

# **Report Of Intermodulation Product Findings**

**Tulsa, Oklahoma**

<b>KWEN</b>	<b>95.5 MHz.</b>
<b>KRAV</b>	<b>96.5 MHz.</b>
<b>KMOD</b>	<b>97.5 MHz.</b>

**Job # 21602**

**August 16, 2008**

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**REPORT OF FINDINGS**  
**KWEN / KRAV / KMOD**  
95.5 MHz. / 96.5 MHz. / 97.5 MHz.

**Introduction:** This report of findings is based on data collected at the KWEN, KRAV, and KMOD broadcast facility located in Tulsa, Oklahoma. The report includes measurements offered as proof that the combined operations of KWEN (95.5 MHz), KRAV (96.5 MHz.), and KMOD ( 97.6 MHz. ) transmitters are in compliance with the FCC Rules and Regulations as required by the Code of Federal Regulations (CFR) Title 47 section 73.317 paragraph (b) through (d). In brief, the collection of measurements presented in this report shows that all possible third order inter-modulation (IM) products generated by this multiplex system are less than the maximum allowable level as required by section 73.317 (b) through (d). Mark Garrison of Electronics Research, Inc. located in Chandler, Indiana performed the measurements summarized herein on August 16, 2008.

**The following exhibits are provided:**

Exhibit A:

- A-1 Drawing Depicting Antenna.
- A-2 SHPX-10BC-SP Antenna Specification Sheet.
- A-3 Drawing Depicting Multiplexing Scheme.
- A-4 973 Series Constant Impedance Specification Sheet.
- A-5 Theoretical Vertical Plane Relative Field Antenna Plots

Exhibit B:

- B-1 Equipment Employed In Intermodulation Product Measurement.
- B-2 Broadcasting Scheme of the Multiplexed Systems.
- Table 1. Carrier Reference Levels.
- Table 2. Calculated Third Order Products.
- Table 3. Intermodulation Analysis Measurements.

**Exhibits Accompanying Report:** Exhibit A provides comprehensive information on both antenna and filters used by these radio stations. Exhibit B illustrates the broadcasting scheme of each station, the layout of the equipment used to isolate and measure potential Intermodulation products and forward carrier reference levels. Found within Table 1 are the narrow band carrier frequency measurements that provide relative output signal levels for the IM analysis. Table 2 lists the calculated third order products that can be generated from FM transmitters broadcasting from the constant impedance system. The IM Analysis Measurements, in Table 3, provides detailed information obtained from the product frequency investigation.

**The Nature of Intermodulation Products (IM):** Intermodulation products result from inadequate transmitter-to-transmitter isolation. Intermodulation products generated from radio stations operating into multiplexed facilities and congested antenna broadcast sites. The mechanics associated with the phenomenon have been well documented. When two or more transmitters are coupled to each other, new spectral components are produced by the mixing of the station frequencies in the active circuits of each transmitter. The common term used to describe this phenomenon is third order product denoted by the mathematical expression  $[2(F_1)-(F_2)]$ , where  $F_1$  signifies the frequency of the transmitter that is generating the Intermodulation product, and  $F_2$  signifies the frequency causing the interference.

**The Multiplexed System:** These measurements were taken with three FM stations operating from the combined antenna system. The KWEN, KRAV, and KMOD system is fundamentally comprised of antenna, feed line and constant impedance system. The SHPX-10BC-SP (antenna) and 973 Series Constant Impedance combiner system and 1431 feet of 6 1/8" MAXLINE are products of Electronics Research, Inc, Refer to Exhibit B-1, for an illustration of the Broadcasting Scheme of these stations.

To accomplish the aggregation of three transmitter signals into a common antenna feed and provide transmitter-to-transmitter isolation, a Constant Impedance combiner was installed. Specifically, the Constant Impedance Combiner utilizes three ERI Model 973-8 series combiners with nonadjacent coupling and group delay compensation module for each station, which is illustrated in the attached Exhibit A-3. The constant impedance combiner, fully assembled, exhibited transmitter port-to-port isolation in excess of -56dB. Other performance measurements, such as match, loss, group-delay, etc, revealed that the multiplexer unit was in proper working condition. Refer to Exhibit A-4 for the Combiner Specification Sheet.

