

FOR  
FCC  
USE  
ONLY

**FCC 302-AM**  
**APPLICATION FOR AM**  
**BROADCAST STATION LICENSE**

(Please read instructions before filling out form.)

FOR COMMISSION USE ONLY

FILE NO. *Bmml-20150304ADE*

*Accepted / Filed*

*MAR - 4 2015*

Federal Communications Commission  
Office of the Secretary

<b>SECTION I - APPLICANT FEE INFORMATION</b>			
1. PAYOR NAME (Last, First, Middle Initial) <b>STAR OVER ORLANDO, INC.</b>			
MAILING ADDRESS (Line 1) (Maximum 35 characters) <b>357 OCEAN SHORE BOULEVARD</b>			
MAILING ADDRESS (Line 2) (Maximum 35 characters)			
CITY <b>ORMOND BEACH</b>	STATE OR COUNTRY (if foreign address) <b>FL</b>	ZIP CODE <b>32176</b>	
TELEPHONE NUMBER (include area code) <b>3866722723</b>	CALL LETTERS <b>WRSO</b>	OTHER FCC IDENTIFIER (If applicable) <b>129548</b>	
2. A. Is a fee submitted with this application?		<input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	
B. If No, indicate reason for fee exemption (see 47 C.F.R. Section		* See note below.	
<input type="checkbox"/> Governmental Entity <input type="checkbox"/> Noncommercial educational licensee <input type="checkbox"/> Other (Please explain):			
C. If Yes, provide the following information:			
Enter in Column (A) the correct Fee Type Code for the service you are applying for. Fee Type Codes may be found in the "Mass Media Services Fee Filing Guide." Column (B) lists the Fee Multiple applicable for this application. Enter fee amount due in Column (C).			
(A)	(B)	(C)	
FEE TYPE CODE	FEE MULTIPLE	FEE DUE FOR FEE TYPE CODE IN COLUMN (A)	FOR FCC USE ONLY
<b>M M R</b>	<b>0 0 0 1</b>	<b>\$ 690.00</b>	
To be used only when you are requesting concurrent actions which result in a requirement to list more than one Fee Type Code.			
(A)	(B)	(C)	
		\$	FOR FCC USE ONLY
<b> </b>	<b>0 0 0 1</b>	<b> </b>	
ADD ALL AMOUNTS SHOWN IN COLUMN C, AND ENTER THE TOTAL HERE. THIS AMOUNT SHOULD EQUAL YOUR ENCLOSED REMITTANCE.		TOTAL AMOUNT REMITTED WITH THIS APPLICATION	FOR FCC USE ONLY
		<b>\$ 690.00</b>	

\* The fee for this application has been submitted electronically through the Commission's Fee Filer service. The Form 159 filing receipt is attached hereto.

SECTION II - APPLICANT INFORMATION		
1. NAME OF APPLICANT STAR OVER ORLANDO, INC.		
MAILING ADDRESS 357 OCEAN SHORE BOULEVARD		
CITY ORMOND BEACH	STATE FL	ZIP CODE 32176

2. This application is for:

- Commercial       Noncommercial  
 AM Directional       AM Non-Directional

Call letters WRSO	Community of License Orlando	Construction Permit File No. BMP-20140211ACI	Modification of Construction Permit File No(s).	Expiration Date of Last Construction Permit 09/11/2016
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3. Is the station now operating pursuant to automatic program test authority in accordance with 47 C.F.R. Section 73.1620?

Yes  No

If No, explain in an Exhibit.

Exhibit No.  
A

4. Have all the terms, conditions, and obligations set forth in the above described construction permit been fully met?

Yes  No

If No, state exceptions in an Exhibit.

Exhibit No.

5. Apart from the changes already reported, has any cause or circumstance arisen since the grant of the underlying construction permit which would result in any statement or representation contained in the construction permit application to be now incorrect?

Yes  No

If Yes, explain in an Exhibit.

Exhibit No.

6. Has the permittee filed its Ownership Report (FCC Form 323) or ownership certification in accordance with 47 C.F.R. Section 73.3615(b)?

