

**S.O. 36099**  
**Report of Test**  
**6025-4-DA**  
**for**  
**Maine Public Broadcasting Corp.**  
**WMEA 90.1 MHz Portland, ME.**

**OBJECTIVE:**

The objective of this test was to demonstrate the directional characteristics of a 6025-4-DA to meet the needs of WMEA and to comply with the requirements of the FCC construction permit, file number BXPED-20180921AAF. This test characterizes only the radiation characteristics of the antenna when mounted on the tower as described. It does not represent or imply any guarantee of specific coverage which can be influenced by factors beyond the scope of this test.

**RESULTS:**

The following Figures are the results of the measurements from our pattern range:

- Figure 1A - Measured Azimuth Pattern with the FCC Composite
- Figure 1B - Measured Composite Azimuth Pattern with the FCC Composite
- Figure 1C - Tabulation of the Horizontal Polarization for the Measured Azimuth Pattern
- Figure 1D - Tabulation of the Vertical Polarization for the Measured Azimuth Pattern
- Figure 1E - Tabulation of the Measured Composite Azimuth Pattern
- Figure 1F - Tabulation of the FCC Composite

The calculated elevation pattern of the antenna is shown in Figure 3.

Construction permit file number BXPED-20180921AAF indicates that the Horizontal radiation component shall not exceed 100 kW at any azimuth and is restricted to the following values at the azimuths specified:

318 Degrees True: 0.42 kilowatts

MEMBER:



From Figure 1A, the maximum radiation of the Horizontal component occurs at 58 Degrees True. At the restricted azimuth of 318 Degrees True, the Horizontal component is 22.80 dB down from the maximum of 100 kW, or 0.05 kW.

The R.M.S. of the Horizontal component is 0.40. The total Horizontal power gain is 14.21. The R.M.S. of the Vertical component is 0.40. The total Vertical power gain is 9.79. See Figure 4 for calculations. The R.M.S. of the FCC composite pattern is 0.446. The R.M.S. of the measured composite pattern is 0.434. Eighty-five percent (85%) of the original authorized FCC composite pattern is 0.379. Therefore this pattern complies with the FCC requirement of 73.316(c)(2)(ix)(A).

**METHOD OF DIRECTIONALIZATION:**

One bay of the 6025-4-DA was mounted on a tower of precise scale to the Stainless G4 tower at the WMEA site. The spacing of the antenna to the tower was varied to achieve the vertical pattern shown in Figure 1A. See Figure 2 for mechanical details.

**METHOD OF MEASUREMENT:**

As allowed by the construction permit, file number BXPED-20180921AAF, a single level of the 6025-4-DA was set up on the Shively Labs scale model antenna pattern measuring range. A scale of 4.5:1 was used.

**EQUIPMENT:**

The 4.5:1 scale model pattern range consists of a wooden rotating pedestal equipped with a position indicator. The scale model bay is placed on the top of this pedestal and is used in the transmission mode at approximately 20 feet above ground level. The receiving corner reflector is spaced 50 feet away from the rotating pedestal at the same level above ground as the transmitting model. The transmitting and receiving signals are carried to a control building by means of RG-9/U double shielded coax cable.

Test Report 6025-4-DA

WMEA

Page Three

The control building is equipped with:

Hewlett Packard Model 4395-A Network Analyzer

PC Based Controller

Output Standard Printer or 'pdf'

All testing is carried out in strict accordance with approved procedures under our ISO9001.

**TEST PROCEDURES:**

The receiving antenna system is mounted so that the horizontal and vertical azimuth patterns are measured independently. The network analyzer was set to 405.45 MHz Calibrated pads are used to check the linearity of the measuring system. For example, 6 dB padding yields a scale reading of 50 from an unpadded reading of 100 in voltage. From the recorded patterns, the R.M.S. values are calculated and recorded as shown in Figure 1A.