**The IM Investigation:** Directional Couplers were placed at key locations throughout the combiner to monitor and maintain the multiplexer's performance. All couplers furnished with the system are factory calibrated and capable of delivering accurate and repeatable RF measurements. To facilitate the taking of the measurements, the coupler located at the antenna output of the 973 series constant impedance combiner system was used. Care was taken in the selection of the measurement location to insure that the measurements would be made far removed from transmitters and any filtering used to reduce broadcast emissions. The coupler selected would normally be used for antenna reflection measurements and thus would provide greater than -35 dB directivity and a forward signal sample of -60 dB.

The forward port of the coupler was used for sampling the outgoing carrier levels and IM products. The IM sampled signal was fed by shielded cable into a Band Pass Filter where all extraneous energy was steeply attenuated. Various attenuation pads were used, when needed, on the band pass filter and/or the FIM-71 to ensure an adequate signal level for measurements without overloading the measurement equipment. A Potomac Instruments FIM-71 Field Strength Receiver Serial # 242 was employed to record the level of all signals investigated. To facilitate the selective tuning of the Receiver and Band Pass Filter a Wavetek Model 3000 Serial # 7512028 signal generator was used. A Rhode & Swartz Analyzer with Spectrum Analyzer option Model ZVL3 Serial # 100396 was used to measure the close in spectral attenuation of each carrier and wide band search for any anomalies that may need further investigation. See attached Exhibit B-1 for an illustration of the measurement equipment.

Prior to recording measurements, all pertinent broadcasting equipment including Transmitters, Constant Impedance Combiner, Feed Line and Antenna were adjusted to optimal performance. In addition, it was confirmed before taking any measurements that all stations of concern were operating at their full licensed power level. From the equipment setup described above, the relative output signal level of each stations forward carrier was made. The resulting signal levels of these measurements are listed in Table 1, column labeled "Adjusted Level". This level will be used as the reference level for possible IM products of each carrier and was necessary to confirm that no significant levels of spurious energy, referenced to each carrier, were present from any transmitter operating from the multiplexed system.

**Table 1 - Carrier Reference Levels.**

Transmitter Frequency (MHz)	Interfering Frequency (MHz)	Pad (dB)	Bandpass Filter Loss (dB)	Total Loss	Full Scale Range (dBμ)	Scale Reading (dBμ)	Adjusted Level (dBμ)	Carrier Reference Level (dBμ)	Level Referenced to Carrier (dB)
95.5	Ref.	6		6	120	7		119	
96.5	Ref.	6		6	120	7		119	
97.5	Ref.	6		6	120	6.5		119.5	

Predictable third-order products due to system harmonics mixed with all on-site interfering frequencies that could be generated from the multiplexed system are calculated and listed in Table 2.

**Table 2 - Third order Products.**

Product Number	Product Frequency (MHz)	Transmitter Frequency (MHz)	Interfering Frequency (MHz)
1	92.5	95.5	98.5
2	93.5	95.5	97.5
3	94.5	95.5	96.5
4	94.5	96.5	98.5
5	95.5	96.5	97.5
6	96.5	97.5	98.5
7	97.5	96.5	95.5
8	98.1	95.5	92.9
9	98.5	97.5	96.5
10	99.5	97.5	95.5
11	100.1	96.5	92.9
12	102.1	97.5	92.9

Using the equipment previously described the IM product measurements were recorded and are listed in Table 3. The signal levels referenced to the carriers are calculated and listed in the column labeled "Level Referenced to Carrier". Refer to Exhibit B-2 for a layout of the measurement equipment.

## IM Measurements Taken in Tulsa, Oklahoma 8-16-08

Product Frequency (MHz)	Transmitter Frequency (MHz)	Interfering Frequency (MHz)	Pad (dB)	Bandpass Filter Loss (dB)	Total Loss	Full Scale Range (dBμ)	Scale Reading (dBμ)	Adjusted Level (dBμ)	Carrier Reference Level (dBμ)	Level Referenced to Carrier (dB)	Notes*
92.5	95.5	98.5	6	11.5	17.5	20	20	17.5	119	-101.5	
93.5	95.5	97.5	6	11.9	17.9	20	20	17.9	119	-101.1	
94.5	95.5	96.5	6	12	18	20	20	18	119	-101	
94.5	96.5	98.5	6	12	18	20	20	18	119	-101	
95.5	96.5	97.5	6	12	18	20	20	18	119	-101	
96.5	97.5	98.5	6	12	18	20	6	32	119.5	-87.5	
97.5	96.5	95.5	6	11.9	17.9	20	20	17.9	119	-101.1	
98.1	95.5	92.9	6	11.1	17.1	20	2	35.1	119	-83.9	
98.5	97.5	96.5	6	13	19	20	2	37	119.5	-82.5	
99.5	97.5	95.5	6	13	19	20	20	19	119.5	-100.5	
100.1	96.5	92.9	6	12.1	18.1	20	20	18.1	119	-100.9	
102.1	97.5	92.9	6	13	19	20	20	19	119.5	-100.5	

