

KHIZ-DT established in the Appendix B DTV Table of Allotments.<sup>3</sup> It is a communications site near Victorville, CA, and is the site from which the station has operated throughout its history. It does now and will continue to provide service to the principal community of Barstow, CA. It is the site for which an application already has been filed for a license to cover the facilities authorized in the construction permit currently held by the station.

The two new transmitter locations involve sites currently used by other television broadcasters. The site at Mt Harvard serves the Los Angeles basin and is part of the complex, together with Mt Wilson, at which transmitters for almost all other television stations in the Los Angeles market are situated. It is a shared site operated by American Tower Corporation. Locating a gap filler transmitter there effectively collocates it with its adjacent channel neighbors, thereby reducing interference to the adjacent channel stations. The Snow Peak site is a communications facility and also currently is used by the transmitter for Station KVMD-DT. It is privately owned, and KHIZ-DT will be a tenant of both the site owner and of KVMD for different aspects of the Snow Peak facility. The Snow Peak transmitter will provide a second DTV service to an area that currently is served by only one DTV station and no analog stations, as well as providing additional service in surrounding underserved areas.

## ***Facilities***

The facilities requested in this application include continued operation at 1000 kW ERP at a height above average terrain of 597 meters at the Quartzite site, operation at almost 170 kW ERP at 879 meters HAAT at Mt Harvard, and operation at 40 kW ERP at 768 meters HAAT at Snow Peak. The currently authorized facility at the Quartzite site meets the requirements of §73.622(f)(5) as it does not exceed “that needed to provide the same geographic coverage area as the largest station within [its] market.” The relationships between the parameters in the cases of the added gap-filler transmitters result in power/height combinations that meet the requirements for maximum allowable facilities

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<sup>3</sup> Memorandum Opinion and Order on Reconsideration of the Seventh Report and Order and the Eighth Report and Order *In the Matter of Advanced Television Systems and Their Impact Upon the Existing Television Broadcast Service*, MB Docket No. 87-268 (FCC 08-72, released March 6, 2008).

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specified by the formula in §73.622(f)(8)(ii) of the Commission's Rules. The basic characteristics of each of the transmitters proposed in the KHIZ-DT DTS network are given in Figures 1a, 1b, and 1c at the end of this report and in the related DTS Engineering portions of the Form 301 application – one for each transmitter.

Three fundamental antenna designs are proposed for use in the KHIZ-DT DTS network. The Quartzite antenna is a cardioid, end-fed, slotted coaxial design with characteristics primarily intended to provide sufficient gain in both its azimuth and elevation patterns to meet the KHIZ-DT service objectives while permitting a more physically robust antenna to be installed than was originally put into operation by the station. As was noted in the Technical Statement that accompanied the application for the construction permit that this application seeks to modify, the original antenna twice failed physically. Consequently, it was necessary to add azimuth gain by reducing service in an area having little to no population in order to continue providing full service throughout the remainder of the KHIZ-DT service area. This situation and its solution were fully described in that earlier Technical Statement.

The antenna designs at Mt Harvard and Snow Peak will be similar, cavity-slot panel arrays, using panels that have azimuth patterns shaped through use of parasitic elements. Each will consist of a total of six panels in a single column. The Mt Harvard pattern will have a single main lobe, while the Snow Peak pattern will have a pair of main lobes in a “peanut” pattern. The azimuth patterns will be rather narrow in their main beams, with a smaller amount of radiation in other directions. A significant amount of electrical beam tilt will be used, with a sharp cut-off of the radiation above the main beam to control the extent of signal projection from each of the antennas, given their very high locations, to permit better control of interference to adjacent regions and within the DTS network. In addition, a small amount of mechanical beam tilt also will be applied to each antenna to position the contours as close to the authorized contour as possible while minimizing projections beyond the authorized contour.

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A plot of the PNLCs<sup>4</sup> of the various transmitters is provided in Figure 2. Since the main, Quartzite Mountain transmitter facility authorized by the outstanding construction permit (herein DTS Site 1) already covers the entire authorized service area of the station,<sup>5</sup> the provisions of §73.626(f)(1) are met by that facility alone. By virtue of the overlap of the contours of the three transmitters, they are contiguous, thereby meeting the requirements of §73.626(f)(3). Also shown in Figure 2 is the 48 dBu contour of the DTS Site 1 facility, which can be seen to encompass the principal community of Barstow, CA. There are no major obstructions in the path over the principal community; thus, the requirements of §73.625(a) and correspondingly of §73.626(f)(4) also are met by the DTS Site 1 transmitter alone. All three transmitters in the proposed DTS network are located within the KHIZ authorized service area, consequently meeting the requirements of §73.626(f)(6).

Although they were filed in the Technical Statement accompanying the original construction permit application that this application now seeks to modify, a description and plots of the pattern characteristics for the DTS Site 1 (Quartzite) antenna nevertheless are reproduced herein. The DTS Site 1 antenna is oriented to place the center of the cardioid azimuth pattern at 218 degrees true. Elevation power gain of the antenna is 23.50 (13.71 dBd) at the vertical beam maximum (1.0 degree below horizontal), 12.10 (10.83 dBd) in the horizontal plane, and 22.02 (13.43 dBd) at 0.677 degree below horizontal, the average depression angle to the radio horizon (computed at 1-degree azimuth intervals). The azimuth power gain is 1.60 (2.04 dB), yielding a total power gain in the main beam of 37.60 (15.75 dBd), in the horizontal plane of 19.36 (12.87 dBd), and toward the radio horizon of 35.23 (15.47 dBd).

