



**MARASHLIAN
& DONAHUE, LLC**
THE COMMLAW GROUP

April 6, 2015

Marlene H. Dortch, Secretary
Federal Communications Commission
445 12th Street, SW
Room TW-A325
Washington, DC 20554

Accepted / Filed

APR - 6 2015

Federal Communications Commission
Office of the Secretary

ATTN: Media Bureau

Re: WRSO(AM), Orlovista, Florida, Facility ID No. 129548
FCC File No. BMML-20150304ADE
Amendment to Application for License to Cover on FCC 302-AM

Dear Ms. Dortch:

On behalf of Star Over Orlando, Inc., by and through its attorney, attached is an amendment, in triplicate, to the above referenced application. The application is amended, as requested,¹ to correct the community of license in Section II, provide Figure 16 (Certified Array Geometry Survey) which was omitted in the original filing, and correct the antenna monitor ratio for tower #3.

If there are any questions concerning this application, please do not hesitate to contact me.

Yours truly,

Nathaniel J. Hardy
Counsel for Star Over Orlando, Inc.

Encls.

cc: Son Nguyen, Audio Division (via email)
Edward Lubetzky, Audio Division (via email)

¹ See Letter, dated March 13, 2015, from Son Nguyen, Supervisory Engineer, Audio Division to counsel. The Letter granted limited program test authority to Star Over Orlando, Inc. See BPTA-20150304ADF. As the application has been amended, Star Over Orlando, Inc. requests that it be granted unlimited program test authority for Station WRSO.

Federal Communications Commission
Washington, D. C. 20554

Approved by OMB
3060-0627
Expires 01/31/98

FOR
FCC
USE
ONLY

APR - 6 2015

Federal Communications Commission
Office of the Secretary

**FCC 302-AM
APPLICATION FOR AM
BROADCAST STATION LICENSE**

(Please read instructions before filling out form.)

FOR COMMISSION USE ONLY

FILE NO.

SECTION I - APPLICANT FEE INFORMATION			
1. PAYOR NAME (Last, First, Middle Initial) <p style="text-align:center">STAR OVER ORLANDO, INC.</p>			
MAILING ADDRESS (Line 1) (Maximum 35 characters) 357 OCEAN SHORE BOULEVARD			
MAILING ADDRESS (Line 2) (Maximum 35 characters)			
CITY ORMOND BEACH	STATE OR COUNTRY (if foreign address) FL	ZIP CODE 32176	
TELEPHONE NUMBER (include area code) 386 5722723 (386) 566-4299	CALL LETTERS WRSO	OTHER FCC IDENTIFIER (If applicable) 129548	
2. A. Is a fee submitted with this application? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No			
B. If No, indicate reason for fee exemption (see 47 C.F.R. Section			
<input type="checkbox"/> Governmental Entity <input type="checkbox"/> Noncommercial educational licensee <input checked="" type="checkbox"/> Other (Please explain):			
This is a minor curative amendment to FCC File No. BMML-20150304ADE.*			
C. If Yes, provide the following information:			
Enter in Column (A) the correct Fee Type Code for the service you are applying for. Fee Type Codes may be found in the "Mass Media Services Fee Filing Guide." Column (B) lists the Fee Multiple applicable for this application. Enter fee amount due in Column (C).			
(A)	(B)	(C)	
FEE TYPE CODE	FEE MULTIPLE	FEE DUE FOR FEE TYPE CODE IN COLUMN (A)	FOR FCC USE ONLY
	0 0 0 1	\$	
To be used only when you are requesting concurrent actions which result in a requirement to list more than one Fee Type Code.			
(A)	(B)	(C)	
	0 0 0 1	\$	FOR FCC USE ONLY
ADD ALL AMOUNTS SHOWN IN COLUMN C, AND ENTER THE TOTAL HERE. THIS AMOUNT SHOULD EQUAL YOUR ENCLOSED REMITTANCE.		TOTAL AMOUNT REMITTED WITH THIS APPLICATION	FOR FCC USE ONLY
		\$	

* The application is amended to correct the community of license of the station in Section II, provide Figure 16 which was omitted and correct the antenna monitor ratio for tower #3.

SECTION II - APPLICANT INFORMATION		
1. NAME OF APPLICANT STAR OVER ORLANDO, INC.		
MAILING ADDRESS 357 OCEAN SHORE BOULEVARD		
CITY ORMOND BEACH	STATE FL	ZIP CODE 32176

2. This application is for:

- Commercial Noncommercial
 AM Directional AM Non-Directional

Call letters WRSO	Community of License ORLOVISTA	Construction Permit File No. BMP-20140211ACD	Modification of Construction Permit File No(s).	Expiration Date of Last Construction Permit 9/11/2016
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3. Is the station now operating pursuant to automatic program test authority in accordance with 47 C.F.R. Section 73.1620?

Yes No

If No, explain in an Exhibit.

Exhibit No.
A

4. Have all the terms, conditions, and obligations set forth in the above described construction permit been fully met?

Yes No

If No, state exceptions in an Exhibit.

Exhibit No.

5. Apart from the changes already reported, has any cause or circumstance arisen since the grant of the underlying construction permit which would result in any statement or representation contained in the construction permit application to be now incorrect?

Yes No

If Yes, explain in an Exhibit.

Exhibit No.

6. Has the permittee filed its Ownership Report (FCC Form 323) or ownership certification in accordance with 47 C.F.R. Section 73.3615(b)?

Yes No

If No, explain in an Exhibit.

Does not apply

Exhibit No.

7. Has an adverse finding been made or an adverse final action been taken by any court or administrative body with respect to the applicant or parties to the application in a civil or criminal proceeding, brought under the provisions of any law relating to the following: any felony; mass media related antitrust or unfair competition; fraudulent statements to another governmental unit; or discrimination?

Yes No

If the answer is Yes, attach as an Exhibit a full disclosure of the persons and matters involved, including an identification of the court or administrative body and the proceeding (by dates and file numbers), and the disposition of the litigation. Where the requisite information has been earlier disclosed in connection with another application or as required by 47 U.S.C. Section 1.65(c), the applicant need only provide: (i) an identification of that previous submission by reference to the file number in the case of an application, the call letters of the station regarding which the application or Section 1.65 information was filed, and the date of filing; and (ii) the disposition of the previously reported matter.

Exhibit No.

8. Does the applicant, or any party to the application, have a petition on file to migrate to the expanded band (1605-1705 kHz) or a permit or license either in the existing band or expanded band that is held in combination (pursuant to the 5 year holding period allowed) with the AM facility proposed to be modified herein?

Yes No

If Yes, provide particulars as an Exhibit.

Exhibit No.

The APPLICANT hereby waives any claim to the use of any particular frequency or of the electromagnetic spectrum as against the regulatory power of the United States because use of the same, whether by license or otherwise, and requests and authorization in accordance with this application. (See Section 304 of the Communications Act of 1934, as amended).

The APPLICANT acknowledges that all the statements made in this application and attached exhibits are considered material representations and that all the exhibits are a material part hereof and are incorporated herein as set out in full in

CERTIFICATION

1. By checking Yes, the applicant certifies, that, in the case of an individual applicant, he or she is not subject to a denial of federal benefits that includes FCC benefits pursuant to Section 5301 of the Anti-Drug Abuse Act of 1988, 21 U.S.C. Section 862, or, in the case of a non-individual applicant (e.g., corporation, partnership or other unincorporated association), no party to the application is subject to a denial of federal benefits that includes FCC benefits pursuant to that section. For the definition of a "party" for these purposes, see 47 C.F.R. Section 1.2002(b).