Respectfully submitted by:



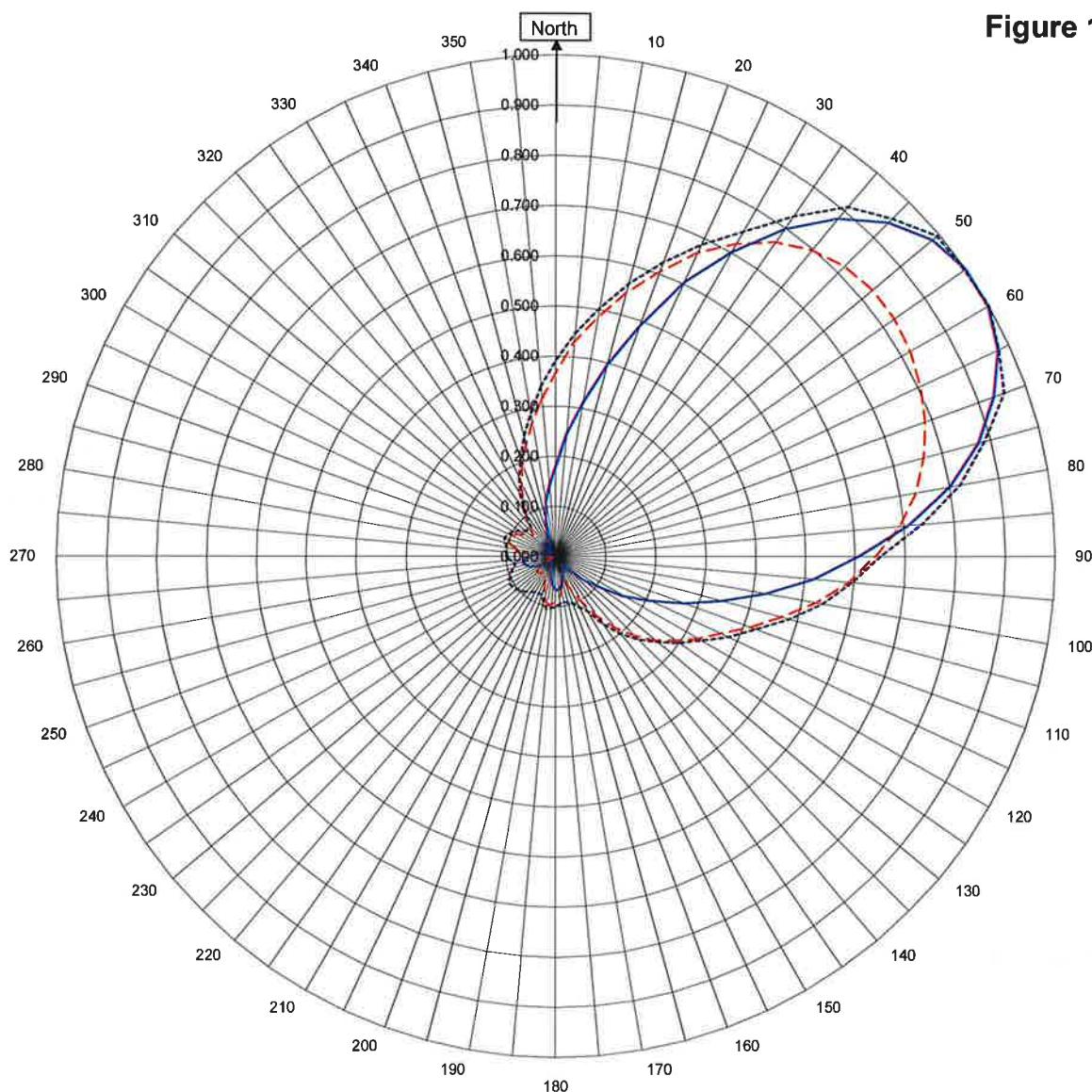
Angela Gillespie  
Vice President, Shively Labs