A plot of the azimuthal radiation pattern of the DTS Site 1 antenna in relative field values is included as Figure 3. The azimuthal power pattern expressed in decibels relative to 1 kW (dBk), at the depression angle having maximum power (1 degree depression), is

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<sup>4</sup> To account for the dipole correction factor, the PNLCs are plotted at 41.5 dBu, with service statistics of F(50,90).

<sup>5</sup> Per §73.626(b), "For purposes of compliance with this section, a station's 'authorized service area' is defined as the area within its predicted noise-limited service contour determined using the facilities authorized for the station in a license or construction permit for non-DTS, single-transmitter-location operation."

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plotted in Figure 4. The tabulated azimuthal field and power values are given in Figure 5. The elevation radiation pattern in relative field values is included as Figure 6. The elevation power pattern expressed in decibels relative to 1 kW (dBk) is plotted in Figure 7. The tabulated elevation field and power values are given in Figure 8. Also uploaded to the CDBS Electronic Filing System (EFS) web site is a version of the elevation pattern in Office Open XML format, with the first column containing depression angle values and the second column containing relative field values of elevation pattern data. Only a single elevation pattern applies to the antenna, and there is no mechanical beam tilt, so only a single column of elevation data is supplied.

The antennas for DTS Site 2 (Mt Harvard) and DTS Site 3 (Snow Peak) are similar to one another in their basic designs, the major difference being the azimuth patterns created by the attached parasitic elements. They also have slightly different electrical beam tilt characteristics, with the DTS Site 2 antenna having its main beam at a depression angle of 3.8 degrees, while the DTS Site 3 antenna has its main beam at a depression angle of 3.5 degrees. Each antenna has somewhat different mechanical beam tilt applied in addition to the electrical beam tilt. Their characteristics and orientations are fully described in Figures 1b and 1c. Because mechanical beam tilt will be used and complete elevation data for the antennas for DTS Sites 2 and 3 is being supplied through files input to the CDBS Electronic Filing System, the azimuth pattern plots supplied in this Technical Statement and the azimuth pattern data supplied in the CDBS input document are for reference only and are at right angles to the axes of the antennas in their respective main beams (i.e., at 3.8 degrees depression for the Site 2 antenna and at 3.5 degrees depression for Site 3). Consequently, the azimuth patterns and data do not take account of the mechanical beam tilt, the effect of which is reflected wholly within the elevation data files.

The essential elevation pattern design of the antennas for DTS Sites 2 and 3 is somewhat unusual. It includes main beams at depression angles of 3.8 and 3.5 degrees, with a rapid fall-off of relative field values above the main beams to deep nulls at depression angles of 0.8 and 0.5 degrees, respectively. The nulls serve two purposes: They help to control the locations of the contours while permitting stronger field strengths to be delivered within

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the service areas, and they help in controlling interference to stations in neighboring markets. The latter consideration is significant in the discussion below on Border Issues. The elevation pattern design also includes a relatively broad peak and significant power levels to depression angles of approximately 17 degrees, thereby providing strong signals to the areas below the mountains on which the gap-filler transmitters are situated.

Elevation power gain of the antenna design for DTS Site 2 is 7.50 (8.75 dBd) at the beam maximum (3.8 degrees below horizontal), less than 0.0015 (–28 dBd) at the null above the main beam (0.8 degrees below horizontal), and 0.916 (–0.38 dBd) in the horizontal plane. The azimuth power gain is 5.70 (7.56 dB), yielding a total power gain in the main beam of 42.66 (16.30 dBd) and of 5.22 (7.18 dBd) in the horizontal plane. All plane and depression angle values are with respect to the antenna axis prior to the effects of any mechanical beam tilt. Because of the mechanical beam tilt applied to this antenna, effective radiated power toward the radio horizon is an inappropriate parameter for this antenna and therefore is not provided.

Equivalent characteristics for the DTS Site 3 antenna are elevation power gain of 7.55 (8.78 dBd) at the beam maximum (3.5 degrees below horizontal), less than 0.0015 (–28 dBd) at the null above the main beam (0.5 degrees below horizontal), and 0.095 (–10.2 dBd) in the horizontal plane. The azimuth power gain is 2.90 (4.62 dB), yielding a total power gain in the main beam of 21.93 (13.41 dBd) and of 0.277 (–5.58 dBd) in the horizontal plane. All plane and depression angle values are with respect to the antenna axis prior to the effects of any mechanical beam tilt. Again, because of the mechanical beam tilt applied to this antenna, effective radiated power toward the radio horizon is an inappropriate parameter for this antenna and therefore is not provided.