Yes  No

If No, explain in an Exhibit.

Does not apply

Exhibit No.

7. Has an adverse finding been made or an adverse final action been taken by any court or administrative body with respect to the applicant or parties to the application in a civil or criminal proceeding, brought under the provisions of any law relating to the following: any felony; mass media related antitrust or unfair competition; fraudulent statements to another governmental unit; or discrimination?

Yes  No

If the answer is Yes, attach as an Exhibit a full disclosure of the persons and matters involved, including an identification of the court or administrative body and the proceeding (by dates and file numbers), and the disposition of the litigation. Where the requisite information has been earlier disclosed in connection with another application or as required by 47 U.S.C. Section 1.65(c), the applicant need only provide: (i) an identification of that previous submission by reference to the file number in the case of an application, the call letters of the station regarding which the application or Section 1.65 information was filed, and the date of filing; and (ii) the disposition of the previously reported matter.

Exhibit No.

8. Does the applicant, or any party to the application, have a petition on file to migrate to the expanded band (1605-1705 kHz) or a permit or license either in the existing band or expanded band that is held in combination (pursuant to the 5 year holding period allowed) with the AM facility proposed to be modified herein?

Yes  No

If Yes, provide particulars as an Exhibit.

Exhibit No.

The APPLICANT hereby waives any claim to the use of any particular frequency or of the electromagnetic spectrum as against the regulatory power of the United States because use of the same, whether by license or otherwise, and requests and authorization in accordance with this application. (See Section 304 of the Communications Act of 1934, as amended).

The APPLICANT acknowledges that all the statements made in this application and attached exhibits are considered material representations and that all the exhibits are a material part hereof and are incorporated herein as set out in full in

**CERTIFICATION**

1. By checking Yes, the applicant certifies, that, in the case of an individual applicant, he or she is not subject to a denial of federal benefits that includes FCC benefits pursuant to Section 5301 of the Anti-Drug Abuse Act of 1988, 21 U.S.C. Section 862, or, in the case of a non-individual applicant (e.g., corporation, partnership or other unincorporated association), no party to the application is subject to a denial of federal benefits that includes FCC benefits pursuant to that section. For the definition of a "party" for these purposes, see 47 C.F.R. Section 1.2002(b).

Yes  No

2. I certify that the statements in this application are true, complete, and correct to the best of my knowledge and belief, and are made in good faith.

Name <b>CARL TUTERA</b>	Signature <i>Carl Tutera</i>	
Title <b>PRESIDENT</b>	Date <b>02/25/2015</b>	Telephone Number <b>3866722723</b>

**WILLFUL FALSE STATEMENTS ON THIS FORM ARE PUNISHABLE BY FINE AND/OR IMPRISONMENT (U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION**

**FCC NOTICE TO INDIVIDUALS REQUIRED BY THE PRIVACY ACT AND THE PAPERWORK REDUCTION ACT**

The solicitation of personal information requested in this application is authorized by the Communications Act of 1934, as amended. The Commission will use the information provided in this form to determine whether grant of the application is in the public interest. In reaching that determination, or for law enforcement purposes, it may become necessary to refer personal information contained in this form to another government agency. In addition, all information provided in this form will be available for public inspection. If information requested on the form is not provided, the application may be returned without action having been taken upon it or its processing may be delayed while a request is made to provide the missing information. Your response is required to obtain the requested authorization.

Public reporting burden for this collection of information is estimated to average 639 hours and 53 minutes per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, can be sent to the Federal Communications Commission, Records Management Branch, Paperwork Reduction Project (3060-0627), Washington, D. C. 20554. Do NOT send completed forms to this address.

THE FOREGOING NOTICE IS REQUIRED BY THE PRIVACY ACT OF 1974, P.L. 93-579, DECEMBER 31, 1974, 5 U.S.C. 552a(e)(3), AND THE PAPERWORK REDUCTION ACT OF 1980, P.L. 96-511, DECEMBER 11, 1980, 44 U.S.C. 3507.