S/O 36099  
Date 3-1-19

# Shively Labs

Shively Labs, a division of Howell Laboratories, Inc. Bridgton, ME (207)647-3327

Figure 1A



## WMEA Portland, ME

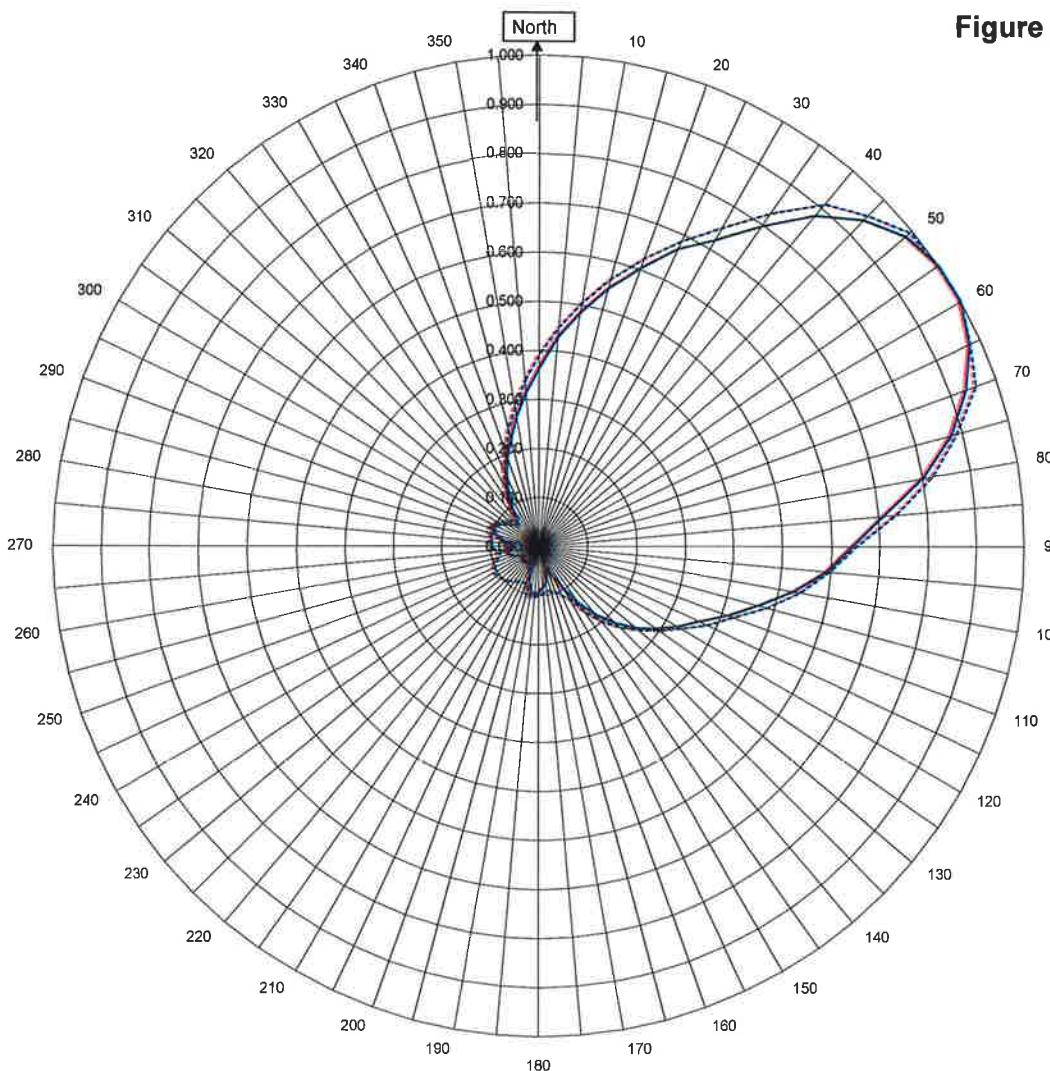
36099  
December 13, 2018

|                   |       |                                     |                   |
|-------------------|-------|-------------------------------------|-------------------|
| Horizontal RMS    | 0.402 | Frequency Plot Scale                | 90.1 / 405.45 mHz |
| Vertical RMS      | 0.397 |                                     |                   |
| H/V Composite RMS | 0.434 | Relative Field                      | 4.5 : 1           |
| FCC Composite RMS | 0.446 | See Figure 2 for Mechanical Details |                   |

|               |                     |
|---------------|---------------------|
| Antenna Model | 6025-4-DA           |
| Pattern Type  | Directional Azimuth |