Plots of the DTS Sites 2 and 3 antenna azimuthal radiation patterns in relative field values are included as Figures 9a and 9b. The azimuthal power patterns expressed in decibels relative to 1 kW (dBk), at the depression angles having maximum power (3.8 and 3.5 degrees depression, respectively), are plotted in Figures 10a and 10b. The tabulated azimuthal field and power values are given in Figures 11a and 11b. The elevation radiation patterns in relative field values are included as Figures 12a and 12b.

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The elevation power patterns expressed in decibels relative to 1 kW (dBk), in the azimuthal directions having maximum power, are plotted in Figures 13a and 13b. The tabulated elevation field and power values are given in Figures 14a and 14b. All of these plots and tables are prior to application of mechanical beam tilt and therefore do not incorporate its effects, which are fully expressed in the data of the elevation patterns placed on file in the online application. The elevation pattern data for each antenna has been uploaded to the CDBS Electronic Filing System (EFS) web site in array form in Office Open XML format, with the first columns containing depression angle values and the first rows containing azimuth values for each column.

Although only a single elevation pattern applies to each of the antennas for DTS Sites 2 and 3, mechanical beam tilt will be applied to each of them. Since the software that the Commission will use to evaluate this application is not yet capable of applying mechanical beam tilt, the pattern rotation implicit in mechanical beam tilt has been pre-applied to the data provided through the EFS. Consequently, a large array of elevation data has been supplied for each antenna. Correspondingly, the Forms 301 DTS have been marked that no mechanical beam tilt and, similarly, that no azimuth rotation is applicable because they already have been built into the data arrays uploaded with the application forms. The actual azimuth rotations and mechanical beam tilt angles and headings for the antennas at DTS Sites 2 and 3 are provided in Figures 1b and 1c below.

All of the transmitters to be used in the KHIZ-DT DTS network will be Type Verified as per Section 73.1660 of the Commission's Rules. All transmitters will be of solid state designs. They will be synchronized using the methods specified in the ATSC Synchronization Standard for Distributed Transmission (A/110B), and they will emit the RF Watermark transmitter identification signal defined in the A/110B document.

### ***Largest In Market Calculation and Service Areas***

As noted above, §73.622(f)(5) provides that stations may exceed the limits on power and antenna height included in §73.622(f)(6) through (8) “up to that needed to provide the same geographic coverage area as the largest station within their market.” The DTS R&O applies the same exception to DTS operations. In ¶35 “Largest Station”

**Figure 1c — Technical Specifications — Proposed KHIZ-DTS Facility  
Channel 44 — Barstow, CA — Site 3: Snow Peak**

**Frequency**

Channel	44
Frequency Band	650 – 656 MHz
Center Frequency	653 MHz

**Location**

Site	Snow Peak, Banning, CA
Geographic Coordinates (NAD27)	34° 02' 16.96" N 116° 48' 46.93" W
Tower Registration (FAA Study Number)	1256620 (2006-AWP-6493-OE)

**Elevation**

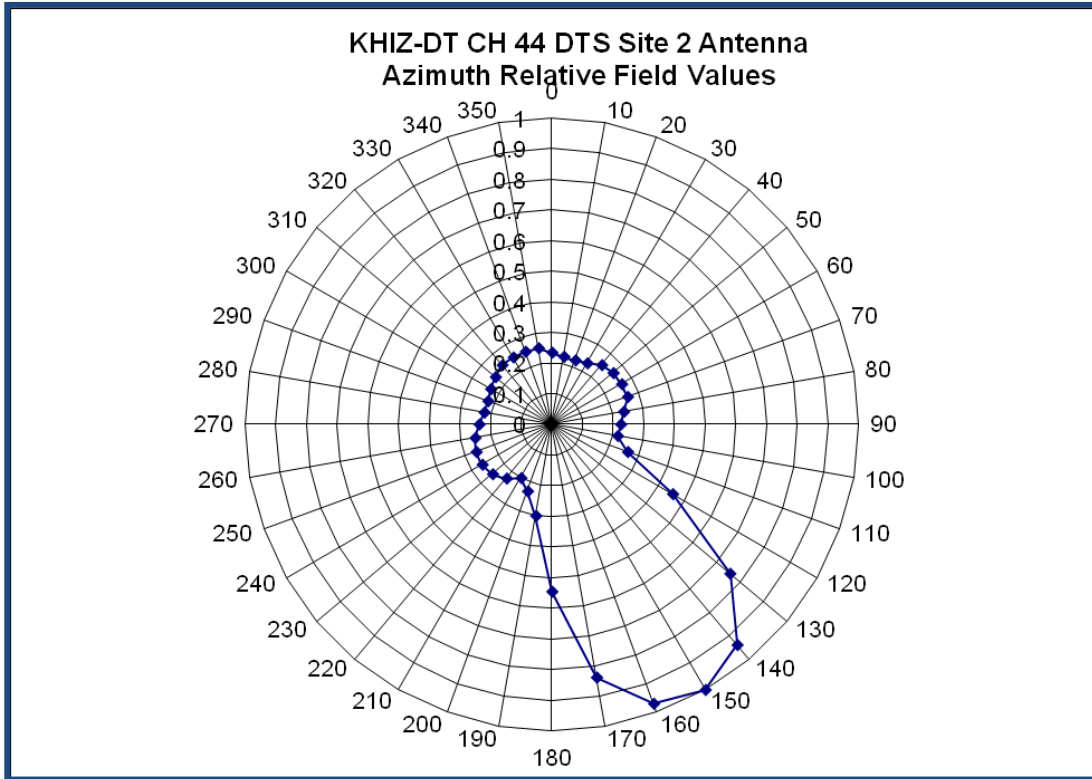
Elevation of site above mean sea level	2407.9 m
Overall height of tower above site elevation	52.1 m
Overall height of tower above mean sea level	2460.0 m
Height of antenna radiation center above site elevation	30.5 m
Elevation of average terrain (45-degree-spaced radials, 3.2-16.1 km)	1617.0 m
Height of antenna radiation center above mean sea level	2438.4 m
Height of antenna radiation center above average terrain (HAAT)	767.6 m

