6                      | 136                          | 110                 | 387               |
| 35               | 0.136 | 0.470 | -29.9     | 50.1                      | 164                          | 135                 | 373               |
| 34               | 0.161 | 0.470 | -28.4     | 59.3                      | 194                          | 161                 | 358               |
| 33               | 0.187 | 0.470 | -27.1     | 68.9                      | 226                          | 189                 | 344               |
| 32               | 0.215 | 0.470 | -25.9     | 79.2                      | 260                          | 220                 | 329               |
| 31               | 0.243 | 0.470 | -24.9     | 89.5                      | 294                          | 252                 | 316               |
| 30               | 0.273 | 0.470 | -23.9     | 100.5                     | 330                          | 286                 | 302               |
| 29               | 0.303 | 0.470 | -22.9     | 111.6                     | 366                          | 320                 | 290               |
| 28               | 0.333 | 0.470 | -22.1     | 122.6                     | 402                          | 355                 | 278               |
| 27               | 0.365 | 0.470 | -21.3     | 134.4                     | 441                          | 393                 | 267               |
| 26               | 0.398 | 0.470 | -20.6     | 146.5                     | 481                          | 432                 | 256               |
| 25               | 0.431 | 0.470 | -19.9     | 158.7                     | 521                          | 472                 | 247               |
| 24               | 0.464 | 0.470 | -19.2     | 170.8                     | 560                          | 512                 | 239               |
| 23               | 0.496 | 0.470 | -18.7     | 182.6                     | 599                          | 552                 | 233               |
| 22               | 0.530 | 0.470 | -18.1     | 195.1                     | 640                          | 594                 | 227               |
| 21               | 0.563 | 0.470 | -17.6     | 207.3                     | 680                          | 635                 | 223               |
| 20               | 0.596 | 0.470 | -17.1     | 219.4                     | 720                          | 677                 | 221               |
| 19               | 0.629 | 0.470 | -16.6     | 231.6                     | 760                          | 718                 | 220               |
| 18               | 0.661 | 0.470 | -16.2     | 243.4                     | 798                          | 759                 | 220               |
| 17               | 0.692 | 0.470 | -15.8     | 254.8                     | 836                          | 799                 | 223               |
| 16               | 0.724 | 0.470 | -15.4     | 266.6                     | 875                          | 841                 | 226               |
| 15               | 0.754 | 0.470 | -15.0     | 277.6                     | 911                          | 880                 | 231               |
| 14               | 0.782 | 0.470 | -14.7     | 287.9                     | 945                          | 917                 | 238               |
| 13               | 0.810 | 0.470 | -14.4     | 298.2                     | 978                          | 953                 | 247               |
| 12               | 0.836 | 0.470 | -14.1     | 307.8                     | 1010                         | 988                 | 257               |
| 11               | 0.861 | 0.470 | -13.9     | 317.0                     | 1040                         | 1021                | 269               |
| 10               | 0.885 | 0.470 | -13.6     | 325.8                     | 1069                         | 1053                | 281               |
| 9                | 0.905 | 0.470 | -13.4     | 333.2                     | 1093                         | 1080                | 296               |
| 8                | 0.924 | 0.470 | -13.3     | 340.2                     | 1116                         | 1105                | 312               |
| 7                | 0.940 | 0.470 | -13.1     | 346.1                     | 1135                         | 1127                | 329               |
| 6                | 0.956 | 0.470 | -13.0     | 352.0                     | 1155                         | 1148                | 346               |
| 5                | 0.969 | 0.470 | -12.9     | 356.8                     | 1171                         | 1166                | 365               |
| 4                | 0.979 | 0.470 | -12.8     | 360.5                     | 1183                         | 1180                | 385               |
| 3                | 0.987 | 0.470 | -12.7     | 363.4                     | 1192                         | 1191                | 405               |
| 2                | 0.994 | 0.470 | -12.6     | 366.0                     | 1201                         | 1200                | 425               |
| 1                | 0.997 | 0.470 | -12.6     | 367.1                     | 1204                         | 1204                | 446               |
| 0                | 1.000 | 0.470 | -12.6     | 368.2                     | 1208                         | 1208                | 467               |

\*\*Free Space Field Equation: Di Dist. (km)=LOG-1((107.2+P(DBK)-FS)/20)