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## WMEA Portland, ME

36099  
December 13, 2018

|                         |       |            |  |
|-------------------------|-------|------------|--|
| <u>H/VComposite RMS</u> | 0.434 | Frequency  | 90.1 / 405.45 mHz  |
| .....FCC Composite RMS  | 0.446 | Plot Scale | Relative Field<br>4.5 : 1<br>See Figure 2 for Mechanical Details |

|               |                           |
|---------------|---------------------------|
| Antenna Model | 6025-4-DA                 |
| Pattern Type  | Directional H/V Composite |

Figure 1C

Tabulation of Horizontal Azimuth Pattern  
WMEA Portland, ME

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0       | 0.181     | 180     | 0.067     |
| 10      | 0.310     | 190     | 0.047     |
| 20      | 0.489     | 200     | 0.023     |
| 30      | 0.700     | 210     | 0.017     |
| 40      | 0.879     | 220     | 0.012     |
| 45      | 0.941     | 225     | 0.013     |
| 50      | 0.982     | 230     | 0.019     |
| 60      | 0.999     | 240     | 0.037     |
| 70      | 0.933     | 250     | 0.057     |
| 80      | 0.800     | 260     | 0.067     |
| 90      | 0.607     | 270     | 0.056     |
| 100     | 0.426     | 280     | 0.029     |
| 110     | 0.273     | 290     | 0.016     |
| 120     | 0.157     | 300     | 0.014     |
| 130     | 0.073     | 310     | 0.015     |
| 135     | 0.042     | 315     | 0.028     |
| 140     | 0.021     | 320     | 0.035     |
| 150     | 0.031     | 330     | 0.022     |
| 160     | 0.043     | 340     | 0.048     |
| 170     | 0.061     | 350     | 0.111     |

Figure 1D

Tabulation of Vertical Azimuth Pattern  
WMEA Portland, ME

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0       | 0.365     | 180     | 0.092     |
| 10      | 0.484     | 190     | 0.094     |
| 20      | 0.604     | 200     | 0.060     |
| 30      | 0.720     | 210     | 0.037     |
| 40      | 0.798     | 220     | 0.043     |
| 45      | 0.819     | 225     | 0.045     |
| 50      | 0.829     | 230     | 0.046     |
| 60      | 0.821     | 240     | 0.023     |
| 70      | 0.788     | 250     | 0.006     |
| 80      | 0.733     | 260     | 0.007     |
| 90      | 0.642     | 270     | 0.032     |
| 100     | 0.529     | 280     | 0.076     |
| 110     | 0.413     | 290     | 0.100     |
| 120     | 0.327     | 300     | 0.089     |
| 130     | 0.259     | 310     | 0.068     |
| 135     | 0.221     | 315     | 0.061     |
| 140     | 0.182     | 320     | 0.072     |
| 150     | 0.100     | 330     | 0.129     |
| 160     | 0.047     | 340     | 0.193     |
| 170     | 0.075     | 350     | 0.270     |

Figure 1E

Tabulation of Composite Azimuth Pattern  
WMEA Portland, ME

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0       | 0.365     | 180     | 0.092     |
| 10      | 0.484     | 190     | 0.094     |
| 20      | 0.604     | 200     | 0.060     |
| 30      | 0.720     | 210     | 0.037     |
| 40      | 0.879     | 220     | 0.043     |
| 45      | 0.941     | 225     | 0.045     |
| 50      | 0.982     | 230     | 0.046     |
| 60      | 0.999     | 240     | 0.037     |
| 70      | 0.933     | 250     | 0.057     |
| 80      | 0.800     | 260     | 0.067     |
| 90      | 0.642     | 270     | 0.056     |
| 100     | 0.529     | 280     | 0.076     |
| 110     | 0.413     | 290     | 0.100     |
| 120     | 0.327     | 300     | 0.089     |
| 130     | 0.259     | 310     | 0.068     |
| 135     | 0.221     | 315     | 0.061     |
| 140     | 0.182     | 320     | 0.072     |
| 150     | 0.100     | 330     | 0.129     |
| 160     | 0.047     | 340     | 0.193     |
| 170     | 0.075     | 350     | 0.270     |