The R & S Analyzer with an option Spectrum Analyzer was used to check the close in spectral attenuation of the carrier to confirm the operation of the transmitter is in compliance with Sections (b) and (c) of the FCC Rules and Regulations.

As a final proof of the systems IM Product performance, a wide band search was undertaken using the Spectrum Analyzer. The purpose for this measurement was to look for suspicious anomalies that may warrant further investigation. My search ranged the complete frequency span of the receiver and resulted in no additional investigations.

**Conclusion:** Based upon my observations and measurements taken on August 16, 2008 as summarized in this document, I, Mark Garrison, find the subject system- specifically the transmitter and filter system for the operation of KWEN, KRAV, and KMOD into the antenna to be in proper working order. Furthermore, based on the measured data, it is my opinion that there are no inter-modulation products in excess of 80 dB below carrier levels generated from or within the station operating on the installed system. Based on this recorded data, I conclude that KWEN, KRAV, and KMOD comply with the requirements of Section 73.317 paragraph (b) through (d) of the FCC Rules and Regulations.

Respectfully submitted,  
Electronics Research, Inc.

Mark Garrison, Field Technician

State of Indiana

( County of Warrick )      SS:

**AFFIDAVIT**

I, Mark Garrison, hereby declare that the following statements are true and correct to the best of my knowledge and belief :

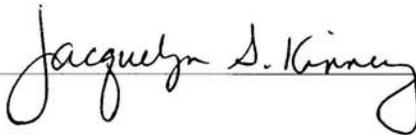
- 1.) I am a Field Technician for Electronics Research, Inc (“ERI”) and have been employed by ERI for 6 years. I am familiar with and have assisted in the design, manufacturing and installation of FM Antennas and FM Multiplexers in my tenure with ERI.
- 2.) I have either prepared and/or directly supervised the preparation of all technical information contained in this Report of Findings and to my knowledge to be accurate and true.
- 3.) ERI has been requested by COX Radio on behalf of radio Stations KWEN, KRAV, and KMOD of Tulsa, Okalohma. to prepare this Report Of Findings.