Min. Hgth.: 220

Figure 12B



TECHNICAL EXHIBIT  
APPLICATION FOR  
MINOR CHANGE IN LICENSED FACILITY  
AURIO A. MATOS BARRETO.  
FM TRANSLATOR STATION W279BU  
SAN JUAN, PUERTO RICO  
FACILITY ID 143465

CH 279 0.25 KW 552 M AMSL

Notification Letter to Arecibo Observatory

*{one sheet follows}*



201 Fletcher Ave.  
Sarasota, FL 34237-6019  
941-329-6000  
941-329-6031 FAX

**Grafton Olivera**  
Direct Dial 941-329-6001  
e-mail: [grifton@dlr.com](mailto:grifton@dlr.com)

August 8, 2014

Via email ([prcz@naic.edu](mailto:prcz@naic.edu))

Angel M. Vázquez, Spectrum Manager  
National Astronomy and Ionosphere Center  
Arecibo Observatory  
HC3 Box 53995  
Arecibo, PR 00612

Gentleman:

On behalf of our client, Aurio A. Matos Barreto, licensee of FM Translator Station W279BU, Gurabo, Puerto Rico, in accordance with Section 73.1030 of the FCC Rules, we are hereby notifying you of proposed changes in the facility of W279BU. The particulars of the proposal are as follows:

Proposed Facility:

Geographical coordinates of antenna location (NAD27): 18-16-49.3 / 66-06-35.3  
Antenna height (Scala CL-FM/VRM, Log Periodic Array): 52.4 m AGL; 552.5 m AMSL  
Antenna Gain: 10.9 dB  
Antenna Orientation: 0° True  
Operating channel: 279 (103.7 MHz)  
Type of emission: F3E  
Effective isotropic radiated power: 0.41 kW – Vertical Polarization

Please review this proposal and let us know your findings. Please feel free to communicate via email (<mailto:grifton@dlr.com>), telefax (941-329-6030) or regular mail.

Very truly yours,

Grafton Olivera, P.E.