Yes No

2. I certify that the statements in this application are true, complete, and correct to the best of my knowledge and belief, and are made in good faith.

Name Carl Tutera	Signature 
Title President	Date 04/01/2015
	Telephone Number (386) 672-2723

(386) 566-4299

WILLFUL FALSE STATEMENTS ON THIS FORM ARE PUNISHABLE BY FINE AND/OR IMPRISONMENT (U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION

FCC NOTICE TO INDIVIDUALS REQUIRED BY THE PRIVACY ACT AND THE PAPERWORK REDUCTION ACT

The solicitation of personal information requested in this application is authorized by the Communications Act of 1934, as amended. The Commission will use the information provided in this form to determine whether grant of the application is in the public interest. In reaching that determination, or for law enforcement purposes, it may become necessary to refer personal information contained in this form to another government agency. In addition, all information provided in this form will be available for public inspection. If information requested on the form is not provided, the application may be returned without action having been taken upon it or its processing may be delayed while a request is made to provide the missing information. Your response is required to obtain the requested authorization.

Public reporting burden for this collection of information is estimated to average 639 hours and 53 minutes per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, can be sent to the Federal Communications Commission, Records Management Branch, Paperwork Reduction Project (3060-0627), Washington, D. C. 20554. Do NOT send completed forms to this address.

THE FOREGOING NOTICE IS REQUIRED BY THE PRIVACY ACT OF 1974, P.L. 93-579, DECEMBER 31, 1974, 5 U.S.C. 552a(e)(3), AND THE PAPERWORK REDUCTION ACT OF 1980, P.L. 96-511, DECEMBER 11, 1980, 44 U.S.C. 3507.

SECTION III - Page 2

9. Description of antenna system ((f directional antenna is used, the information requested below should be given for each element of the array. Use separate sheets if necessary.)

Type Radiator	Overall height in meters of radiator above base insulator, or above base, if grounded.	Overall height in meters above ground (without obstruction lighting)	Overall height in meters above ground (include obstruction lighting)	If antenna is either top loaded or sectionalized, describe fully in an Exhibit.
Guyed Tower	92.53	93.0	94.2	Exhibit No. N/A

Excitation Series Shunt

Geographic coordinates to nearest second. For directional antenna give coordinates of center of array. For single vertical radiator give tower location.

North Latitude 28 ° 34 ' 18 "	West Longitude 81 ° 26 ' 02 "
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If not fully described above, attach as an Exhibit further details and dimensions including any other antenna mounted on tower and associated isolation circuits.

Exhibit No.
ENG

Also, if necessary for a complete description, attach as an Exhibit a sketch of the details and dimensions of ground system.

Exhibit No.
ENG

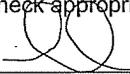
10. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit?

No Change from Construction Permit

11. Give reasons for the change in antenna or common point resistance.

New Adjustment

I certify that I represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and that it is true to the best of my knowledge and belief.

Name (Please Print or Type) Kurt Gorman	Signature (check appropriate box below) 
Address (include ZIP Code) Phasetek Inc. 550 California Rd., Unit 11 Quakertown, PA 18951	Date March 30, 2015 Telephone No. (Include Area Code) 215-536-6648

- Technical Director
- Registered Professional Engineer
- Chief Operator
- Technical Consultant
- Other (specify)

EXHIBIT A
APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO(AM), 810 KHZ, DA-2, ORLOVISTA, FLORIDA

Pursuant to the terms of the underlying construction permit, the station must request program test authority prior to beginning such tests. See Special Operating Conditions, No. 1, FCC File No. BMP-20140211ACD.

ENGINEERING STATEMENT CONCERNING

APPLICATION FOR LICENSE INFORMATION

EMPLOYING MOMENT METHOD MODELING

WRSO, 810 KHZ, DA-2

ORLOVISTA, FLORIDA

FEBRUARY, 2015

PHASETEK INC.
**ENGINEERING STATEMENT CONCERNING
APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015**

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302-AM

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PHASETEK INC.

**ENGINEERING STATEMENT CONCERNING
APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015**

SUMMARY

Adjustment of the Antenna System and a Proof of Performance employing Moment Method Modeling were performed on Radio Station WRSO, 810 KHz, Orlovista, Florida, after modification of Antenna Phasing equipment. The existing transmission and sampling lines were utilized. WRSO holds Construction Permit Number: BMP-20140211ACD to increase Day power and change Day radiation pattern. The Night radiation pattern remains as licensed. This report was prepared on behalf of Star Over Orlando, Inc. licensee of Radio Station WRSO.

SITE MODIFICATIONS

The WRSO Transmitter site is that as currently licensed. The Day Antenna Phasing and Branching equipment has been modified. All Towers remain unchanged. A License Application employing Moment Method Modeling as set forth in Section 73.151(C) has been done to cover the Radio Station WRSO Construction Permit and license under the new rules.

REFERENCE POINTS

Reference Points were measured at pattern minima and maxima for the Directional modes of operation. These Points and their measured field intensity are shown in Figure 15.

SPECIAL OPERATING CONDITION #6

No new tower construction has been done at the WRSO transmitter site. All towers and grounding remain as previously licensed. Therefore, implementation of the WRSO construction permit has not adversely affected AM stations WDYZ, 990 kHz or WRLZ, 1270 kHz. WHOO, 1080 kHz operates from a licensed site that is more than 5 km from the WRSO site. Verification of no spurious products from the above stations was performed.

PHASETEK INC.

ENGINEERING STATEMENT CONCERNING APPLICATION FOR LICENSE INFORMATION EMPLOYING MOMENT METHOD MODELING WRSO, 810 KHZ, DA-2 ORLOVISTA, FLORIDA FEBRUARY, 2015

METHOD OF MOMENTS DETAIL

All Moment Method Modeling was done with Expert MININEC Broadcast Professional, Version 23. One wire was used to represent each Tower. Towers were driven individually to verify the Model compared to measured impedance data. Once the Model was verified, both the Day and Night Directional Antenna Systems were computed. For Directional modes, the complex voltage values for sources located at ground level were computed. These sources produce current moment sums for each Tower that, when normalized, equate to the Theoretical Field Parameters for each respective Tower.

MEASURING EQUIPMENT AND PERSONNEL

All Tower Resistance and Reactance measurements were made with a Delta Electronics OIB-3 Operating Impedance Bridge. Before use, tests of known impedances were made to verify operation. All Field Intensity Measurements were made with two Potomac Instruments Field Intensity Meters: An FIM-41, Serial Number 2181, calibrated on October 9, 2009 and another FIM-41, Serial Number 643, calibrated July 3, 2003. Both meters were calibrated by Potomac Instruments, Silver Spring, Maryland. Both meters were also compared to a Potomac Instruments FIM-21, serial number 901, calibrated August 29, 2012 by Potomac Instruments and agreed within tolerance. All measurements were taken by Phasetek Inc. personnel supervised by Kurt Gorman of Phasetek Inc.

CONCLUSION

It is believed that the WRSO Antenna System has been constructed and adjusted in accordance with all applicable Commission rules and regulations. The foregoing was prepared on behalf of Star Over Orlando, Inc., under the immediate supervision of Kurt Gorman, Phasetek Inc., Quakertown, Pennsylvania, whose qualifications are a matter of record with the Federal Communications Commission. The statements herein are true and correct of his knowledge, except such statements made on information and belief, and as to these statements he believes them to be true and correct.