**Antenna**

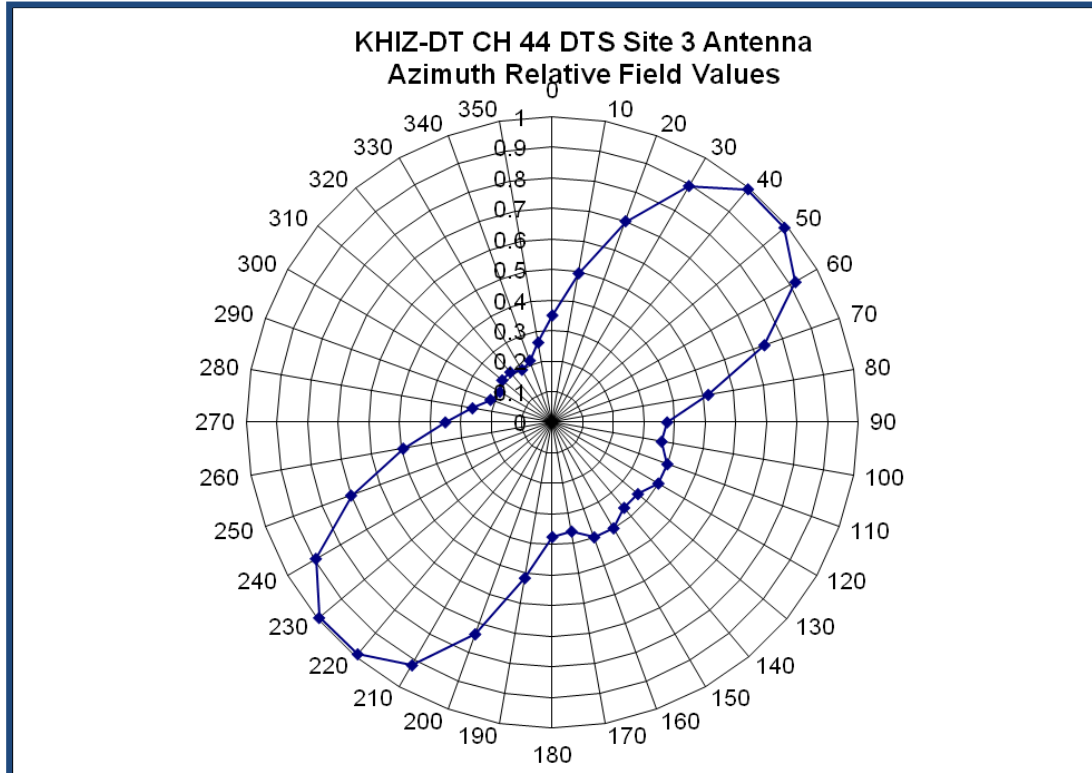
Manufacturer	Radio Frequency Systems
Model	DX24-H-44
Description	Side-Mounted UHF Cavity-Slot
Orientation (rotation around vertical axis)	135° true
Electrical beam tilt	3.5°
Mechanical beam tilt	1.2° down toward 207° true
Polarization	Horizontal
Gain (in horizontal plane – 0° depression)	0.277 (–5.58 dBd)
Gain (peak of beam – 3.5° depression)	21.93 (13.41 dBd)

**Power**

Effective radiated power (ERP) (main beam – 1.0° depression)	40.0 kW
Effective radiated power (ERP) (horizontal plane)	0.505 kW