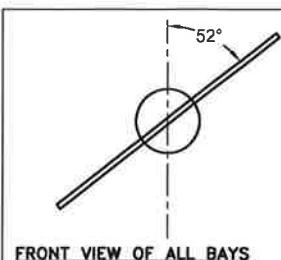
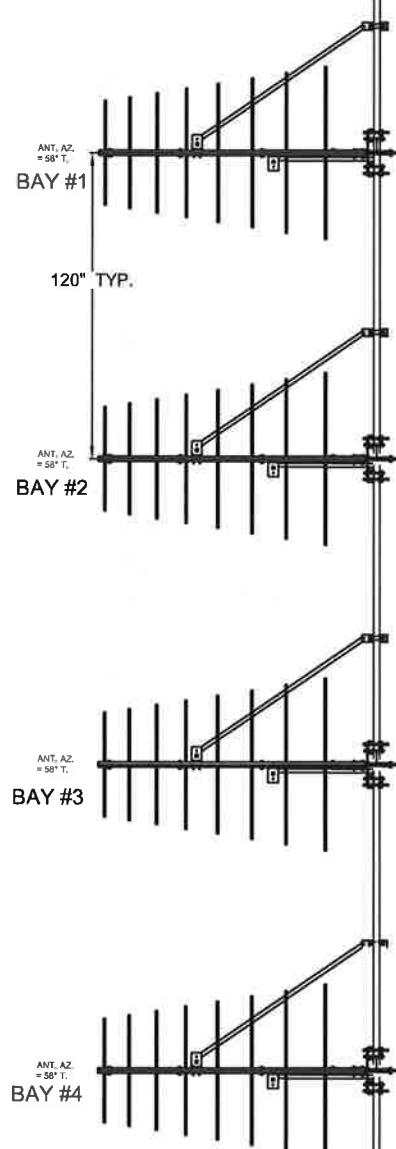
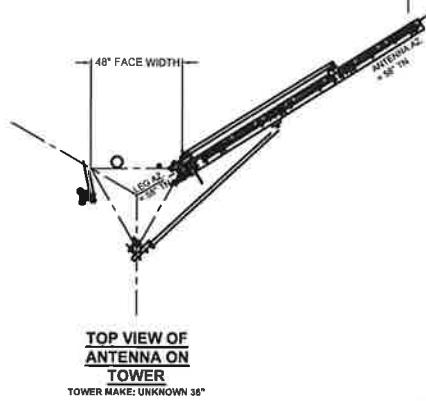
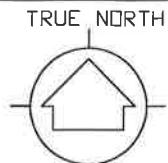
Figure 1F

Tabulation of FCC Directional Composite  
WMEA Portland, ME

| Azimuth | Rel Field | Azimuth | Rel Field |
|---------|-----------|---------|-----------|
| 0       | 0.392     | 180     | 0.100     |
| 10      | 0.504     | 190     | 0.107     |
| 20      | 0.624     | 200     | 0.080     |
| 30      | 0.748     | 210     | 0.082     |
| 40      | 0.910     | 220     | 0.092     |
| 50      | 0.995     | 230     | 0.102     |
| 60      | 1.000     | 240     | 0.108     |
| 70      | 0.955     | 250     | 0.096     |
| 80      | 0.820     | 260     | 0.082     |
| 90      | 0.650     | 270     | 0.100     |
| 100     | 0.543     | 280     | 0.100     |
| 110     | 0.424     | 290     | 0.110     |
| 120     | 0.335     | 300     | 0.100     |
| 130     | 0.265     | 310     | 0.078     |
| 140     | 0.200     | 320     | 0.078     |
| 150     | 0.124     | 330     | 0.142     |
| 160     | 0.098     | 340     | 0.206     |
| 170     | 0.091     | 350     | 0.290     |
| 115     | 1.000     |         |           |