PHASETEK INC.

**ENGINEERING STATEMENT CONCERNING
APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015**



**Kurt Gorman, President
Phasetek Inc.
Quakertown, Pennsylvania**

FIGURE 1

ANTENNA SYSTEM AS ADJUSTED

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

ANTENNA SYSTEM DESCRIPTION

1. The Antenna System consists of four (4), uniform, guyed, vertical steel transmitting Towers. All Towers stand 92.53M (90.0°) above their Base Insulators. The Towers are arranged with Tower 1 as a reference; Tower 2 is spaced 90.0° on a bearing of 81.6°T. Tower 3 is spaced 225.0° on a bearing of 7.0°T. Tower 4 is spaced 208.1° on a bearing of 343.4°T. Tower 2 supports an FM translator antenna and a STL antenna. Both feeds for these Antennas are isolated at the base with Isocouplers. All towers have aviation obstruction lighting. The lighting circuits are isolated at the base with a choke for each tower.
2. The Ground System for each Tower consists of (120) buried copper Radials, 92.5M in length, except where they intersect with copper transverse straps between Towers or property boundaries. Copper strap connects all Towers to the main Transmitter grounding point.
3. The Sampling System consists of four (4), Delta Electronics TCT-3, 1.0 V/A Toroidal Current Transformers. All TCT's are at the Output of each Antenna Tuning Unit. These TCT's are connected to a Potomac Instruments 1901-4 Antenna Monitor via four (4) equal lengths of Andrew, LDF2-50, 3/8" phase stabilized foam coaxial cable.
4. Tower registration numbers:
Tower 1: 1247871
Tower 2: 1247872
Tower 3: 1247873
Tower 4: 1247874

**FIGURE 1
ANTENNA SYSTEM AS ADJUSTED**

**APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
CONTINUED**

**WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015**

ANTENNA SYSTEM DESCRIPTION – Continued

DIRECTIONAL OPERATION (DAY)

COMMON POINT

Impedance = 50.0 – j 8.1 Ohms
Current = 20.5 Amperes
Power = 21,060 Watts

DIRECTIONAL OPERATION (NIGHT)

COMMON POINT

Impedance = 50.0 – j 8.1 Ohms
Current = 2.94 Amperes
Power = 432 Watts

Directional Antenna Monitor indications are within $\pm 5\%$ and $\pm 3^\circ$ of the modeled TCT values.

FIGURE 2
WRSO SAMPLING SYSTEM DESCRIPTION/MEASUREMENTS

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

SAMPLING SYSTEM DESCRIPTION

The Sampling System consists of Delta Electronics TCT-3 Toroidal Sampling Transformers (1.0 volt/amp) mounted at the base of each Tower. The sampling devices are connected to the Antenna Monitor with equal lengths of Andrew LDF2-50. The Antenna Monitor is a Potomac Instruments Model 1901-4, Serial Number 653.

SAMPLE LINE MEASUREMENTS

Impedance measurements were made of the Antenna Sampling Lines using an Array Solutions 2180 Vector Network Analyzer (VNA). Measurements were done with the lines open circuited and then connected to the TCT's.

The table below shows the frequencies above and below the carrier frequency where resonance, defined as zero reactance corresponding with low resistance, was found. Frequencies of resonance occur at odd multiples of 90 degrees electrical length, the Sample Line length at the resonant frequency above the carrier frequency, which is the closest one to the carrier frequency, was found to be 450 electrical degrees. The electrical length at carrier frequency appearing in the table below was calculated by ratioing the frequencies.

SAMPLE LINE MEASUREMENTS

	Resonant Frequency (KHz) below 810 KHz	Resonant Frequency (KHz) above 810 KHz	Calculated Electrical Length (deg) at 810 KHz	Measured Impedance (ohms) Connected to TCT @ 810 KHz
Tower 1	552.459	924.855	394.1	52.45 +j 0.25
Tower 2	552.443	924.877	394.1	52.07 +j 0.37
Tower 3	552.430	924.876	394.1	51.81 -j 0.71
Tower 4	552.428	924.777	394.1	51.48 -j 0.52

FIGURE 2
WSRF SAMPLING SYSTEM DESCRIPTION/MEASUREMENTS

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
CONTINUED

WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

SAMPLE LINE MEASUREMENTS (CONTINUED)

To determine the characteristic impedance values of the Sample Lines, open-circuited measurements were made with frequencies offset to produce ± 45 degrees of electrical length from resonance. The characteristic impedance was calculated using the following formula, where $R_1 + j X_1$ and $R_2 + j X_2$ are the measured impedances at the +45 and -45 degree offset frequencies, respectively:

$$Z_0 = ((R_1^2 + X_1^2)^{1/2} \cdot (R_2^2 + X_2^2)^{1/2})^{1/2}$$

Tower	+ 45 Degree Offset Frequency (kHz)	+ 45 Degree Measured Impedance (Ohms)	- 45 Degree Offset Frequency (kHz)	- 45 Degree Measured Impedance (Ohms)	Calculated Characteristic Impedance (Ohms)
1	1017.3	9.9 +j 48.6	832.4	9.2 -j 48.4	49.43
2	1017.4	9.9 +j 48.5	832.4	9.1 -j 48.4	49.37
3	1017.4	9.8 +j 48.6	832.4	9.2 -j 48.5	49.47
4	1017.3	9.7 +j 48.7	832.3	9.0 -j 48.5	49.49

SAMPLING TCT MEASUREMENTS

Measurements of the Delta Electronics Model TCT-3, 1.0 V/A Toroidal Current Transformers were performed by a Hewlett Packard 8752A, Network Analyzer. Measurements are normalized to Tower #2 (reference) and are within the manufacturer's rating of $\pm 2.0\%$ and $\pm 3.0^\circ$.

FIGURE 2
WSRF SAMPLING SYSTEM DESCRIPTION/MEASUREMENTS

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
CONTINUED
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
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SAMPLING TCT MEASUREMENTS CONT'D

TOWER	TCT SERIAL #	MAGNITUDE	PHASE
1	17304	1.000	0.1°
2	17307	1.000	0.0°
3	17308	1.001	0.0°
4	17309	1.002	-0.1°

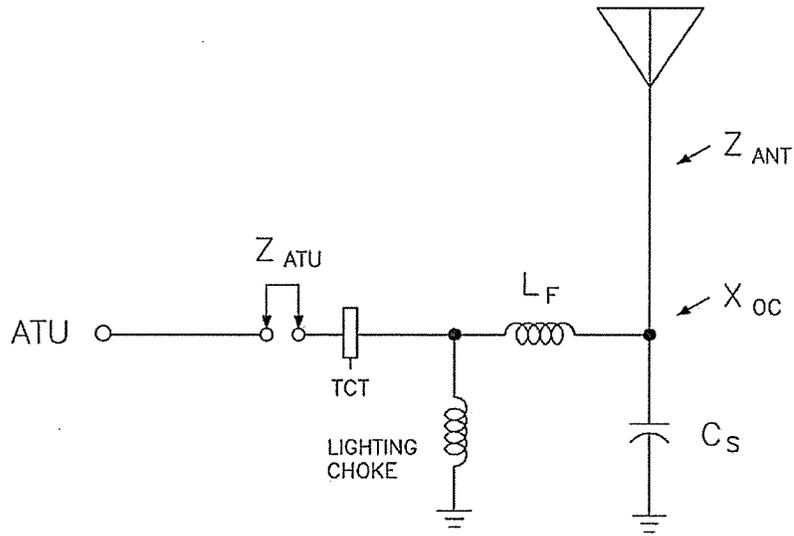
ANTENNA MONITOR MEASUREMENT

Measurement of the Potomac Instruments Model 1901-4 Antenna Monitor was performed to verify calibration. A single RF Voltage was applied to the Reference Input (Tower #2) and each other Input by use of a "T" divider and equal electrical length coaxial cables. This yields the following:

Tower	Ratio	Phase
1	1.000	0.4°
2	1.000	0.0°
3	1.000	0.2°
4	1.000	0.3°

The above is within the manufacturer's rating of $\pm 1.0\%$ and $\pm 1.0^\circ$.