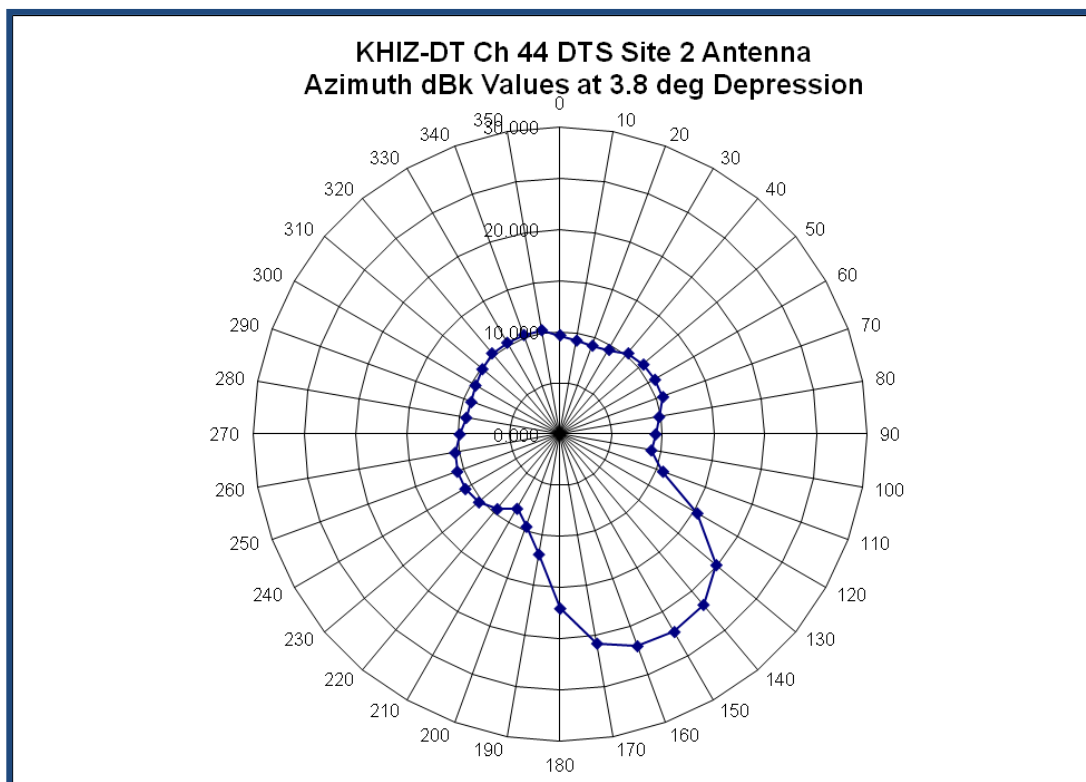


**Figure 9a — DTS Site 2 Antenna Azimuth Relative Field Values**

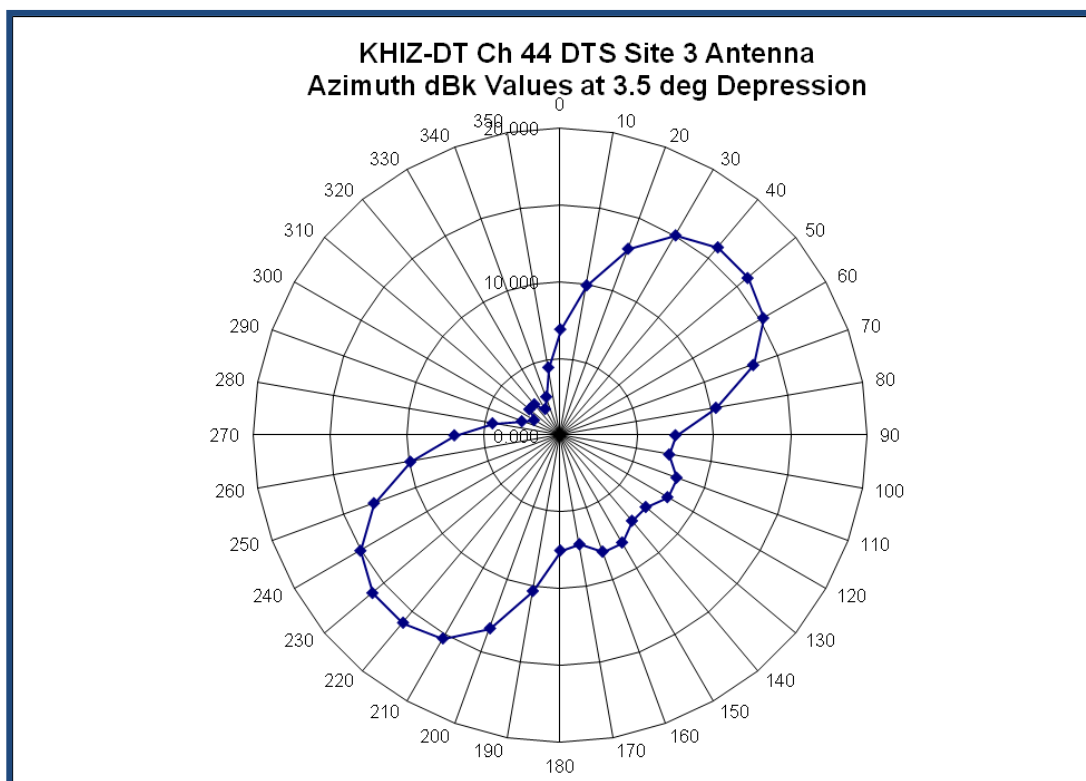


**Figure 9b — DTS Site 3 Antenna Azimuth Relative Field Values**





**Figure 10a — DTS Site 2 Antenna Azimuth dBk Values**



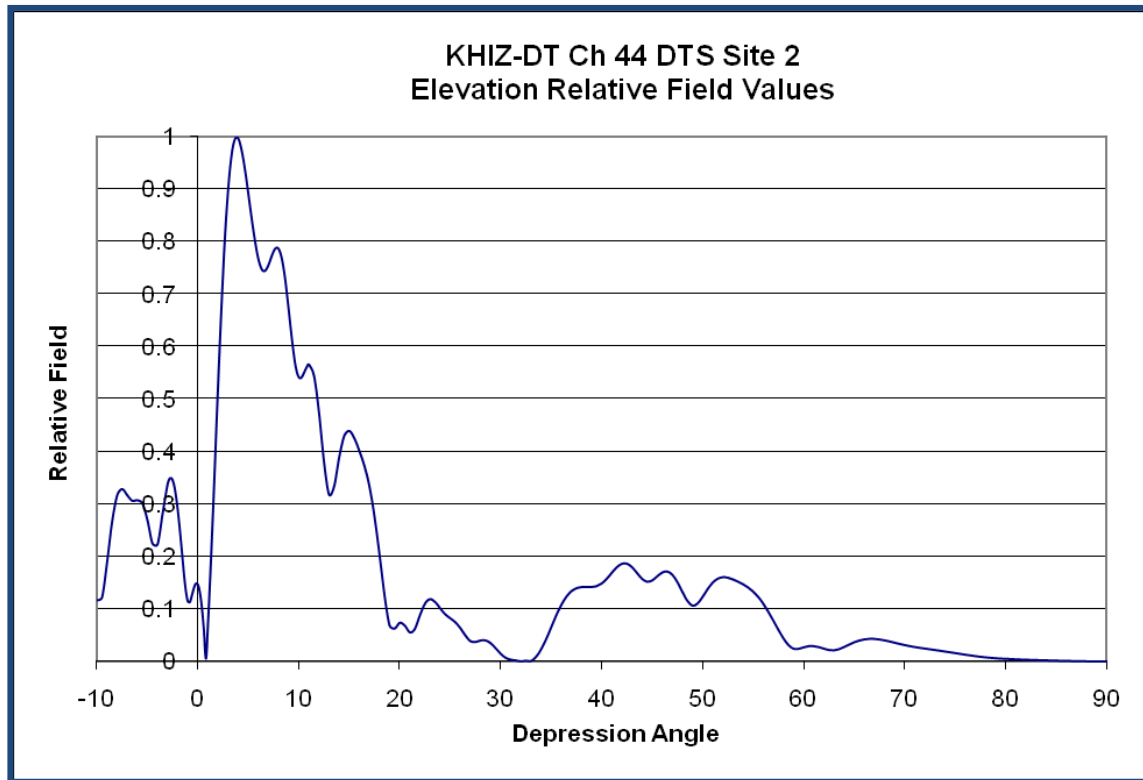
**Figure 10b — DTS Site 3 Antenna Azimuth dBk Values**

**Figure 11b— KHIZ-DT Site 3 Azimuthal Radiation Pattern Tabulated Values**

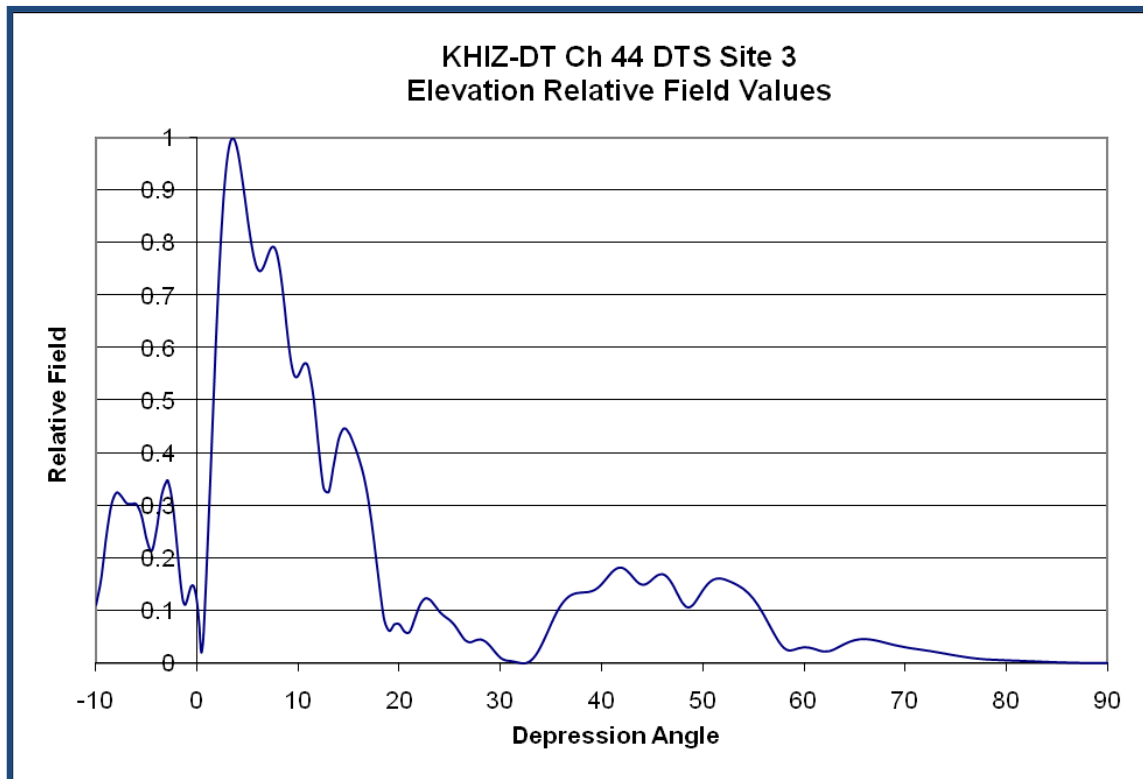
Azimuth	Relative Field	Effective Radiated Power (dBk)	Azimuth	Relative Field	Effective Radiated Power (dBk)
0	0.350	6.902	180	0.375	7.501
10	0.495	9.913	190	0.518	10.299
20	0.700	12.923	200	0.738	13.376
30	0.893	15.033	210	0.918	15.273
40	0.995	15.977	220	0.990	15.933
50	0.990	15.933	max 226	1.000	16.021
max 44	1.000	16.021	230	0.995	15.977
60	0.918	15.273	240	0.893	15.033
70	0.738	13.376	250	0.700	12.923
80	0.518	10.299	260	0.495	9.913
90	0.375	7.501	270	0.350	6.902
min 97	0.360	7.147	280	0.265	4.486
100	0.363	7.207	290	0.215	2.669
110	0.400	8.062	min 295	0.190	1.596
120	0.400	8.062	300	0.199	1.976
130	0.365	7.266	310	0.214	2.629
140	0.365	7.266	320	0.214	2.629
150	0.400	8.062	330	0.199	1.976
160	0.400	8.062	min 335	0.190	1.596
170	0.363	7.207	340	0.215	2.669
min 173	0.360	7.147	350	0.265	4.486