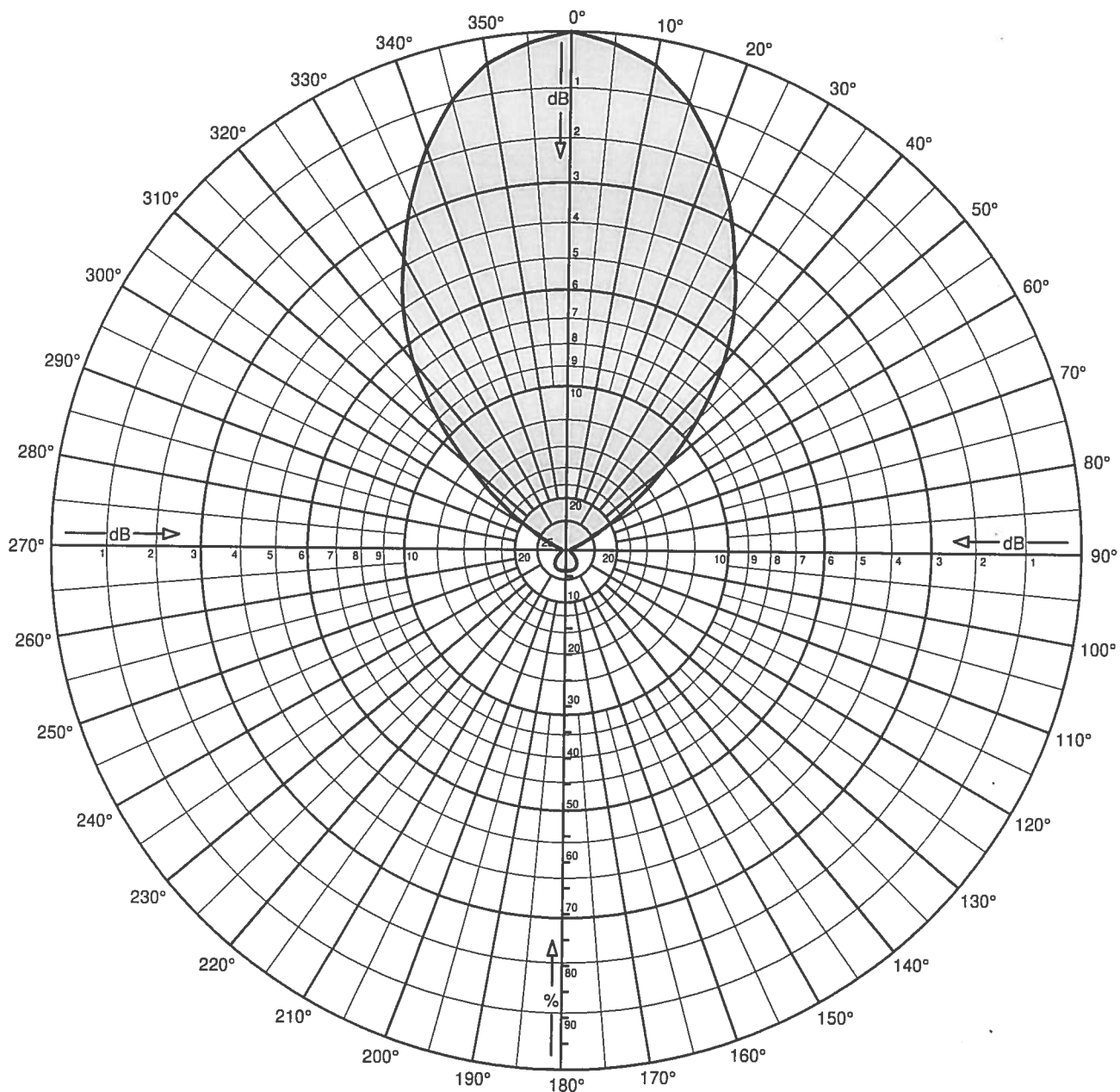


TECHNICAL EXHIBIT  
APPLICATION FOR  
MINOR CHANGE IN LICENSED FACILITY  
AURIO A. MATOS BARRETO.  
FM TRANSLATOR STATION W279BU  
SAN JUAN, PUERTO RICO  
FACILITY ID 143465

CH 279 0.25 KW 552 M AMSL

Antenna Pattern Data

*{five sheets follow}*



3 x CL-FM/HRM/50N Log-periodic Array