**6025-3**

ANTENNA AZIMUTH = 58° TN  
52° SLANT BAY ROTATION



**SHIVELY LABS®**  
A DIVISION OF HOWELL LABORATORIES INC., BRIDGTON, MAINE

|             |            |        |           |
|-------------|------------|--------|-----------|
| SHOP ORDER: | FREQUENCY: | SCALE: | DRAWN BY: |
| 36099       | 90.1       | N.T.S. | ASP       |

TITLE:  
**FIGURE 2, WMEA, 90.1 MHz  
MODEL 6025-4/1, SLANT ELEMENTS**

DATE:  
1-10-19

**FIGURE 2**

| AZIMUTH | ATTENUATION | PHASE |
|---------|-------------|-------|
| 58°     | 0 db        | 0°    |
|         |             |       |
|         |             |       |

Antenna Mfg.: Shively Labs

Antenna Type: 6025

Station: WMEA

Frequency: 90.1

Channel #: 211

Figure: Figure 3

Date: 1/15/2019

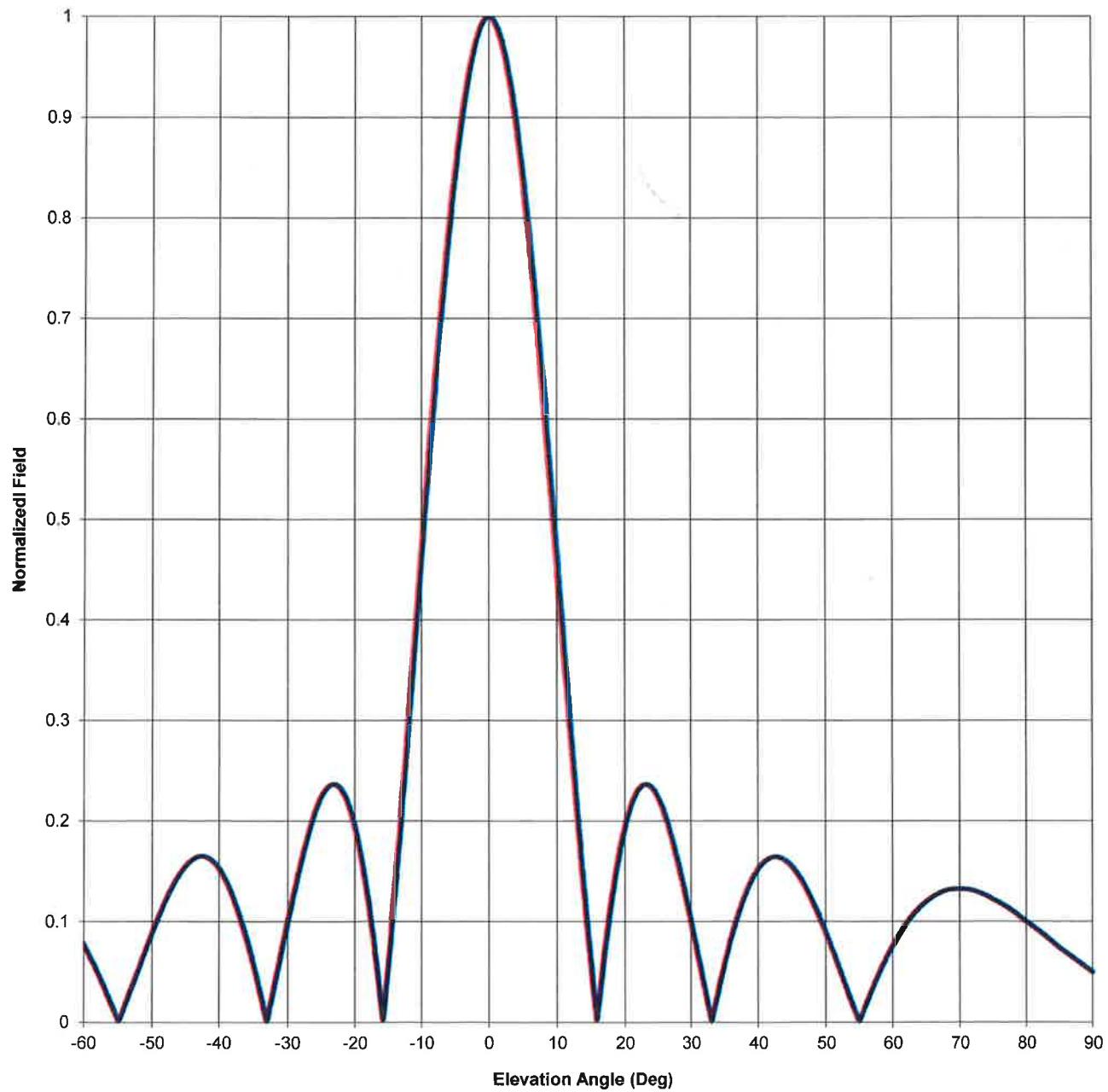
Beam Tilt 0

Gain (Max) 2.276

3.571 dB

Gain (Horizon) 2.276

3.571 dB



Antenna Mfg.: Shively Labs

Date: 1/15/2019

Antenna Type: 6025

Station: WMEA

Beam Tilt 0

Frequency: 90.1

Gain (Max) 2.276

3.571 dB

Channel #: 211

Gain (Horizon) 2.276

3.571 dB

Figure: Figure 3

| Angle of Depression (Deg) | Relative Field |
|---------------------------|----------------|---------------------------|----------------|---------------------------|----------------|---------------------------|----------------|
| -90                       | 0.050          | -44                       | 0.161          | 0                         | 1.000          | 46                        | 0.145          |
| -89                       | 0.055          | -43                       | 0.165          | 1                         | 0.992          | 47                        | 0.134          |
| -88                       | 0.060          | -42                       | 0.164          | 2                         | 0.973          | 48                        | 0.120          |
| -87                       | 0.064          | -41                       | 0.160          | 3                         | 0.941          | 49                        | 0.105          |
| -86                       | 0.069          | -40                       | 0.153          | 4                         | 0.897          | 50                        | 0.088          |
| -85                       | 0.074          | -39                       | 0.141          | 5                         | 0.844          | 51                        | 0.071          |
| -84                       | 0.079          | -38                       | 0.125          | 6                         | 0.779          | 52                        | 0.053          |
| -83                       | 0.085          | -37                       | 0.106          | 7                         | 0.708          | 53                        | 0.035          |
| -82                       | 0.090          | -36                       | 0.083          | 8                         | 0.630          | 54                        | 0.017          |
| -81                       | 0.095          | -35                       | 0.057          | 9                         | 0.548          | 55                        | 0.001          |
| -80                       | 0.100          | -34                       | 0.028          | 10                        | 0.463          | 56                        | 0.018          |
| -79                       | 0.105          | -33                       | 0.003          | 11                        | 0.376          | 57                        | 0.034          |
| -78                       | 0.110          | -32                       | 0.035          | 12                        | 0.291          | 58                        | 0.049          |
| -77                       | 0.115          | -31                       | 0.068          | 13                        | 0.208          | 59                        | 0.063          |
| -76                       | 0.119          | -30                       | 0.101          | 14                        | 0.129          | 60                        | 0.076          |
| -75                       | 0.122          | -29                       | 0.132          | 15                        | 0.056          | 61                        | 0.088          |
| -74                       | 0.126          | -28                       | 0.161          | 16                        | 0.010          | 62                        | 0.098          |
| -73                       | 0.129          | -27                       | 0.187          | 17                        | 0.069          | 63                        | 0.107          |
| -72                       | 0.131          | -26                       | 0.208          | 18                        | 0.119          | 64                        | 0.114          |