EXHIBIT A  
APPLICATION FOR LICENSE INFORMATION  
EMPLOYING MOMENT METHOD MODELING  
WRSO(AM), 810 KHZ, DA-2, ORLOVISTA, FLORIDA

Pursuant to the terms of the underlying construction permit, the station must request program test authority prior to beginning such tests. See Special Operating Conditions, No. 1, FCC File No. BMP-20140211ACD.



**SECTION III - Page 2**

9. Description of antenna system ((f directional antenna is used, the information requested below should be given for each element of the array. Use separate sheets if necessary.)

Type Radiator <b>Guyed Tower</b>	Overall height in meters of radiator above base insulator, or above base, if grounded. <b>92.53</b>	Overall height in meters above ground (without obstruction lighting) <b>93.0</b>	Overall height in meters above ground (include obstruction lighting) <b>94.2</b>	If antenna is either top loaded or sectionalized, describe fully in an Exhibit. <div style="border: 1px solid black; padding: 2px;">Exhibit No. <b>N/A</b></div>
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Excitation  Series  Shunt

Geographic coordinates to nearest second. For directional antenna give coordinates of center of array. For single vertical radiator give tower location.

North Latitude <b>28</b> ° <b>34</b> ' <b>18</b> "	West Longitude <b>81</b> ° <b>26</b> ' <b>02</b> "
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If not fully described above, attach as an Exhibit further details and dimensions including any other antenna mounted on tower and associated isolation circuits.

Exhibit No.  
**ENG**

Also, if necessary for a complete description, attach as an Exhibit a sketch of the details and dimensions of ground system.

Exhibit No.  
**ENG**

10. In what respect, if any, does the apparatus constructed differ from that described in the application for construction permit or in the permit?

**No Change from Construction Permit**

11. Give reasons for the change in antenna or common point resistance.

**New Adjustment**

I certify that I represent the applicant in the capacity indicated below and that I have examined the foregoing statement of technical information and that it is true to the best of my knowledge and belief.

Name (Please Print or Type) <b>Kurt Gorman</b>	Signature (check appropriate box below) 
Address (include ZIP Code) <b>Phasetek Inc.</b> <b>550 California Rd., Unit 11</b> <b>Quakertown, PA 18951</b>	Date <b>February 23, 2015</b>
	Telephone No. (Include Area Code) <b>215-536-6648</b>

Technical Director

Registered Professional Engineer

Chief Operator

Technical Consultant

Other (specify)

**ENGINEERING STATEMENT CONCERNING**

**APPLICATION FOR LICENSE INFORMATION**

**EMPLOYING MOMENT METHOD MODELING**

**WRSO, 810 KHZ, DA-2**

**ORLOVISTA, FLORIDA**

**FEBRUARY, 2015**

***PHASETEK INC.***  
**ENGINEERING STATEMENT CONCERNING  
APPLICATION FOR LICENSE INFORMATION  
EMPLOYING MOMENT METHOD MODELING  
WRSO, 810 KHZ, DA-2  
ORLOVISTA, FLORIDA  
FEBRUARY, 2015**

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# ***PHASETEK INC.***

## **ENGINEERING STATEMENT CONCERNING APPLICATION FOR LICENSE INFORMATION EMPLOYING MOMENT METHOD MODELING WRSO, 810 KHZ, DA-2 ORLOVISTA, FLORIDA FEBRUARY, 2015**

### **SUMMARY**

Adjustment of the Antenna System and a Proof of Performance employing Moment Method Modeling were performed on Radio Station WRSO, 810 KHz, Orlovista, Florida, after modification of Antenna Phasing equipment. The existing transmission and sampling lines were utilized. WRSO holds Construction Permit Number: BMP-20140211ACD to increase Day power and change Day radiation pattern. The Night radiation pattern remains as licensed. This report was prepared on behalf of Star Over Orlando, Inc. licensee of Radio Station WRSO.

### **SITE MODIFICATIONS**

The WRSO Transmitter site is that as currently licensed. The Day Antenna Phasing and Branching equipment has been modified. All Towers remain unchanged. A License Application employing Moment Method Modeling as set forth in Section 73.151(C) has been done to cover the Radio Station WRSO Construction Permit and license under the new rules.