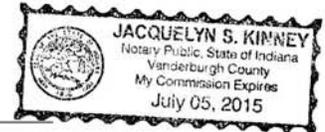
Mark Garrison; Field Technician



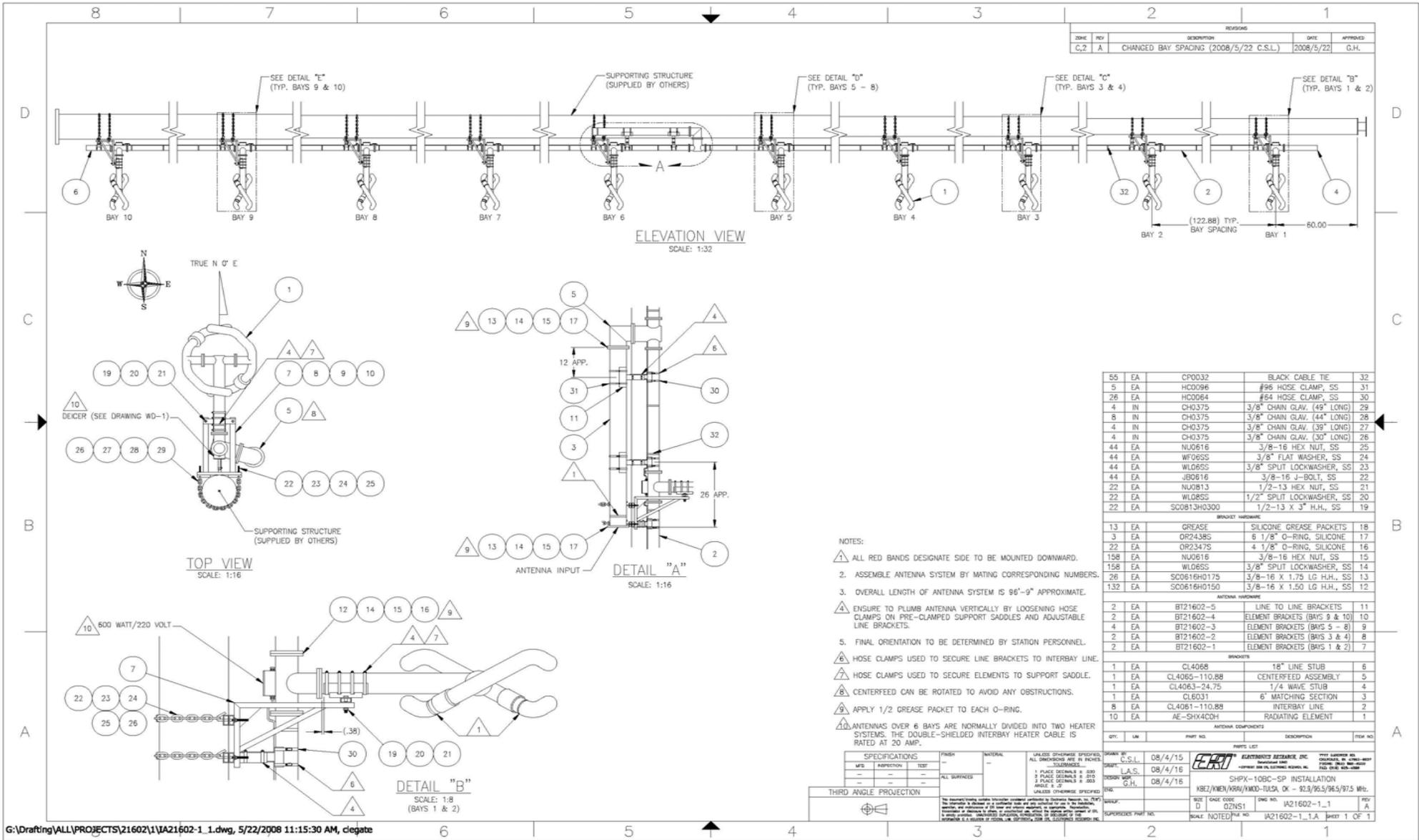
*Subscribed and sworn to before me on this 18th, day of August, 2008.*

Jacquelyn Kinney; Notary Public  
My commission expires July 5, 2015





# EXHIBIT A-1



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**A-2 ERI Antenna Specification Sheet**

Tulsa, Oklahoma

**General Specifications**

Antenna Type.....High Power FM-Broadcast, Suitable For Diplexing  
 Model Number ..... SHPX-10BC-SP  
 Number of Bay ..... Ten  
 Polarization..... Right Hand Circular

**Electrical Specifications**

Antenna Input Power Capability . . . . . 75 KW Max <sup>(1)</sup>  
 Operating Frequency Band..... 95.5, 96.5, & 97.5 Megahertz.  
 VSWR. . . . . <1.04:1 @ Operating Frequencies <sup>(2)</sup>  
 Azimuthal Pattern Circularity ..... Better Than +/- 2dB from RMS (Free Space)  
 Power Split ..... 50/50 ( Horizontal & Vertical )  
 Frequency Specific Information:

<u>Frequency</u>	<u>Station ERP</u>	<u>Beam Tilt</u>	<u>First Null Fill</u>	<u>Second Null Fill</u>	<u>Power Gain</u>	<u>Line Loss</u> <sup>(3)</sup>	<u>Filter Loss</u> <sup>(4)</sup>	<u>Computed TPO</u>
<u>95.5</u>	<u>100 KW</u>	<u>0°</u>	<u>1%</u>	<u>0%</u>	<u>5.684</u>	<u>-.6726 db</u>	<u>-.611 db</u>	<u>23.6 KW</u>
<u>96.5</u>	<u>100 KW</u>	<u>0°</u>	<u>5 %</u>	<u>0%</u>	<u>5.615</u>	<u>-.6726 db</u>	<u>-.523 db</u>	<u>23.4 KW</u>
<u>97.5</u>	<u>100 KW</u>	<u>0°</u>	<u>12%</u>	<u>0%</u>	<u>5.427</u>	<u>-.6726 db</u>	<u>-.509 db</u>	<u>24.1 KW</u>