FIGURE 3
WRSO TOWER IMPEDANCE MEASUREMENTS COMPARED TO
METHOD OF MOMENTS MODEL
APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015



TOWER	Specified Cs (pf)	Measured L _F (μH)	Measured X _F (Ω)	Modeled Z _{ANT} (Ω)	Modeled Z _{ATU} (Ω)	Measured Z _{ATU} (Ω)
1	15	3.93	+j20.0	51.0 +j 55.4	49.2 +j 74.5	49.0 +j 76.0
2	45	5.11	+j26.0	49.9 +j 52.3	48.7 +j 77.3	48.0 +j 78.6
3	15	4.13	+j21.0	51.0 +j 55.2	49.2 +j 75.3	49.5 +j 76.8
4	15	3.93	+j20.0	50.9 +j 55.3	49.1 +j 74.5	49.9 +j 75.1

Tower	Calculated X _{OC} (Ω)
1	+j 4,537.3
2	+j 14,883.9
3	+j 4,539.1
4	+j 4,537.3

**FIGURE 4
WRSO MOMENT MODEL PARAMETERS**

**APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
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Tower #	Wire #	# of Segments	Base Node
1	1	10	1
2	2	10	11
3	3	10	21
4	4	10	31

Tower #	Physical Height Degrees	Modeled Height Degrees	Modeled Radius Meters	% of Equivalent Radius
1	90.0	96.5	.243	100.0
2	90.0	96.0	.243	100.0
3	90.0	96.5	.243	100.0
4	90.0	96.5	.243	100.0

All Towers are uniform cross section, guyed with Base Insulator. All towers are three (3) sided, 20" face width.

All Base Insulators are manufactured by Austin Insulators, part number A-4197L, with an assumed capacity of 15pf (-j13,099.2 ohms @ 810 kHz). Tower #2 FM Isocoupler is Phasetek Inc. Model #P600-407 with a capacity of 20pf (-j9,824.4 ohms @ 810 kHz). Tower #2 STL isocoupler is a Moseley Model #ICU-1D with a capacity of 10pF (-j19,648.8 ohms @ 810 kHz).

All Towers have Kintronic Labs 3 wire lighting choke. These measure +j3,350 ohms @ 810 kHz.

FIGURE 5
WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING

WRSO, 810 KHZ, DA-2

ORLOVISTA, FLORIDA

FEBRUARY, 2015

WRSO TOWER 1 (OTHERS OPEN)

GEOMETRY

Wire coordinates in degrees; other dimensions in meters

Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4
 current nodes = 40

Individual wires	minimum		maximum	
	wire	value	wire	value
segment length	2	9.6	1	9.65
radius	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHZ)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	1	1	1.	0	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	11	0	14,883.9	0	0	0
2	21	0	4,539.1	0	0	0
3	31	0	4,537.3	0	0	0

IMPEDANCE

normalization = 50.

freq (MHZ)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = .81	1; node 51.	1, sector 55.39	1, 75.294	1, 47.4	2.8531	-6.3583	-1.1424

FIGURE 5
WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS

WRSO TOWER 2 (OTHERS OPEN)

GEOMETRY

Wire coordinates in degrees; other dimensions in meters
 Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4
 current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	lowest frequency	step	no. of steps	segment length (wavelengths) minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	11	1	1.	0	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	1	0	4,537.3	0	0	0
2	21	0	4,539.1	0	0	0
3	31	0	4,537.3	0	0	0

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node 11, sector 1							
.81	49.848	52.312	72.259	46.4	2.7319	-6.6681	-1.0534

FIGURE 5
WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS

WRSO TOWER 3 (OTHERS OPEN)

GEOMETRY

Wire coordinates in degrees; other dimensions in meters
Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4
current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	21	1	1.	0	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	1	0	4,537.3	0	0	0
2	11	0	14,883.9	0	0	0
3	31	0	4,537.3	0	0	0

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node .81	51.04	55.237	75.208	47.3	2.8444	-6.3794	-1.1361

FIGURE 5 WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS

WRSO TOWER 4 (OTHERS OPEN)

GEOMETRY

Wire coordinates in degrees; other dimensions in meters

Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4
current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	lowest frequency	step	no. of steps	segment length (wavelengths)	
				minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	31	1	1.	0	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	1	0	4,537.3	0	0	0
2	11	0	14,883.9	0	0	0
3	21	0	4,539.1	0	0	0

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node 31, sector 1							
.81	50.943	55.333	75.213	47.4	2.8517	-6.3616	-1.1414

FIGURE 6
WRSO MOMENT MODEL ARRAY SYNTHESIS
(DIRECTIONAL – DAY)

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

WRSO DAY

MEDIUM WAVE ARRAY SYNTHESIS FROM FIELD RATIOS

Frequency = .81 MHz

tower	field ratio magnitude	phase (deg)
1	1.	0
2	.931	-99.8
3	.744	-101.
4	.68	-11.3

VOLTAGES AND CURRENTS - rms

source node	voltage magnitude	phase (deg)	current magnitude	phase (deg)
1	666.332	74.8	14.3908	1.4
11	1,131.51	314.2	12.9567	265.5
21	828.243	301.5	10.6227	264.9
31	313.52	69.4	10.012	349.3

Sum of square of source currents = 1,176.11
 Total power = 20,000. watts

TOWER ADMITTANCE MATRIX

admittance	real (mhos)	imaginary (mhos)
Y(1, 1)	.00871243	-.00882986
Y(1, 2)	.00496811	.00269084
Y(1, 3)	.00272785	-.00149079
Y(1, 4)	.00332803	-.00202396
Y(2, 1)	.00496807	.00269091
Y(2, 2)	.00865981	-.00902374
Y(2, 3)	.00278277	-.00215183
Y(2, 4)	.0020943	-.00141139
Y(3, 1)	.00272784	-.00149078
Y(3, 2)	.00278277	-.00215185
Y(3, 3)	.00848884	-.00890128
Y(3, 4)	.00491857	.0025569
Y(4, 1)	.00332803	-.00202395
Y(4, 2)	.0020943	-.00141141
Y(4, 3)	.00491857	.0025569
Y(4, 4)	.00852187	-.00877838

TOWER IMPEDANCE MATRIX

impedance	real (ohms)	imaginary (ohms)
Z(1, 1)	51.0064	55.2755
Z(1, 2)	25.7748	-24.7706
Z(1, 3)	-18.1711	-3.06078
Z(1, 4)	-16.5232	-8.91811
Z(2, 1)	25.7744	-24.7709
Z(2, 2)	49.6066	52.1707
Z(2, 3)	-17.189	-5.32849
Z(2, 4)	-17.8057	1.08107