### **REFERENCE POINTS**

Reference Points were measured at pattern minima and maxima for the Directional modes of operation. These Points and their measured field intensity are shown in Figure 15.

### **SPECIAL OPERATING CONDITION #6**

No new tower construction has been done at the WRSO transmitter site. All towers and grounding remain as previously licensed. Therefore, implementation of the WRSO construction permit has not adversely affected AM stations WDYZ, 990 kHz or WRLZ, 1270 kHz. WHOO, 1080 kHz operates from a licensed site that is more than 5 km from the WRSO site. Verification of no spurious products from the above stations was performed.

# ***PHASETEK INC.***

## **ENGINEERING STATEMENT CONCERNING APPLICATION FOR LICENSE INFORMATION EMPLOYING MOMENT METHOD MODELING WRSO, 810 KHZ, DA-2 ORLOVISTA, FLORIDA FEBRUARY, 2015**

### **METHOD OF MOMENTS DETAIL**

All Moment Method Modeling was done with Expert MININEC Broadcast Professional, Version 23. One wire was used to represent each Tower. Towers were driven individually to verify the Model compared to measured impedance data. Once the Model was verified, both the Day and Night Directional Antenna Systems were computed. For Directional modes, the complex voltage values for sources located at ground level were computed. These sources produce current moment sums for each Tower that, when normalized, equate to the Theoretical Field Parameters for each respective Tower.

### **MEASURING EQUIPMENT AND PERSONNEL**

All Tower Resistance and Reactance measurements were made with a Delta Electronics OIB-3 Operating Impedance Bridge. Before use, tests of known impedances were made to verify operation. All Field Intensity Measurements were made with two Potomac Instruments Field Intensity Meters: An FIM-41, Serial Number 2181, calibrated on October 9, 2009 and another FIM-41, Serial Number 643, calibrated July 3, 2003. Both meters were calibrated by Potomac Instruments, Silver Spring, Maryland. Both meters were also compared to a Potomac Instruments FIM-21, serial number 901, calibrated August 29, 2012 by Potomac Instruments and agreed within tolerance. All measurements were taken by Phasetek Inc. personnel supervised by Kurt Gorman of Phasetek Inc.

### **CONCLUSION**

It is believed that the WRSO Antenna System has been constructed and adjusted in accordance with all applicable Commission rules and regulations. The foregoing was prepared on behalf of Star Over Orlando, Inc., under the immediate supervision of Kurt Gorman, Phasetek Inc., Quakertown, Pennsylvania, whose qualifications are a matter of record with the Federal Communications Commission. The statements herein are true and correct of his knowledge, except such statements made on information and belief, and as to these statements he believes them to be true and correct.

***PHASETEK INC.***

**ENGINEERING STATEMENT CONCERNING  
APPLICATION FOR LICENSE INFORMATION  
EMPLOYING MOMENT METHOD MODELING  
WRSO, 810 KHZ, DA-2  
ORLOVISTA, FLORIDA  
FEBRUARY, 2015**



---

**Kurt Gorman, President  
Phasetek Inc.  
Quakertown, Pennsylvania**

## FIGURE 1

### ANTENNA SYSTEM AS ADJUSTED

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EMPLOYING MOMENT METHOD MODELING  
WRSO, 810 KHZ, DA-2  
ORLOVISTA, FLORIDA  
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#### ANTENNA SYSTEM DESCRIPTION