Frequency:        MHz

Oriented at 0 degrees

Gain: 10.9 dBd (x 12.3)

Horizontal Polarization

Vertical stacked 0.5 wavelength

Horizontal plane Pattern



3 x CL-FM/HRM/50N Log-periodic Array

Frequency: MHz

Oriented at 0 degrees

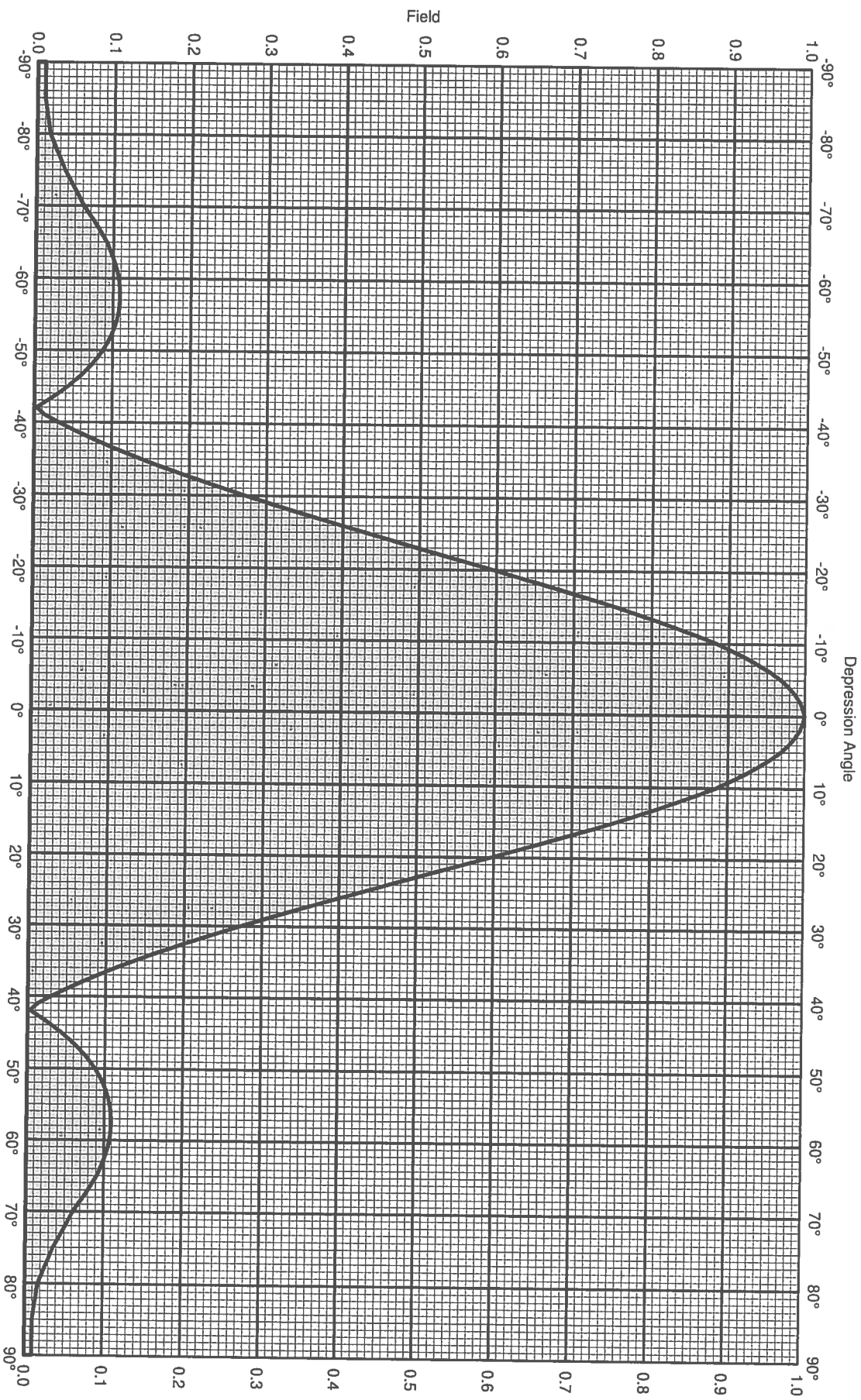
Gain: 10.9 dBd (x 12.3)