FIGURE 6
WRSO MOMENT MODEL ARRAY SYNTHESIS
(DIRECTIONAL – DAY)

Z(3, 1)	-18.171	-3.06079
Z(3, 2)	-17.189	-5.32855
Z(3, 3)	50.7966	55.1332
Z(3, 4)	25.9233	-25.0164
Z(4, 1)	-16.5232	-8.91811
Z(4, 2)	-17.8056	1.081
Z(4, 3)	25.9233	-25.0164
Z(4, 4)	50.7251	55.2564

FIGURE 7
WRSO MOMENT MODEL SUMMARY FOR
DIRECTIONAL DAY MODE

APPLICATION FOR LICENSE INFORMATION
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ORLOVISTA, FLORIDA
FEBRUARY, 2015

WRSO DAY

GEOMETRY

Wire coordinates in degrees; other dimensions in meters
 Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4
 current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	1	1	942.336	74.8	voltage
2	11	1	1,600.19	314.2	voltage
3	21	1	1,171.31	301.5	voltage
4	31	1	443.384	69.4	voltage

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node .81	1; node 13.16	1, sector 1 44.393	1 46.303	73.5	6.9132	-2.5306	-3.5497
source = 2; node .81	2; node 57.597	11, sector 1 65.643	1 87.33	48.7	3.2042	-5.6086	-1.3959
source = 3; node .81	3; node 62.626	21, sector 1 46.445	1 77.969	36.6	2.3062	-8.0665	-.737
source = 4; node .81	4; node 5.3731	31, sector 1 30.85	1 31.314	80.1	12.878	-1.3517	-5.7274

FIGURE 7
WRSO MOMENT MODEL SUMMARY FOR
DIRECTIONAL DAY MODE

CURRENT rms
 Frequency = .81 MHz
 Input power = 20,000. watts
 Efficiency = 100. %
 coordinates in degrees

current	no.	X	Y	Z	mag (amps)	phase (deg)	real (amps)	imaginary (amps)
GND	0	0	0	0	14.3908	1.4	14.3868	.340922
	2	0	0	9.65	14.7135	.8	14.7121	.202131
	3	0	0	19.3	14.5145	.4	14.5141	.10502
	4	0	0	28.95	13.8928	.1	13.8927	.0264191
	5	0	0	38.6	12.8779	359.8	12.8778	-.0355023
	6	0	0	48.25	11.4992	359.6	11.4989	-.0803309
	7	0	0	57.9	9.78984	359.4	9.78926	-.107014
	8	0	0	67.55	7.78531	359.2	7.78447	-.114348
	9	0	0	77.2	5.51781	359.	5.51688	-.101099
	10	0	0	86.85	2.9972	358.7	2.99649	-.0656428
END	0	0	0	96.5	0	0	0	0
GND	13.1475	-89.0345	0	12.9567	265.5	-1.02345	-12.9162	
12	13.1475	-89.0345	9.6	13.4673	263.	-1.63043	-13.3682	
13	13.1475	-89.0345	19.2	13.4336	261.6	-1.97168	-13.2881	
14	13.1475	-89.0345	28.8	12.9755	260.4	-2.15967	-12.7945	
15	13.1475	-89.0345	38.4	12.1214	259.5	-2.21057	-11.9181	
16	13.1475	-89.0345	48.	10.8978	258.7	-2.13273	-10.6871	
17	13.1475	-89.0345	57.6	9.33466	258.	-1.93352	-9.13221	
18	13.1475	-89.0345	67.2	7.46468	257.5	-1.62078	-7.28659	
19	13.1475	-89.0345	76.8	5.31777	256.9	-1.20195	-5.18015	
20	13.1475	-89.0345	86.4	2.90268	256.5	-.6796	-2.822	
END	13.1475	-89.0345	96.	0	0	0	0	
GND	223.323	-27.4206	0	10.6227	264.9	-.938196	-10.5812	
22	223.323	-27.4206	9.65	10.8886	262.3	-1.46813	-10.7892	
23	223.323	-27.4206	19.3	10.7693	260.6	-1.76492	-10.6236	
24	223.323	-27.4206	28.95	10.3339	259.3	-1.92665	-10.1527	
25	223.323	-27.4206	38.6	9.60155	258.2	-1.9675	-9.3978	
26	223.323	-27.4206	48.25	8.59224	257.3	-1.89486	-8.3807	
27	223.323	-27.4206	57.9	7.32948	256.5	-1.71532	-7.12594	
28	223.323	-27.4206	67.55	5.83915	255.8	-1.43594	-5.65983	
29	223.323	-27.4206	77.2	4.14509	255.1	-1.06348	-4.00635	
30	223.323	-27.4206	86.85	2.25478	254.6	-.60047	-2.17336	
END	223.323	-27.4206	96.5	0	0	0	0	
GND	199.427	59.4518	0	10.012	349.3	9.83826	-1.85722	
32	199.427	59.4518	9.65	10.1324	349.1	9.94864	-1.92081	
33	199.427	59.4518	19.3	9.93024	348.9	9.74478	-1.91023	
34	199.427	59.4518	28.95	9.45594	348.8	9.27484	-1.84179	
35	199.427	59.4518	38.6	8.72779	348.6	8.55677	-1.7193	
36	199.427	59.4518	48.25	7.765	348.5	7.60953	-1.54606	
37	199.427	59.4518	57.9	6.58971	348.4	6.45499	-1.32568	
38	199.427	59.4518	67.55	5.22569	348.3	5.11665	-1.06198	
39	199.427	59.4518	77.2	3.6943	348.2	3.61563	-.75833	
40	199.427	59.4518	86.85	2.00203	348.	1.95853	-.415087	
END	199.427	59.4518	96.5	0	0	0	0	

FIGURE 8
WRSO MOMENT MODEL ARRAY SYNTHESIS
(DIRECTIONAL – NIGHT)

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

WRSO NIGHT

MEDIUM WAVE ARRAY SYNTHESIS FROM FIELD RATIOS

Frequency = .81 MHz

tower	field ratio magnitude	phase (deg)
1	1.	0
2	0	0
3	.95	-29.5
4	0	0

VOLTAGES AND CURRENTS - rms

source node	voltage magnitude	phase (deg)	current magnitude	phase (deg)
1	164.627	63.8	2.37815	3.2
11	48.2653	296.8	.0838396	27.5
21	132.326	21.8	2.32942	334.2
31	93.6368	269.	.167967	358.8

Sum of square of source currents = 22.234
 Total power = 400. watts

TOWER ADMITTANCE MATRIX
 admittance real (mhos)

	real (mhos)	imaginary (mhos)
Y(1, 1)	.00871243	-.00882986
Y(1, 2)	.00496811	.00269084
Y(1, 3)	.00272785	-.00149079
Y(1, 4)	.00332803	-.00202396
Y(2, 1)	.00496807	.00269091
Y(2, 2)	.00865981	-.00902374
Y(2, 3)	.00278277	-.00215183
Y(2, 4)	.0020943	-.00141139
Y(3, 1)	.00272784	-.00149078
Y(3, 2)	.00278277	-.00215185
Y(3, 3)	.00848884	-.00890128
Y(3, 4)	.00491857	.0025569
Y(4, 1)	.00332803	-.00202395
Y(4, 2)	.0020943	-.00141141
Y(4, 3)	.00491857	.0025569
Y(4, 4)	.00852187	-.00877838