Notes: Derived from data supplied by manufacturer. Complete data set available upon request.

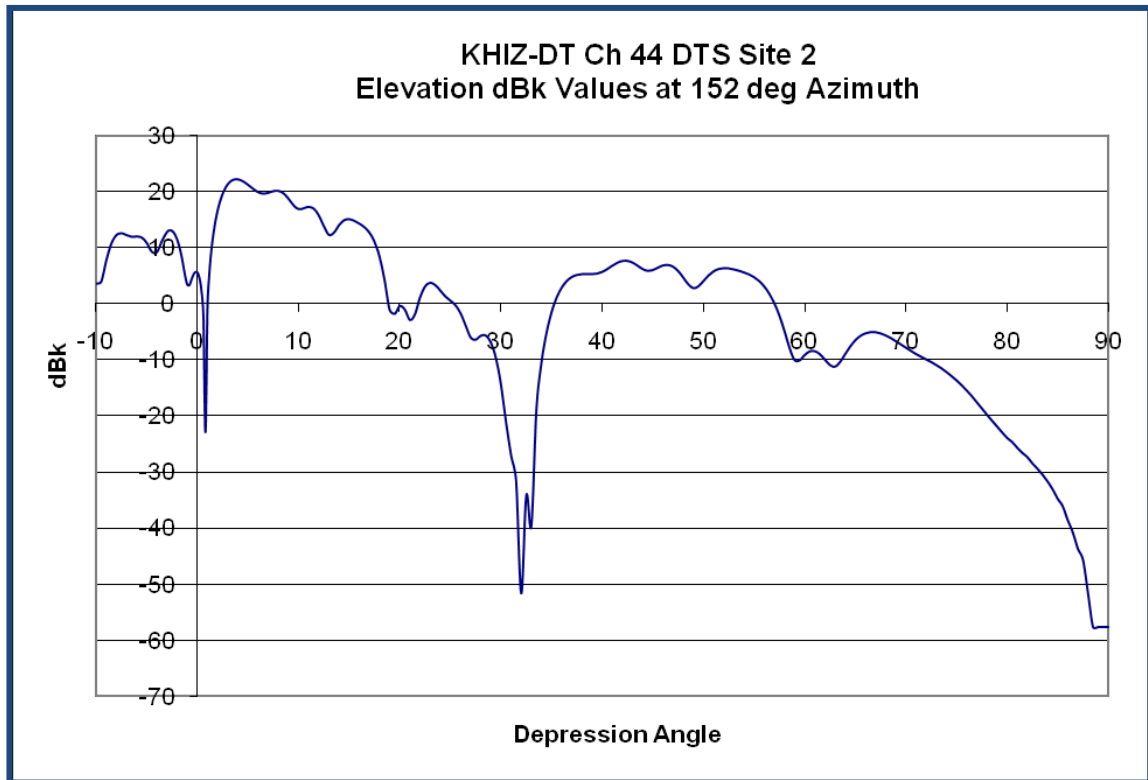
Does not show the effects of mechanical beam tilt, which are included only in the file uploaded within Form 301 on FCC Electronic Filing System