Horizontal Polarization

Vertical stacked 0.5 wavelength

Horizontal plane Pattern

| Angle | Field | Rel.dB | dBd    | PwrMult | Angle | Field | Rel.dB | dBd    | PwrMult |
|-------|-------|--------|--------|---------|-------|-------|--------|--------|---------|
| 0     | 1.000 | 0.00   | 10.90  | 12.30   | 180   | 0.040 | -27.96 | -17.06 | 0.02    |
| 5     | 0.980 | -0.18  | 10.72  | 11.82   | 185   | 0.040 | -27.96 | -17.06 | 0.02    |
| 10    | 0.950 | -0.45  | 10.45  | 11.10   | 190   | 0.040 | -27.96 | -17.06 | 0.02    |
| 15    | 0.895 | -0.96  | 9.94   | 9.85    | 195   | 0.040 | -27.96 | -17.06 | 0.02    |
| 20    | 0.820 | -1.72  | 9.18   | 8.27    | 200   | 0.040 | -27.96 | -17.06 | 0.02    |
| 25    | 0.735 | -2.67  | 8.23   | 6.65    | 205   | 0.039 | -28.07 | -17.17 | 0.02    |
| 30    | 0.645 | -3.81  | 7.09   | 5.12    | 210   | 0.038 | -28.29 | -17.39 | 0.02    |
| 35    | 0.562 | -5.00  | 5.90   | 3.89    | 215   | 0.036 | -28.87 | -17.97 | 0.02    |
| 40    | 0.470 | -6.56  | 4.34   | 2.72    | 220   | 0.034 | -29.50 | -18.60 | 0.01    |
| 45    | 0.360 | -8.87  | 2.03   | 1.59    | 225   | 0.029 | -30.75 | -19.85 | 0.01    |
| 50    | 0.250 | -12.04 | -1.14  | 0.77    | 230   | 0.025 | -32.04 | -21.14 | 0.01    |
| 55    | 0.155 | -16.19 | -5.29  | 0.30    | 235   | 0.020 | -33.98 | -23.08 | 0.00    |
| 60    | 0.085 | -21.41 | -10.51 | 0.09    | 240   | 0.015 | -36.48 | -25.58 | 0.00    |
| 65    | 0.045 | -26.94 | -16.04 | 0.02    | 245   | 0.012 | -38.06 | -27.16 | 0.00    |
| 70    | 0.020 | -33.98 | -23.08 | 0.00    | 250   | 0.010 | -40.00 | -29.10 | 0.00    |
| 75    | 0.010 | -40.00 | -29.10 | 0.00    | 255   | 0.010 | -40.00 | -29.10 | 0.00    |
| 80    | 0.010 | -40.00 | -29.10 | 0.00    | 260   | 0.010 | -40.00 | -29.10 | 0.00    |
| 85    | 0.010 | -40.00 | -29.10 | 0.00    | 265   | 0.010 | -40.00 | -29.10 | 0.00    |
| 90    | 0.010 | -40.00 | -29.10 | 0.00    | 270   | 0.010 | -40.00 | -29.10 | 0.00    |
| 95    | 0.010 | -40.00 | -29.10 | 0.00    | 275   | 0.010 | -40.00 | -29.10 | 0.00    |
| 100   | 0.010 | -40.00 | -29.10 | 0.00    | 280   | 0.010 | -40.00 | -29.10 | 0.00    |
| 105   | 0.010 | -40.00 | -29.10 | 0.00    | 285   | 0.010 | -40.00 | -29.10 | 0.00    |
| 110   | 0.010 | -40.00 | -29.10 | 0.00    | 290   | 0.020 | -33.98 | -23.08 | 0.00    |
| 115   | 0.012 | -38.06 | -27.16 | 0.00    | 295   | 0.045 | -26.94 | -16.04 | 0.02    |
| 120   | 0.015 | -36.48 | -25.58 | 0.00    | 300   | 0.085 | -21.41 | -10.51 | 0.09    |
| 125   | 0.020 | -33.98 | -23.08 | 0.00    | 305   | 0.155 | -16.19 | -5.29  | 0.30    |
| 130   | 0.025 | -32.04 | -21.14 | 0.01    | 310   | 0.250 | -12.04 | -1.14  | 0.77    |
| 135   | 0.029 | -30.75 | -19.85 | 0.01    | 315   | 0.360 | -8.87  | 2.03   | 1.59    |
| 140   | 0.034 | -29.50 | -18.60 | 0.01    | 320   | 0.470 | -6.56  | 4.34   | 2.72    |
| 145   | 0.036 | -28.87 | -17.97 | 0.02    | 325   | 0.562 | -5.00  | 5.90   | 3.89    |
| 150   | 0.038 | -28.29 | -17.39 | 0.02    | 330   | 0.645 | -3.81  | 7.09   | 5.12    |
| 155   | 0.039 | -28.07 | -17.17 | 0.02    | 335   | 0.735 | -2.67  | 8.23   | 6.65    |
| 160   | 0.040 | -27.96 | -17.06 | 0.02    | 340   | 0.820 | -1.72  | 9.18   | 8.27    |
| 165   | 0.040 | -27.96 | -17.06 | 0.02    | 345   | 0.895 | -0.96  | 9.94   | 9.85    |
| 170   | 0.040 | -27.96 | -17.06 | 0.02    | 350   | 0.950 | -0.45  | 10.45  | 11.10   |
| 175   | 0.040 | -27.96 | -17.06 | 0.02    | 355   | 0.980 | -0.18  | 10.72  | 11.82   |



**KATHREIN**  
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<http://www.kathrein-scala.com>

3 x CL-FM/HRM/50N Log-periodic Array

Frequency: MHz

Oriented at 0 degrees

Gain: 10.9 dBd (x 12.3)

Horizontal Polarization

Vertical stacked 0.5 wavelength

Vertical plane Pattern



3 x CL-FM/HRM/50N Log-periodic Array

Frequency: MHz

Oriented at 0 degrees

Gain: 10.9 dBd (x 12.3)