TOWER IMPEDANCE MATRIX
 impedance real (ohms)

	real (ohms)	imaginary (ohms)
Z(1, 1)	51.0064	55.2755
Z(1, 2)	25.7748	-24.7706
Z(1, 3)	-18.1711	-3.06078
Z(1, 4)	-16.5232	-8.91811
Z(2, 1)	25.7744	-24.7709
Z(2, 2)	49.6066	52.1707
Z(2, 3)	-17.189	-5.32849
Z(2, 4)	-17.8057	1.08107
Z(3, 1)	-18.171	-3.06079
Z(3, 2)	-17.189	-5.32855

FIGURE 8
WRSO MOMENT MODEL ARRAY SYNTHESIS
(DIRECTIONAL – NIGHT)

Z(3, 3)	50.7966	55.1332
Z(3, 4)	25.9233	-25.0164
Z(4, 1)	-16.5232	-8.91811
Z(4, 2)	-17.8056	1.081
Z(4, 3)	25.9233	-25.0164
Z(4, 4)	50.7251	55.2564

FIGURE 9
WRSO MOMENT MODEL SUMMARY FOR
DIRECTIONAL NIGHT MODE

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

GEOMETRY
WRSO NIGHT

GEOMETRY
Wire coordinates in degrees; other dimensions in meters
Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4
current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION
Frequencies (MHZ)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	1	1	232.817	63.8	voltage
2	21	1	187.137	21.8	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	11	0	575.64	0	0	0
2	31	0	557.47	0	0	0

IMPEDANCE

normalization = 50.							
freq (MHZ)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node 1, sector 1							
.81	33.962	60.298	69.204	60.6	4.0454	-4.385	-1.9677
source = 2; node 21, sector 1							
.81	38.307	41.942	56.803	47.6	2.6061	-7.0254	-.96023

FIGURE 9
WRSO MOMENT MODEL SUMMARY FOR
DIRECTIONAL NIGHT MODE

CURRENT rms
 Frequency = .81 MHz
 Input power = 400. watts
 Efficiency = 100. %
 coordinates in degrees

current	no.	X	Y	Z	mag (amps)	phase (deg)	real (amps)	imaginary (amps)
	GND	0	0	0	2.37861	3.2	2.37493	.132359
	2	0	0	9.65	2.46164	1.7	2.4605	.0750189
	3	0	0	19.3	2.44764	.8	2.44738	.036138
	4	0	0	28.95	2.35775	.1	2.35775	5.86E-03
	5	0	0	38.6	2.19733	359.6	2.19726	-.0168924
	6	0	0	48.25	1.97135	359.1	1.97108	-.0323633
	7	0	0	57.9	1.68539	358.6	1.6849	-.0406187
	8	0	0	67.55	1.34544	358.2	1.34479	-.0417169
	9	0	0	77.2	.956957	357.9	.95629	-.0357237
	10	0	0	86.85	.521547	357.5	.521059	-.0225592
	END	0	0	96.5	0	0	0	0
	GND	13.1475	-89.0345	0	.0839735	26.8	.074951	.0378669
	12	13.1475	-89.0345	9.6	.0462457	26.7	.0412989	.0208101
	13	13.1475	-89.0345	19.2	.0212658	26.3	.0190663	9.42E-03
	14	13.1475	-89.0345	28.8	2.42E-03	17.1	2.32E-03	7.13E-04
	15	13.1475	-89.0345	38.4	.0112656	210.2	-9.73E-03	-5.67E-03
	16	13.1475	-89.0345	48.	.0200294	209.5	-.0174351	-9.86E-03
	17	13.1475	-89.0345	57.6	.0242098	209.5	-.021067	-.0119289
	18	13.1475	-89.0345	67.2	.0241126	209.7	-.020936	-.0119625
	19	13.1475	-89.0345	76.8	.0200658	210.	-.0173698	-.0100462
	20	13.1475	-89.0345	86.4	.0123212	210.4	-.0106294	-6.23E-03
	END	13.1475	-89.0345	96.	0	0	0	0
	GND	223.323	-27.4206	0	2.32935	334.2	2.09728	-1.01355
	22	223.323	-27.4206	9.65	2.37803	332.6	2.11045	-1.09592
	23	223.323	-27.4206	19.3	2.34445	331.5	2.06053	-1.11833
	24	223.323	-27.4206	28.95	2.24331	330.7	1.95597	-1.09846
	25	223.323	-27.4206	38.6	2.07908	330.	1.80038	-1.03981
	26	223.323	-27.4206	48.25	1.85632	329.4	1.59776	-.945034
	27	223.323	-27.4206	57.9	1.58028	328.9	1.35275	-.816912
	28	223.323	-27.4206	67.55	1.25663	328.4	1.07033	-.658427
	29	223.323	-27.4206	77.2	.890562	328.	.755004	-.472303
	30	223.323	-27.4206	86.85	.483689	327.6	.408257	-.259387
	END	223.323	-27.4206	96.5	0	0	0	0
	GND	199.427	59.4518	0	.1679	358.9	.167871	-3.11E-03
	32	199.427	59.4518	9.65	.094281	358.9	.0942651	-1.73E-03
	33	199.427	59.4518	19.3	.0448671	359.	.0448606	-7.6E-04
	34	199.427	59.4518	28.95	6.88E-03	.2	6.88E-03	2.49E-05
	35	199.427	59.4518	38.6	.021208	178.3	-.0211983	6.41E-04
	36	199.427	59.4518	48.25	.0398862	178.4	-.0398714	1.08E-03
	37	199.427	59.4518	57.9	.0494597	178.4	-.0494414	1.34E-03
	38	199.427	59.4518	67.55	.0502426	178.4	-.0502228	1.41E-03
	39	199.427	59.4518	77.2	.0425701	178.3	-.0425515	1.26E-03
	40	199.427	59.4518	86.85	.0266035	178.2	-.02659	8.48E-04
	END	199.427	59.4518	96.5	0	0	0	0

**FIGURE 10
DERIVED DIRECTIONAL PARAMETERS**

**APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015**

DAY:

Tower	Theoretical		Base Network Input Current		Normalized TCT	
	Field	Phase	Amplitude	Phase	Amplitude	Phase
1 (SW)	1.000	0.0°	14.62	+1.15°	1.114	+95.9°
2 (SE)	.931	-99.8°	13.12	-94.76°	1.000	0.0°
3 (NE)	.744	-101.0°	10.80	-95.84°	.823	-1.1°
4 (NW)	.680	-11.3°	10.14	-10.79°	.773	+84.0°

NIGHT:

Tower	Theoretical		Base Network Input Current		Normalized TCT	
	Field	Phase	Amplitude	Phase	Amplitude	Phase
1 (SW)	1.000	0.0°	2.42	+2.77°	1.000	0.0°
2 (SE)			DETUNED			
3 (NE)	.950	-29.5°	2.37	-26.27°	.979	-29.0°
4 (NW)			DETUNED			

FIGURE 11
WRSO TOWER BASE CIRCUIT ANALYSIS DESCRIPTION

APPLICATION FOR LICENSE INFORMATION
EMPLOYING MOMENT METHOD MODELING
WRSO, 810 KHZ, DA-2
ORLOVISTA, FLORIDA
FEBRUARY, 2015

CIRCUIT ANALYSIS

Circuit Analysis was performed on each Tower of the WRSO model. "Phasetek" nodal Circuit Analysis program was used to compute base model Input/Output voltages and currents. For the Directional modes, the calculated Mininec Tower Base Drive Voltage was used to determine the Base Network Input Current. This point is the location of the Sampling TCT. " Z_1 " represents the ATU Shunt impedance, " Z_2 " represents the Tower Feed impedance, and " Z_3 " represents the Tower Base Shunt impedance.