| -71                       | 0.132          | -25                       | 0.224          | 19                        | 0.161          | 65                        | 0.120          |
| -70                       | 0.132          | -24                       | 0.234          | 20                        | 0.194          | 66                        | 0.125          |
| -69                       | 0.132          | -23                       | 0.236          | 21                        | 0.216          | 67                        | 0.129          |
| -68                       | 0.131          | -22                       | 0.231          | 22                        | 0.231          | 68                        | 0.131          |
| -67                       | 0.129          | -21                       | 0.217          | 23                        | 0.236          | 69                        | 0.132          |
| -66                       | 0.125          | -20                       | 0.194          | 24                        | 0.234          | 70                        | 0.132          |
| -65                       | 0.120          | -19                       | 0.161          | 25                        | 0.224          | 71                        | 0.132          |
| -64                       | 0.114          | -18                       | 0.120          | 26                        | 0.208          | 72                        | 0.131          |
| -63                       | 0.107          | -17                       | 0.069          | 27                        | 0.186          | 73                        | 0.129          |
| -62                       | 0.098          | -16                       | 0.010          | 28                        | 0.161          | 74                        | 0.126          |
| -61                       | 0.088          | -15                       | 0.056          | 29                        | 0.132          | 75                        | 0.122          |
| -60                       | 0.076          | -14                       | 0.129          | 30                        | 0.100          | 76                        | 0.119          |
| -59                       | 0.063          | -13                       | 0.208          | 31                        | 0.068          | 77                        | 0.115          |
| -58                       | 0.049          | -12                       | 0.291          | 32                        | 0.035          | 78                        | 0.110          |
| -57                       | 0.034          | -11                       | 0.376          | 33                        | 0.003          | 79                        | 0.105          |
| -56                       | 0.018          | -10                       | 0.463          | 34                        | 0.028          | 80                        | 0.100          |
| -55                       | 0.001          | -9                        | 0.548          | 35                        | 0.057          | 81                        | 0.095          |
| -54                       | 0.017          | -8                        | 0.630          | 36                        | 0.083          | 82                        | 0.090          |
| -53                       | 0.035          | -7                        | 0.708          | 37                        | 0.106          | 83                        | 0.085          |
| -52                       | 0.053          | -6                        | 0.780          | 38                        | 0.125          | 84                        | 0.079          |
| -51                       | 0.071          | -5                        | 0.844          | 39                        | 0.140          | 85                        | 0.074          |
| -50                       | 0.089          | -4                        | 0.897          | 40                        | 0.152          | 86                        | 0.069          |
| -49                       | 0.105          | -3                        | 0.941          | 41                        | 0.160          | 87                        | 0.064          |
| -48                       | 0.121          | -2                        | 0.973          | 42                        | 0.164          | 88                        | 0.060          |
| -47                       | 0.134          | -1                        | 0.992          | 43                        | 0.164          | 89                        | 0.055          |
| -46                       | 0.146          | 0                         | 1.000          | 44                        | 0.161          | 90                        | 0.050          |
| -45                       | 0.155          |                           |                | 45                        | 0.155          |                           |                |