Horizontal Polarization

Vertical stacked 0.5 wavelength

Vertical plane Pattern

| Angle | Field | Rel.dB | dBd    | PwrMult | Angle | Field | Rel.dB | dBd    | PwrMult |
|-------|-------|--------|--------|---------|-------|-------|--------|--------|---------|
| 0     | 1.000 | 0.00   | 10.90  | 12.30   | 45    | 0.043 | -27.23 | -16.33 | 0.02    |
| 1     | 0.997 | -0.02  | 10.88  | 12.24   | 46    | 0.055 | -25.27 | -14.37 | 0.04    |
| 2     | 0.994 | -0.06  | 10.84  | 12.14   | 47    | 0.064 | -23.81 | -12.91 | 0.05    |
| 3     | 0.987 | -0.11  | 10.79  | 11.99   | 48    | 0.073 | -22.71 | -11.81 | 0.07    |
| 4     | 0.979 | -0.18  | 10.72  | 11.79   | 49    | 0.081 | -21.83 | -10.93 | 0.08    |
| 5     | 0.969 | -0.28  | 10.62  | 11.55   | 50    | 0.088 | -21.15 | -10.25 | 0.09    |
| 6     | 0.956 | -0.39  | 10.51  | 11.24   | 51    | 0.093 | -20.61 | -9.71  | 0.11    |
| 7     | 0.940 | -0.53  | 10.37  | 10.88   | 52    | 0.098 | -20.18 | -9.28  | 0.12    |
| 8     | 0.924 | -0.69  | 10.21  | 10.50   | 53    | 0.102 | -19.85 | -8.95  | 0.13    |
| 9     | 0.905 | -0.87  | 10.03  | 10.08   | 54    | 0.105 | -19.61 | -8.71  | 0.13    |
| 10    | 0.885 | -1.06  | 9.84   | 9.64    | 55    | 0.107 | -19.42 | -8.52  | 0.14    |
| 11    | 0.861 | -1.30  | 9.60   | 9.13    | 56    | 0.108 | -19.31 | -8.41  | 0.14    |
| 12    | 0.836 | -1.56  | 9.34   | 8.60    | 57    | 0.109 | -19.26 | -8.36  | 0.15    |
| 13    | 0.810 | -1.83  | 9.07   | 8.07    | 58    | 0.109 | -19.26 | -8.36  | 0.15    |
| 14    | 0.782 | -2.13  | 8.77   | 7.53    | 59    | 0.108 | -19.30 | -8.40  | 0.14    |
| 15    | 0.754 | -2.45  | 8.45   | 6.99    | 60    | 0.107 | -19.39 | -8.49  | 0.14    |
| 16    | 0.724 | -2.81  | 8.09   | 6.44    | 61    | 0.105 | -19.58 | -8.68  | 0.14    |
| 17    | 0.692 | -3.19  | 7.71   | 5.90    | 62    | 0.102 | -19.81 | -8.91  | 0.13    |
| 18    | 0.661 | -3.60  | 7.30   | 5.37    | 63    | 0.099 | -20.09 | -9.19  | 0.12    |
| 19    | 0.629 | -4.03  | 6.87   | 4.86    | 64    | 0.095 | -20.41 | -9.51  | 0.11    |
| 20    | 0.596 | -4.49  | 6.41   | 4.38    | 65    | 0.091 | -20.78 | -9.88  | 0.10    |
| 21    | 0.563 | -4.99  | 5.91   | 3.90    | 66    | 0.086 | -21.32 | -10.42 | 0.09    |
| 22    | 0.530 | -5.52  | 5.38   | 3.45    | 67    | 0.080 | -21.93 | -11.03 | 0.08    |
| 23    | 0.496 | -6.08  | 4.82   | 3.03    | 68    | 0.074 | -22.62 | -11.72 | 0.07    |
| 24    | 0.464 | -6.68  | 4.22   | 2.64    | 69    | 0.068 | -23.40 | -12.50 | 0.06    |
| 25    | 0.431 | -7.31  | 3.59   | 2.28    | 70    | 0.061 | -24.28 | -13.38 | 0.05    |
| 26    | 0.398 | -8.01  | 2.89   | 1.95    | 71    | 0.056 | -24.99 | -14.09 | 0.04    |
| 27    | 0.365 | -8.75  | 2.15   | 1.64    | 72    | 0.051 | -25.78 | -14.88 | 0.03    |
| 28    | 0.333 | -9.54  | 1.36   | 1.37    | 73    | 0.046 | -26.66 | -15.76 | 0.03    |
| 29    | 0.303 | -10.38 | 0.52   | 1.13    | 74    | 0.041 | -27.66 | -16.76 | 0.02    |
| 30    | 0.273 | -11.29 | -0.39  | 0.91    | 75    | 0.036 | -28.81 | -17.91 | 0.02    |
| 31    | 0.243 | -12.28 | -1.38  | 0.73    | 76    | 0.032 | -29.79 | -18.89 | 0.01    |
| 32    | 0.215 | -13.37 | -2.47  | 0.57    | 77    | 0.028 | -30.91 | -20.01 | 0.01    |
| 33    | 0.187 | -14.54 | -3.64  | 0.43    | 78    | 0.025 | -32.20 | -21.30 | 0.01    |
| 34    | 0.161 | -15.85 | -4.95  | 0.32    | 79    | 0.021 | -33.72 | -22.82 | 0.01    |
| 35    | 0.136 | -17.30 | -6.40  | 0.23    | 80    | 0.017 | -35.58 | -24.68 | 0.00    |
| 36    | 0.113 | -18.96 | -8.06  | 0.16    | 81    | 0.015 | -36.30 | -25.40 | 0.00    |
| 37    | 0.090 | -20.89 | -9.99  | 0.10    | 82    | 0.014 | -37.09 | -26.19 | 0.00    |
| 38    | 0.069 | -23.22 | -12.32 | 0.06    | 83    | 0.013 | -37.95 | -27.05 | 0.00    |
| 39    | 0.049 | -26.16 | -15.26 | 0.03    | 84    | 0.011 | -38.92 | -28.02 | 0.00    |
| 40    | 0.031 | -30.31 | -19.41 | 0.01    | 85    | 0.010 | -40.00 | -29.10 | 0.00    |
| 41    | 0.013 | -37.62 | -26.72 | 0.00    | 86    | 0.010 | -40.00 | -29.10 | 0.00    |
| 42    | 0.010 | -40.00 | -29.10 | 0.00    | 87    | 0.010 | -40.00 | -29.10 | 0.00    |
| 43    | 0.018 | -35.04 | -24.14 | 0.00    | 88    | 0.010 | -40.00 | -29.10 | 0.00    |
| 44    | 0.031 | -30.11 | -19.21 | 0.01    | 89    | 0.010 | -40.00 | -29.10 | 0.00    |
|       |       |        |        |         | 90    | 0.010 | -40.00 | -29.10 | 0.00    |