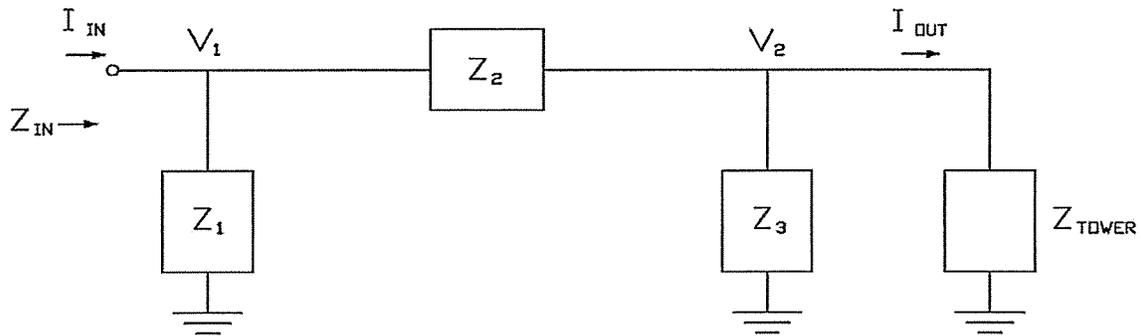


FIGURE 12
WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS

CUSTOMER : WRSO
 NETWORK ID : TOWER 1 (OTHERS OPEN)

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 51.00, 55.39 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.43	55.42
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	82.82	-8.57

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	49.18	74.50	89.27	56.57
INPUT CURRENT (AMPS) :	0.62	-0.93	1.12	-56.57
OUTPUT CURRENT (AMPS) :	0.62	-0.91	1.10	-55.93

INPUT/OUTPUT CURRENT RATIO = 1.0183
 INPUT/OUTPUT PHASE = -0.64 DEGREES

FIGURE 12
WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS

CUSTOMER : WRSO
 NETWORK ID : TOWER 2 (OTHERS OPEN)

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 26.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -4366.40 OHMS
 TOWER IMPEDANCE (R,X) : 49.85, 52.31 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.06	52.36
1		2	0.00	26.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	78.19	-11.19

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	48.74	77.29	91.38	57.76
INPUT CURRENT (AMPS) :	0.58	-0.93	1.09	-57.76
OUTPUT CURRENT (AMPS) :	0.58	-0.91	1.08	-57.57

INPUT/OUTPUT CURRENT RATIO = 1.0113
 INPUT/OUTPUT PHASE = -0.19 DEGREES

FIGURE 12
WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS

CUSTOMER : WRSO
 NETWORK ID : TOWER 3 (OTHERS OPEN)

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 21.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 51.04, 55.24 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.47	55.27
1		2	0.00	21.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	82.08	-8.95

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	49.20	75.31	89.95	56.85
INPUT CURRENT (AMPS) :	0.61	-0.93	1.11	-56.85
OUTPUT CURRENT (AMPS) :	0.61	-0.91	1.09	-56.21

INPUT/OUTPUT CURRENT RATIO = 1.0186
 INPUT/OUTPUT PHASE = -0.64 DEGREES

FIGURE 12
WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS

CUSTOMER : WRSO
 NETWORK ID : TOWER 4 (OTHERS OPEN)

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 50.94, 55.33 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.38	55.37
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	82.81	-8.58

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	49.13	74.45	89.20	56.58
INPUT CURRENT (AMPS) :	0.62	-0.94	1.12	-56.58
OUTPUT CURRENT (AMPS) :	0.62	-0.91	1.10	-55.94

INPUT/OUTPUT CURRENT RATIO = 1.0183
 INPUT/OUTPUT PHASE = -0.64 DEGREES

FIGURE 13
WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE

CUSTOMER : WRSO
 NETWORK ID : TOWER 1 DAY

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 13.16, 44.39 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	13.25	44.53
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	944.81	79.77
2	666.33	74.80

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	12.75	63.36	64.63	78.62
INPUT CURRENT (AMPS) :	14.62	0.29	14.62	1.15
OUTPUT CURRENT (AMPS) :	14.39	0.33	14.39	1.31

INPUT/OUTPUT CURRENT RATIO = 1.0158
 INPUT/OUTPUT PHASE = -0.16 DEGREES

FIGURE 13
WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE

CUSTOMER : WRSO
 NETWORK ID : TOWER 2 DAY

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 26.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -4366.40 OHMS
 TOWER IMPEDANCE (R,X) : 57.60, 65.64 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	59.36	65.85
1		2	0.00	26.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	1395.79	-36.64
2	1131.51	314.20

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	56.22	90.37	106.43	58.12
INPUT CURRENT (AMPS) :	-1.09	-13.07	13.12	-94.76
OUTPUT CURRENT (AMPS) :	-1.02	-12.92	12.96	-94.54

INPUT/OUTPUT CURRENT RATIO = 1.0122
 INPUT/OUTPUT PHASE = -0.22 DEGREES

FIGURE 13
WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE

CUSTOMER : WRSO
 NETWORK ID : TOWER 3 DAY

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 21.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 62.63, 46.44 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	63.07	46.31
1		2	0.00	21.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	976.38	-47.93
2	828.24	301.50

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	60.59	67.10	90.41	47.92
INPUT CURRENT (AMPS) :	-1.10	-10.74	10.80	-95.84
OUTPUT CURRENT (AMPS) :	-0.94	-10.58	10.62	-95.06

INPUT/OUTPUT CURRENT RATIO = 1.0167
 INPUT/OUTPUT PHASE = -0.78 DEGREES

FIGURE 13
WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE

CUSTOMER : WRSO
 NETWORK ID : TOWER 4 DAY

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 5.37, 30.85 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	5.40	30.92
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	511.47	73.25
2	313.52	69.40

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	5.24	50.17	50.44	84.04
INPUT CURRENT (AMPS) :	9.96	-1.90	10.14	-10.79
OUTPUT CURRENT (AMPS) :	9.84	-1.86	10.01	-10.72

INPUT/OUTPUT CURRENT RATIO = 1.0128
 INPUT/OUTPUT PHASE = -0.07 DEGREES

FIGURE 14
WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL NIGHT MODE

CUSTOMER : WRSO
 NETWORK ID : TOWER 1 NIGHT

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 33.96, 60.30 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	34.28	60.49
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	207.15	70.27
2	164.63	63.80

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	32.68	78.93	85.43	67.51
INPUT CURRENT (AMPS) :	2.42	0.12	2.42	2.77
OUTPUT CURRENT (AMPS) :	2.38	0.13	2.38	3.19

INPUT/OUTPUT CURRENT RATIO = 1.0194
 INPUT/OUTPUT PHASE = -0.42 DEGREES

FIGURE 14
WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL NIGHT MODE

CUSTOMER : WRSO
 NETWORK ID : TOWER 3 NIGHT

FREQUENCY : 810.00 kHz
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS
 TOWER FEED IMPEDANCE (R,X) : 0.00, 21.00 OHMS
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS
 TOWER IMPEDANCE (R,X) : 38.31, 41.94 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	38.55	41.96
1		2	0.00	21.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	171.44	32.90
2	132.33	21.80