**Mechanical Specifications**

Antenna Feed System..... Fed With 6 1/8” ERI MACXLine  
 Input Connector ..... 6 1/8”-50 Ohm EIA Flanged  
 Element Deicing ..... Heaters  
 Interbay Spacing..... 122.875” Center to Center  
 Array Length ..... 96’ 9”  
 Construction Material (Antenna) ..... All Noncorrosive  
 Construction Material (Mounting) ..... Stainless Steel

1) Power Capability Has Been Rated Assuming an Operating Transmission VSWR of 1.5:1  
 2) VSWR Specification Achieved After On Site Tuning For User Specific Frequencies.  
 3) Line Loss Assumes A Feed Run of 1431 Feet of 6 1/8 ERI MAXLINE Rigid.  
 4) Losses Taken From Actual Combiner.



**A-4 ERI Combiner Specification Sheet**

Tulsa, Oklahoma

**General Specifications:**

Multiplexer Type 973 Series Constant Impedance with Nonadjacent coupler's and Group Delay  
 Number of Combining Units ..... Three  
 Injected Port to Injected Port Isolation..... < - 56 dB  
 Output Connector ..... 6 1/8 "50 Ohm EIA (Flanged)  
 Output Power (Designed) ..... 28 KW<sup>(1)</sup>

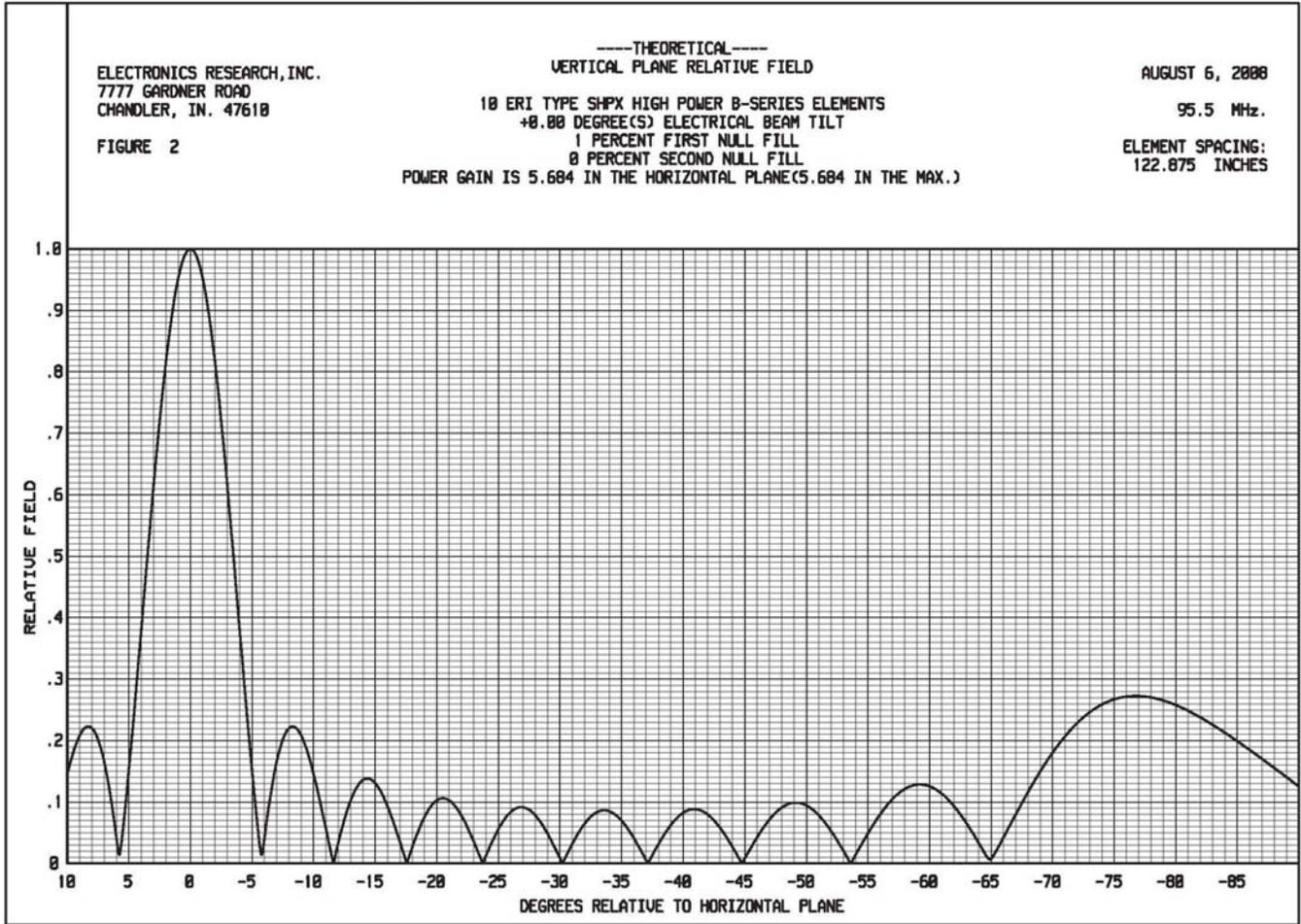
Heat Removal..... Forced Air  
 Physical Arrangement.....All Components floor standing