3 x CL-FM/HRM/50N Log-periodic Array

Frequency: MHz

Oriented at 0 degrees

Gain: 10.9 dBd (x 12.3)

Horizontal Polarization

Vertical stacked 0.5 wavelength

Vertical plane Pattern

| Angle | Field | Rel.dB | dBd    | PwrMult | Angle | Field | Rel.dB | dBd    | PwrMult |
|-------|-------|--------|--------|---------|-------|-------|--------|--------|---------|
| -90   | 0.010 | -40.00 | -29.10 | 0.00    | -45   | 0.043 | -27.23 | -16.33 | 0.02    |
| -89   | 0.010 | -40.00 | -29.10 | 0.00    | -44   | 0.031 | -30.11 | -19.21 | 0.01    |
| -88   | 0.010 | -40.00 | -29.10 | 0.00    | -43   | 0.018 | -35.04 | -24.14 | 0.00    |
| -87   | 0.010 | -40.00 | -29.10 | 0.00    | -42   | 0.010 | -40.00 | -29.10 | 0.00    |
| -86   | 0.010 | -40.00 | -29.10 | 0.00    | -41   | 0.013 | -37.63 | -26.73 | 0.00    |
| -85   | 0.010 | -40.00 | -29.10 | 0.00    | -40   | 0.031 | -30.31 | -19.41 | 0.01    |
| -84   | 0.011 | -38.92 | -28.02 | 0.00    | -39   | 0.049 | -26.16 | -15.26 | 0.03    |
| -83   | 0.013 | -37.95 | -27.05 | 0.00    | -38   | 0.069 | -23.22 | -12.32 | 0.06    |
| -82   | 0.014 | -37.09 | -26.19 | 0.00    | -37   | 0.090 | -20.89 | -9.99  | 0.10    |
| -81   | 0.015 | -36.30 | -25.40 | 0.00    | -36   | 0.113 | -18.96 | -8.06  | 0.16    |
| -80   | 0.017 | -35.58 | -24.68 | 0.00    | -35   | 0.136 | -17.30 | -6.40  | 0.23    |
| -79   | 0.021 | -33.72 | -22.82 | 0.01    | -34   | 0.161 | -15.85 | -4.95  | 0.32    |
| -78   | 0.025 | -32.20 | -21.30 | 0.01    | -33   | 0.187 | -14.54 | -3.64  | 0.43    |
| -77   | 0.028 | -30.91 | -20.01 | 0.01    | -32   | 0.215 | -13.37 | -2.47  | 0.57    |
| -76   | 0.032 | -29.79 | -18.89 | 0.01    | -31   | 0.243 | -12.28 | -1.38  | 0.73    |
| -75   | 0.036 | -28.81 | -17.91 | 0.02    | -30   | 0.273 | -11.29 | -0.39  | 0.91    |
| -74   | 0.041 | -27.66 | -16.76 | 0.02    | -29   | 0.303 | -10.38 | 0.52   | 1.13    |
| -73   | 0.046 | -26.66 | -15.76 | 0.03    | -28   | 0.333 | -9.54  | 1.36   | 1.37    |
| -72   | 0.051 | -25.78 | -14.88 | 0.03    | -27   | 0.365 | -8.75  | 2.15   | 1.64    |
| -71   | 0.056 | -24.99 | -14.09 | 0.04    | -26   | 0.398 | -8.01  | 2.89   | 1.95    |
| -70   | 0.061 | -24.28 | -13.38 | 0.05    | -25   | 0.431 | -7.31  | 3.59   | 2.28    |