S.O. 36099

Figure 4

VALIDATION OF TOTAL POWER GAIN CALCULATION

WMEA Portland, ME

MODEL 6025-4-DA

Elevation Gain of Antenna 2.276

Horizontal RMS value divided by the Vertical RMS value equals the Horiz. - Vert. Ratio

H RMS 0.401793 V RMS 0.397422 H/V Ratio 1.011

Elevation Gain of Horizontal Component 2.301

Elevation Gain of Vertical Component 2.251

Horizontal Azimuth Gain equals  $1/(RMS)^2$ . 6.194

Vertical Azimuth Gain equals  $1/(RMS/\text{Max Vert})^2$ . 4.362

Max. Vertical 0.83

\*Total Horizontal Power Gain is the Elevation Gain Times the Azimuth Gain

Total Horizontal Power Gain = 14.253

\*Total Vertical Power Gain is the Elevation Gain Times the Azimuth Gain

Total Vertical Power Gain = 9.819

=====

ERP divided by Horizontal Power Gain equals Antenna Input Power

100 kW ERP Divided by H Gain 14.253 equals 7.016 kW H Antenna Input Power

Antenna Input Power times Vertical Power Gain equals Vertical ERP

7.016 kW Times V Gain 9.819 equals 68.890 kW V ERP

Maximum Value of the Vertical Component squared times the Maximum ERP equals the Vertical ERP

(0.83)<sup>2</sup> Times 100.00 Equals 68.890 kW Vertical ERP

NOTE: Calculating the ERP of the Vertical Component by two methods validates the total power gain calculations