1. The Antenna System consists of four (4), uniform, guyed, vertical steel transmitting Towers. All Towers stand 92.53M (90.0°) above their Base Insulators. The Towers are arranged with Tower 1 as a reference; Tower 2 is spaced 90.0° on a bearing of 81.6°T. Tower 3 is spaced 225.0° on a bearing of 7.0°T. Tower 4 is spaced 208.1° on a bearing of 343.4°T. Tower 2 supports an FM translator antenna and a STL antenna. Both feeds for these Antennas are isolated at the base with Isocouplers. All towers have aviation obstruction lighting. The lighting circuits are isolated at the base with a choke for each tower.
2. The Ground System for each Tower consists of (120) buried copper Radials, 92.5M in length, except where they intersect with copper transverse straps between Towers or property boundaries. Copper strap connects all Towers to the main Transmitter grounding point.
3. The Sampling System consists of four (4), Delta Electronics TCT-3, 1.0 V/A Toroidal Current Transformers. All TCT's are at the Output of each Antenna Tuning Unit. These TCT's are connected to a Potomac Instruments 1901-4 Antenna Monitor via four (4) equal lengths of Andrew, LDF2-50, 3/8" phase stabilized foam coaxial cable.
4. Tower registration numbers:  
Tower 1: 1247871  
Tower 2: 1247872  
Tower 3: 1247873  
Tower 4: 1247874

**FIGURE 1  
ANTENNA SYSTEM AS ADJUSTED**

**APPLICATION FOR LICENSE INFORMATION  
EMPLOYING MOMENT METHOD MODELING  
CONTINUED**

**WRSO, 810 KHZ, DA-2  
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**ANTENNA SYSTEM DESCRIPTION – Continued**

**DIRECTIONAL OPERATION (DAY)**

**COMMON POINT**

Impedance = 50.0 – j 8.1 Ohms  
Current = 20.5 Amperes  
Power = 21,060 Watts

**DIRECTIONAL OPERATION (NIGHT)**

**COMMON POINT**

Impedance = 50.0 – j 8.1 Ohms  
Current = 2.94 Amperes  
Power = 432 Watts

Directional Antenna Monitor indications are within  $\pm 5\%$  and  $\pm 3^\circ$  of the modeled TCT values.

**FIGURE 2**  
**WRSO SAMPLING SYSTEM DESCRIPTION/MEASUREMENTS**

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**WRSO, 810 KHZ, DA-2**  
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**SAMPLING SYSTEM DESCRIPTION**

The Sampling System consists of Delta Electronics TCT-3 Toroidal Sampling Transformers (1.0 volt/amp) mounted at the base of each Tower. The sampling devices are connected to the Antenna Monitor with equal lengths of Andrew LDF2-50. The Antenna Monitor is a Potomac Instruments Model 1901-4, Serial Number 653.

**SAMPLE LINE MEASUREMENTS**

Impedance measurements were made of the Antenna Sampling Lines using an Array Solutions 2180 Vector Network Analyzer (VNA). Measurements were done with the lines open circuited and then connected to the TCT's.

The table below shows the frequencies above and below the carrier frequency where resonance, defined as zero reactance corresponding with low resistance, was found. Frequencies of resonance occur at odd multiples of 90 degrees electrical length, the Sample Line length at the resonant frequency above the carrier frequency, which is the closest one to the carrier frequency, was found to be 450 electrical degrees. The electrical length at carrier frequency appearing in the table below was calculated by ratioing the frequencies.

**SAMPLE LINE MEASUREMENTS**

	<b>Resonant Frequency (KHz) below 810 KHz</b>	<b>Resonant Frequency (KHz) above 810 KHz</b>	<b>Calculated Electrical Length (deg) at 810 KHz</b>	<b>Measured Impedance (ohms) Connected to TCT @ 810 KHz</b>
<b>Tower 1</b>	552.459	924.855	394.1	52.45 +j 0.25
<b>Tower 2</b>	552.443	924.877	394.1	52.07 +j 0.37
<b>Tower 3</b>	552.430	924.876	394.1	51.81 -j 0.71
<b>Tower 4</b>	552.428	924.777	394.1	51.48 -j 0.52