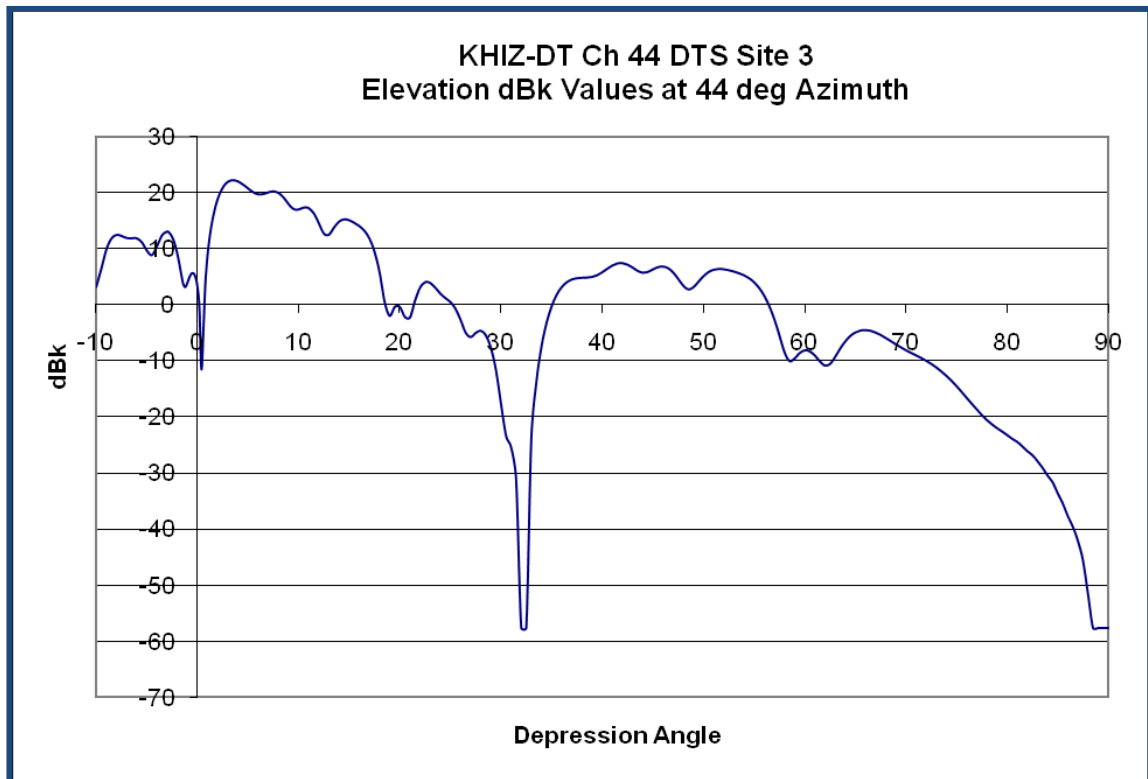
**Figure 12a — DTS Site 2 Antenna Elevation Relative Field Values**



**Figure 12b — DTS Site 3 Antenna Elevation Relative Field Values**



**Figure 13a — DTS Site 2 Antenna Elevation dBk Values**



**Figure 13b — DTS Site 3 Antenna Elevation dBk Values**

**Figure 14b — KHIZ-DT Site 3 Elevation Radiation Pattern Tabulated Values**

Depression Angle	Relative Field	Effective Radiated Power (dBk)	Depression Angle	Relative Field	Effective Radiated Power (dBk)
-5.0	0.236	3.475	9.0	0.614	11.785
-4.5	0.214	2.621	9.5	0.555	10.899
-4.0	0.257	4.213	10.0	0.548	10.799
-3.5	0.321	6.148	10.5	0.568	11.105
-3.0	0.348	6.842	11.0	0.563	11.026
-2.5	0.311	5.875	11.5	0.506	10.110
-2.0	0.224	3.026	12.0	0.413	8.344
-1.5	0.132	-1.635	12.5	0.333	6.475
-1.0	0.120	-2.396	13.0	0.326	6.282
-0.5	0.147	-0.639	13.5	0.377	7.557
0.0	0.113	-2.956	14.0	0.427	8.635
0.5	0.034	-14.159	14.5	0.447	9.025
1.0	0.210	2.477	15.0	0.439	8.862
1.5	0.446	8.964	15.5	0.416	8.409
2.0	0.675	12.612	16.0	0.389	7.822
2.5	0.855	14.653	16.5	0.353	6.986
3.0	0.966	15.717	17.0	0.301	5.592
3.5	1.000	16.021	17.5	0.230	3.259
4.0	0.975	15.803	18.0	0.150	-0.458
4.5	0.915	15.250	18.5	0.082	-5.693
5.0	0.845	14.556	19.0	0.061	-8.216
5.5	0.784	13.906	19.5	0.074	-6.618
6.0	0.750	13.518	20.0	0.074	-6.630
6.5	0.753	13.555	20.5	0.060	-8.402
7.0	0.778	13.838	21.0	0.059	-8.518
7.5	0.792	13.999	21.5	0.084	-5.535
8.0	0.770	13.752	22.0	0.110	-3.183
8.5	0.702	12.940	22.5	0.123	-2.203

Notes: Derived from data supplied by manufacturer. Complete data set available upon request.

Does not show the effects of mechanical beam tilt, which are included only in the file uploaded within Form 301 on FCC Electronic Filing System