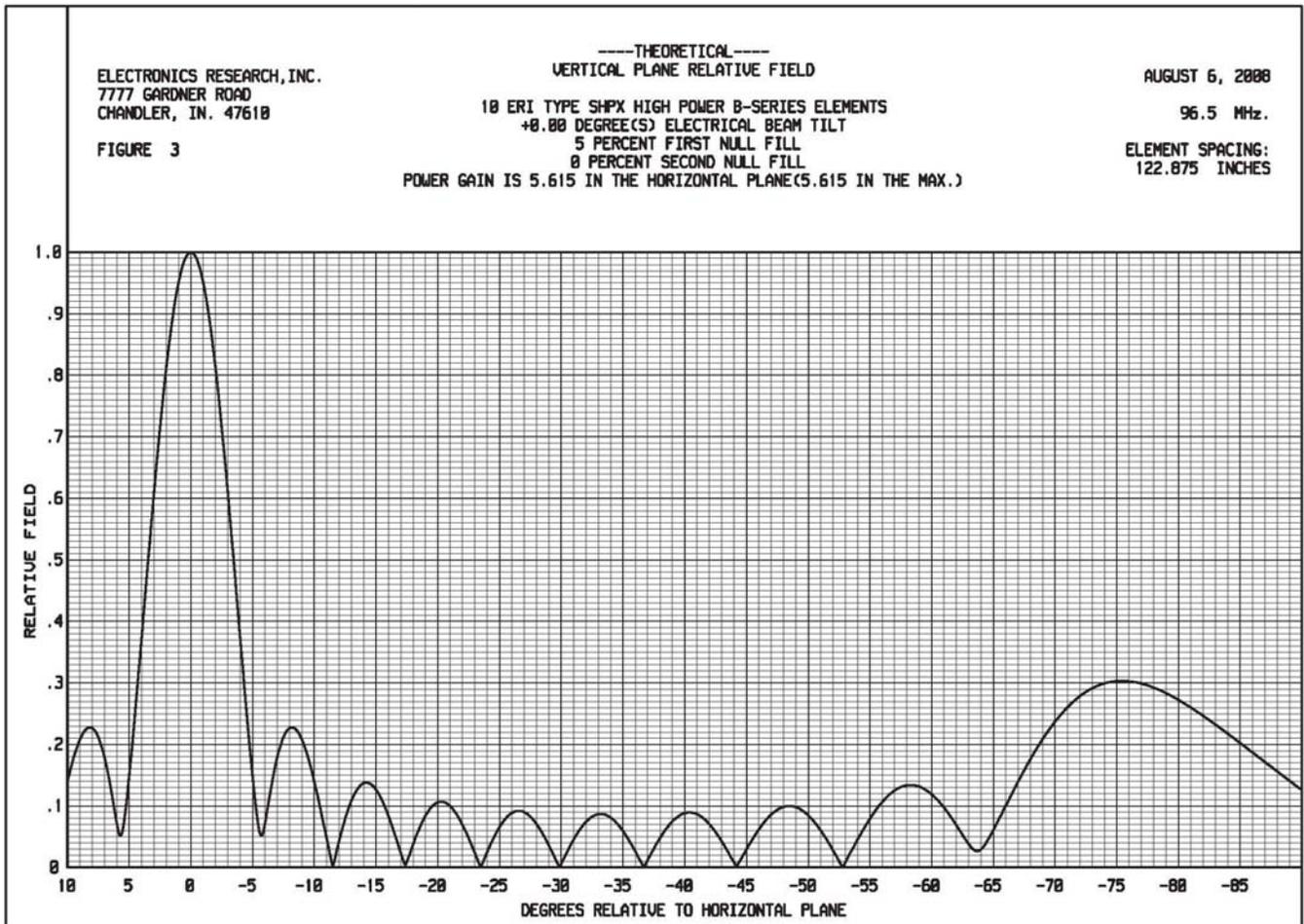
**Injected Port Specifications:**

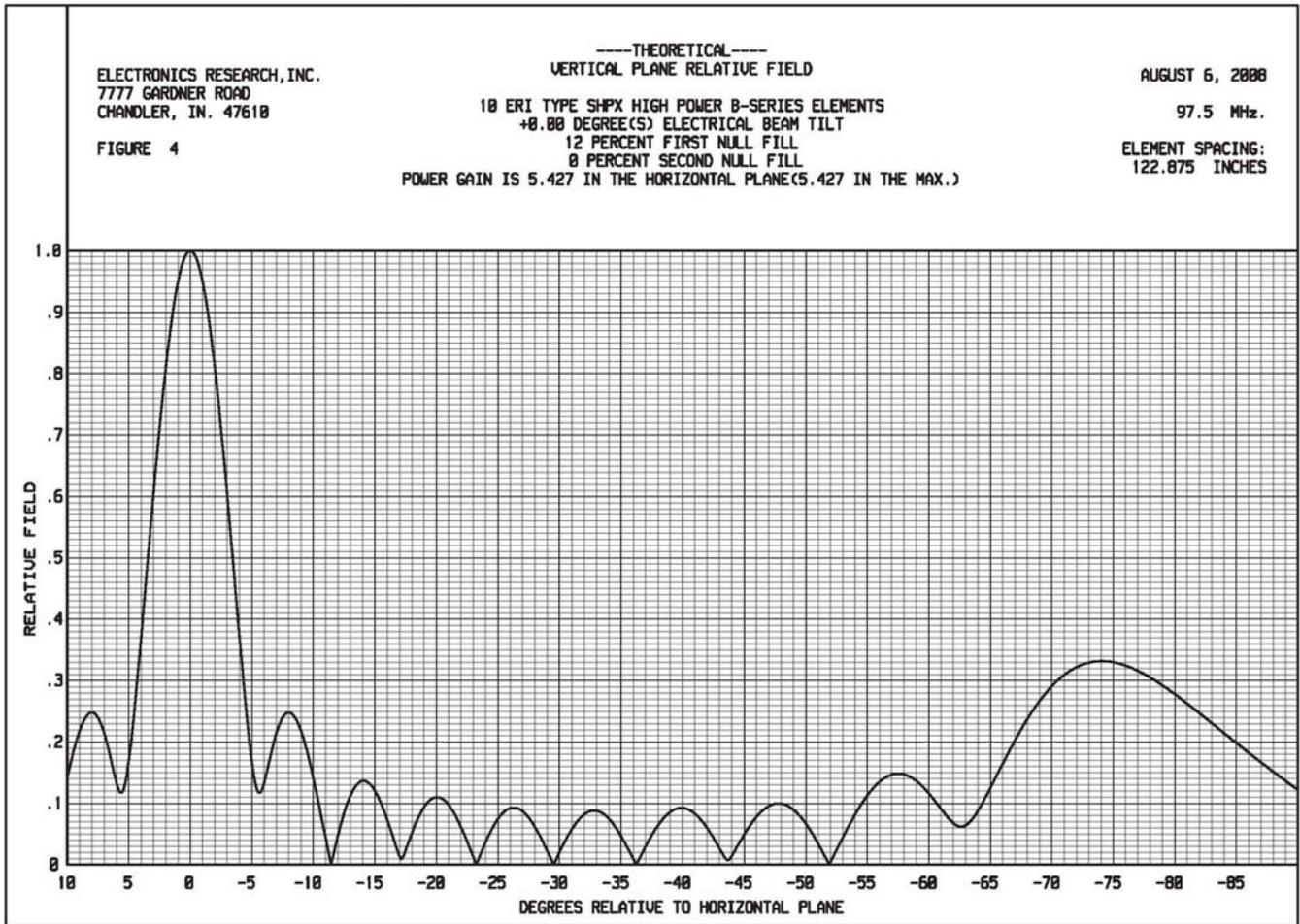
Frequency Assignment ..... 95.5, 96.5, & 97.5 MHz.  
 Power Rating, Each Injected Port (Designed) ..... 25 KW  
 Input Connector ..... 3-1/8" 50 Ohm EIA (Flanged)  
 VSWR..... < 1.08:1 @ +/-150 KHz.<sup>(2)</sup>  
 Group Delay ..... Less than 100ns Overall Variation, Carrier @ +/- 150 KHz.  
 Insertion Loss (Measured):