**FIGURE 2**  
**WSRF SAMPLING SYSTEM DESCRIPTION/MEASUREMENTS**

**APPLICATION FOR LICENSE INFORMATION**  
**EMPLOYING MOMENT METHOD MODELING**  
**CONTINUED**

**WRSO, 810 KHZ, DA-2**  
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**SAMPLE LINE MEASUREMENTS (CONTINUED)**

To determine the characteristic impedance values of the Sample Lines, open-circuited measurements were made with frequencies offset to produce  $\pm 45$  degrees of electrical length from resonance. The characteristic impedance was calculated using the following formula, where  $R_1 + j X_1$  and  $R_2 + j X_2$  are the measured impedances at the +45 and -45 degree offset frequencies, respectively:

$$Z_0 = ((R_1^2 + X_1^2)^{1/2} \cdot (R_2^2 + X_2^2)^{1/2})^{1/2}$$

Tower	+ 45 Degree Offset Frequency (kHz)	+ 45 Degree Measured Impedance (Ohms)	- 45 Degree Offset Frequency (kHz)	- 45 Degree Measured Impedance (Ohms)	Calculated Characteristic Impedance (Ohms)
1	1017.3	9.9 +j 48.6	832.4	9.2 -j 48.4	49.43
2	1017.4	9.9 +j 48.5	832.4	9.1 -j 48.4	49.37
3	1017.4	9.8 +j 48.6	832.4	9.2 -j 48.5	49.47
4	1017.3	9.7 +j 48.7	832.3	9.0 -j 48.5	49.49

**SAMPLING TCT MEASUREMENTS**

Measurements of the Delta Electronics Model TCT-3, 1.0 V/A Toroidal Current Transformers were performed by a Hewlett Packard 8752A, Network Analyzer. Measurements are normalized to Tower #2 (reference) and are within the manufacturer's rating of  $\pm 2.0\%$  and  $\pm 3.0^\circ$ .

**FIGURE 2**  
**WSRF SAMPLING SYSTEM DESCRIPTION/MEASUREMENTS**

**APPLICATION FOR LICENSE INFORMATION**  
**EMPLOYING MOMENT METHOD MODELING**  
**CONTINUED**

**WRSO, 810 KHZ, DA-2**  
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**SAMPLING TCT MEASUREMENTS CONT'D**

<b>TOWER</b>	<b>TCT SERIAL #</b>	<b>MAGNITUDE</b>	<b>PHASE</b>
1	17304	1.000	0.1 <sup>o</sup>
2	17307	1.000	0.0 <sup>o</sup>
3	17308	1.001	0.0 <sup>o</sup>
4	17309	1.002	-0.1 <sup>o</sup>

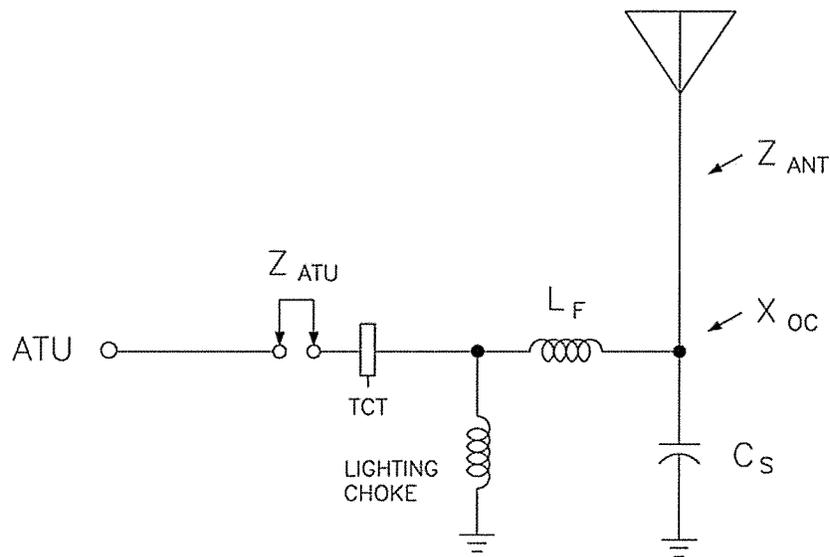
**ANTENNA MONITOR MEASUREMENT**

Measurement of the Potomac Instruments Model 1901-4 Antenna Monitor was performed to verify calibration. A single RF Voltage was applied to the Reference Input (Tower #2) and each other Input by use of a "T" divider and equal electrical length coaxial cables. This yields the following:

<b>Tower</b>	<b>Ratio</b>	<b>Phase</b>
1	1.000	0.4 <sup>o</sup>
2	1.000	0.0 <sup>o</sup>
3	1.000	0.2 <sup>o</sup>
4	1.000	0.3 <sup>o</sup>

The above is within the manufacturer's rating of  $\pm 1.0\%$  and  $\pm 1.0^{\circ}$ .