| -69   | 0.068 | -23.40 | -12.50 | 0.06    | -24   | 0.464 | -6.68  | 4.22   | 2.64    |
| -68   | 0.074 | -22.62 | -11.72 | 0.07    | -23   | 0.496 | -6.08  | 4.82   | 3.03    |
| -67   | 0.080 | -21.93 | -11.03 | 0.08    | -22   | 0.530 | -5.52  | 5.38   | 3.45    |
| -66   | 0.086 | -21.32 | -10.42 | 0.09    | -21   | 0.563 | -4.99  | 5.91   | 3.90    |
| -65   | 0.091 | -20.78 | -9.88  | 0.10    | -20   | 0.596 | -4.49  | 6.41   | 4.38    |
| -64   | 0.095 | -20.41 | -9.51  | 0.11    | -19   | 0.629 | -4.03  | 6.87   | 4.86    |
| -63   | 0.099 | -20.09 | -9.19  | 0.12    | -18   | 0.661 | -3.60  | 7.30   | 5.37    |
| -62   | 0.102 | -19.81 | -8.91  | 0.13    | -17   | 0.692 | -3.19  | 7.71   | 5.90    |
| -61   | 0.105 | -19.58 | -8.68  | 0.14    | -16   | 0.724 | -2.81  | 8.09   | 6.44    |
| -60   | 0.107 | -19.39 | -8.49  | 0.14    | -15   | 0.754 | -2.45  | 8.45   | 6.99    |
| -59   | 0.108 | -19.30 | -8.40  | 0.14    | -14   | 0.782 | -2.13  | 8.77   | 7.53    |
| -58   | 0.109 | -19.26 | -8.36  | 0.15    | -13   | 0.810 | -1.83  | 9.07   | 8.07    |
| -57   | 0.109 | -19.26 | -8.36  | 0.15    | -12   | 0.836 | -1.56  | 9.34   | 8.60    |
| -56   | 0.108 | -19.31 | -8.41  | 0.14    | -11   | 0.861 | -1.30  | 9.60   | 9.13    |
| -55   | 0.107 | -19.42 | -8.52  | 0.14    | -10   | 0.885 | -1.06  | 9.84   | 9.64    |
| -54   | 0.105 | -19.61 | -8.71  | 0.13    | -9    | 0.905 | -0.87  | 10.03  | 10.08   |
| -53   | 0.102 | -19.85 | -8.95  | 0.13    | -8    | 0.924 | -0.69  | 10.21  | 10.50   |
| -52   | 0.098 | -20.18 | -9.28  | 0.12    | -7    | 0.940 | -0.53  | 10.37  | 10.88   |
| -51   | 0.093 | -20.61 | -9.71  | 0.11    | -6    | 0.956 | -0.39  | 10.51  | 11.24   |
| -50   | 0.088 | -21.15 | -10.25 | 0.09    | -5    | 0.969 | -0.28  | 10.62  | 11.55   |
| -49   | 0.081 | -21.83 | -10.93 | 0.08    | -4    | 0.979 | -0.18  | 10.72  | 11.79   |
| -48   | 0.073 | -22.71 | -11.81 | 0.07    | -3    | 0.987 | -0.11  | 10.79  | 11.99   |
| -47   | 0.064 | -23.81 | -12.91 | 0.05    | -2    | 0.994 | -0.06  | 10.84  | 12.14   |
| -46   | 0.055 | -25.27 | -14.37 | 0.04    | -1    | 0.997 | -0.02  | 10.88  | 12.24   |
|       |       |        |        |         | 0     | 1.000 | 0.00   | 10.90  | 12.30   |