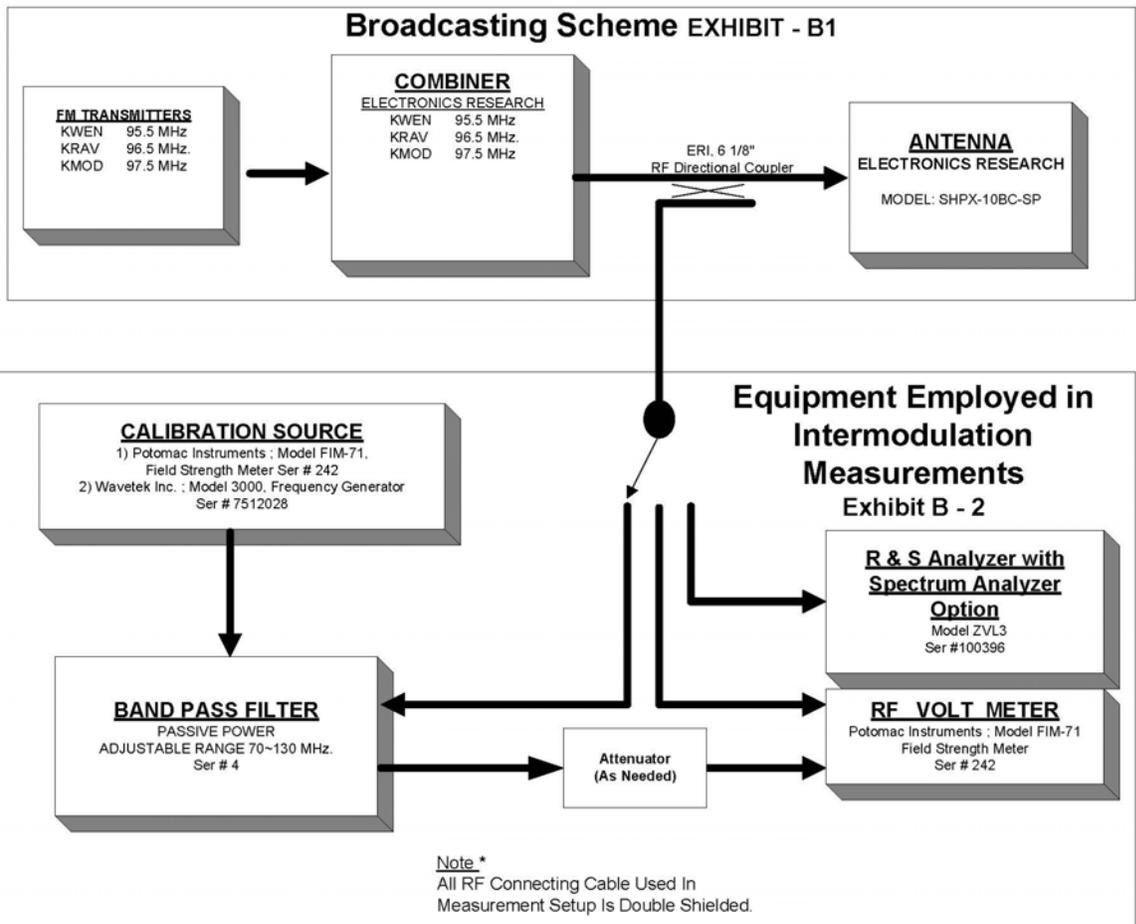
95.5 MHz. .... - 0.611 dB  
 96.5 MHz..... - 0.523 dB  
 97.6 MHz..... -0.509 dB

1) Power Rating Listed is as Designed Only. Actual Power Capabilities May Vary.  
 2) When Terminated in 50 Ohm Resistive Load.









Broadcasting Scheme and Equipment Employed in Intermodulation Measurements

EXHIBIT B