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	37.14	62.22	72.46	59.17
INPUT CURRENT (AMPS) :	2.12	-1.05	2.37	-26.27
OUTPUT CURRENT (AMPS) :	2.10	-1.01	2.33	-25.79

INPUT/OUTPUT CURRENT RATIO = 1.0156
 INPUT/OUTPUT PHASE = -0.48 DEGREES

FIGURE 15

WRSO REFERENCE POINTS -- DA-D

1/3/2015

<u>Radial</u>		<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>	
						<u>deg</u>	<u>min</u>		<u>sec</u>
N 10 E	1	1.52	1003	160.0	N	28	35	6.4	Mercy Drive at Unisource entrance
					W	81	25	52.5	
	2	4.91	1020	35.0	N	28	36	54.4	Parking lot of #6401 Edgewater Drive
					W	81	25	31.7	
	3	5.45	1025	33.0	N	28	37	11.9	Driveway 3531 Dr. Love Road
					W	81	25	27.9	
N 72 E	1	1.84	1040	1310.0	N	28	34	36.2	John Young Pkwy. --south end of Wawa parking lot
					W	81	24	57.4	
	2	2.40	1048	1080.0	N	28	34	41.9	Regent Ave. 100' north of Silver Star Rd.
					W	81	24	37.9	
	3	2.74	1053	1100.0	N	28	34	45.5	Orange Blossom Trail opposite gate
					W	81	24	26.2	
N 127.5 E	1	2.22	1126	138.0	N	28	33	35.3	100' west of int. John Young Pkwy + WD Judge Road
					W	81	24	56.8	
	2	3.67	1105	81.0	N	28	33	5.9	Arlington St + Vern Dr -- southwest corner
					W	81	24	14.6	
	3	3.54	1114	105.0	N	28	33	8.5	W Colonial Dr -- east edge of Citgo parking lot
					W	81	24	19.1	

FIGURE 15 CONTINUED

WRSO REFERENCE POINTS -- DA-D cont. 1/3/2015

<u>Radial</u>		<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>	
					<u>deg</u>	<u>min</u>	<u>sec</u>		
N 230 E	1	2.48	1048	7.6	N	28	33	26.6	San Domingo Rd near Balboa -- drwy opp spd lim 25
					W	81	27	12.1	
	2	2.93	1032	22.0	N	28	33	16.7	Mailbox 810 Governors Ave
					W	81	27	24.4	
	3	3.24	1027	18.3	N	28	33	10.6	Hastings St -- St Andrew Church lot drwy
					W	81	27	33.6	
N 269.5 E	1	1.45	1055	43.0	N	28	34	17.0	Drwy 2117 Beecher St
					W	81	26	55.2	
	2	1.94	1105	20.5	N	28	34	16.9	Casa Vida Apts. @ curve south of Building N -- on road
					W	81	27	13.6	
	3	2.27	1112	22.2	N	28	34	15.6	Golf Club Pkwy + Silver Spruce @ fire hydrant
					W	81	27	25.4	
N 322.5 E	1	2.60	1122	24.2	N	28	35	24.5	White Heron Dr + Donovan St -- west side
					W	81	27	0.8	
	2	2.89	1128	27.8	N	28	35	31.5	Grandview off Pine Hills Rd @ spd lim 25
					W	81	27	7.9	
	3	3.50	1133	23.1	N	28	35	47.0	Mailbox 4403 Robbins Ave
					W	81	27	22.0	

FIGURE 15 CONTINUED

WRSO REFERENCE POINTS -- DA-N

1/3/2015

<u>Radial</u>		<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>	
					<u>deg</u>	<u>min</u>	<u>sec</u>		
N 28.5 E	1	1.24	1338	14.1	N	28	34	58.6	Road to industrial building -- @ fence
					W	81	25	41.3	
	2	2.16	1353	7.7	N	28	35	18.8	Int of Bay Lake Road + Eunice Ave
					W	81	25	22.7	
	3	3.73	1403	5.6	N	28	36	3.2	Trotters Park lot by fire hydrant + stop sign
					W	81	24	55.2	
N 89.5 E	1	2.31	1428	135.0	N	28	34	18.5	Lynx Lane @ bus stop
					W	81	24	37.1	
	2	2.71	1413	91.0	N	28	34	19.3	Orange Blossom Trl W side -- Pr'ton Commerce Ctr.
					W	81	24	22.1	
	3	3.11	1421	72.0	N	28	34	19.1	1503 W Smith St -- parking lot
					W	81	24	7.5	
N 139 E	1	3.05	1453	8.0	N	28	33	3.8	John Young Pkwy W side -- center of mall parking lot
					W	81	24	47.8	
	2	4.04	1448	1.95	N	28	32	39.1	int Lakeland Ave + Washington St
					W	81	24	25.1	
	3	4.68	1439	2.8	N	28	32	23.7	Church St opp stadium box office
					W	81	24	9.0	

FIGURE 15 CONTINUED

WRSO REFERENCE POINTS -- DA-N cont. 1/3/2015

<u>Radial</u>		<u>Dist</u>		<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>
		<u>km</u>	<u>Time</u>		<u>deg</u>	<u>min</u>	<u>sec</u>	
N 235 E	1	1.76	1343	7.0	N 28 33 45.2			Mailbox 4913 Cortez Dr
					W 81 26 55.0			
	2	2.09	1350	4.5	N 28 33 39.1			Drwy 1109 Santa Anita St
					W 81 27 4.8			
	3	2.46	1356	9.6	N 28 33 31.8			Mailbox 1006 Emerald Rd
					W 81 27 15.9			
N 284.5 E	1	1.70	1406	120.0	N 28 34 31.3			Queensway Rd + Kipp @ street sign
					W 81 27 2.6			
	2	2.30	1413	96.0	N 28 34 37.1			Drwy 5800 Golf Club Pkwy
					W 81 27 23.7			
	3	3.02	1419	71.0	N 28 34 42.1			Mailbox 2609 Pioneer Rd
					W 81 27 49.7			
N 345.5 E	1	1.14	1432	20.4	N 28 34 53.5			Seaboard Rd north side @ C+S -- on drain
					W 81 26 13.0			
	2	1.67	1441	13.7	N 28 35 10.1			Shader Rd W of Daltile plant + rail -- S side @ drain
					W 81 26 17.6			
	3	4.45	1458	3.0	N 28 36 37.3			opp drwy 5426 Lee Ann Dr
					W 81 26 43.6			

FIGURE 16: CERTIFIED ARRAY GEOMETRY SURVEY

Summary of Post Construction Certified Array Geometry

Tower	Specified Array Geometry			Post-Construction Certification*		Distance From Specified Base Location	
	Spacing (Deg.)	Spacing (Meters)	Azimuth (Deg. T.)	Spacing (Feet)	Azimuth (Deg. T.)	(Meters)	(Deg.)
1	Ref.	Ref.	Ref.	Ref.	Ref.	Ref.	Ref.
2	90.0	92.53	81.6	302.69	81.5	0.35	0.3
3	225.0	231.33	7.0	759.74	6.9	0.61	0.6
4	208.1	213.95	343.4	702.41	343.2	0.69	0.7

*From March 27, 2015 Record Survey Plan prepared by William D. Donley

The "as built" tower displacements from their specified locations, expressed in electrical degrees at carrier frequency, which correspond to space phasing differences in the far-field radiation pattern of the array, are well below the +/- degree operating phase range specified for antenna monitor parameters by the FCC Rules.