**FIGURE 3**  
**WRSO TOWER IMPEDANCE MEASUREMENTS COMPARED TO**  
**METHOD OF MOMENTS MODEL**  
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TOWER	Specified $C_s$ (pf)	Measured $L_F$ ( $\mu$ H)	Measured $X_F$ ( $\Omega$ )	Modeled $Z_{ANT}$ ( $\Omega$ )	Modeled $Z_{ATU}$ ( $\Omega$ )	Measured $Z_{ATU}$ ( $\Omega$ )
1	15	3.93	+j20.0	51.0 +j 55.4	49.2 +j 74.5	49.0 +j 76.0
2	45	5.11	+j26.0	49.9 +j 52.3	48.7 +j 77.3	48.0 +j 78.6
3	15	4.13	+j21.0	51.0 +j 55.2	49.2 +j 75.3	49.5 +j 76.8
4	15	3.93	+j20.0	50.9 +j 55.3	49.1 +j 74.5	49.9 +j 75.1

Tower	Calculated $X_{OC}$ ( $\Omega$ )
1	+j 4,537.3
2	+j 14,883.9
3	+j 4,539.1
4	+j 4,537.3

**FIGURE 4  
WRSO MOMENT MODEL PARAMETERS**

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<b>Tower #</b>	<b>Wire #</b>	<b># of Segments</b>	<b>Base Node</b>
1	1	10	1
2	2	10	11
3	3	10	21
4	4	10	31

<b>Tower #</b>	<b>Physical Height Degrees</b>	<b>Modeled Height Degrees</b>	<b>Modeled Radius Meters</b>	<b>% of Equivalent Radius</b>
1	90.0	96.5	.243	100.0
2	90.0	96.0	.243	100.0
3	90.0	96.5	.243	100.0
4	90.0	96.5	.243	100.0

All Towers are uniform cross section, guyed with Base Insulator. All towers are three (3) sided, 20" face width.

All Base Insulators are manufactured by Austin Insulators, part number A-4197L, with an assumed capacity of 15pf (-j13,099.2 ohms @ 810 kHz). Tower #2 FM Isocoupler is Phasetek Inc. Model #P600-407 with a capacity of 20pf (-j9,824.4 ohms @ 810 kHz). Tower #2 STL isocoupler is a Moseley Model #ICU-1D with a capacity of 10pF (-j19,648.8 ohms @ 810 kHz).

All Towers have Kintronic Labs 3 wire lighting choke. These measure +j3,350 ohms @ 810 kHz.

**FIGURE 5**  
**WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS**

**APPLICATION FOR LICENSE INFORMATION**  
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WRSO TOWER 1 (OTHERS OPEN)

GEOMETRY

Wire coordinates in degrees; other dimensions in meters  
 Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4  
 current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency	step	no. of steps	segment length (wavelengths)
	lowest			minimum maximum
1	.81	0	1	.0266667 .0268056

Sources

source	node	sector	magnitude	phase	type
1	1	1	1.	0	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	11	0	14,883.9	0	0	0
2	21	0	4,539.1	0	0	0
3	31	0	4,537.3	0	0	0

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = .81	1; 51.	node 1, 55.39	sector 1, 75.294	47.4	2.8531	-6.3583	-1.1424

**FIGURE 5**  
**WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS**

WRSO TOWER 2 (OTHERS OPEN)

GEOMETRY

Wire coordinates in degrees; other dimensions in meters  
Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4  
current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	11	1	1.	0	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	1	0	4,537.3	0	0	0
2	21	0	4,539.1	0	0	0
3	31	0	4,537.3	0	0	0

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = .81	1; node 49.848	11, sector 52.312	1, 72.259	46.4	2.7319	-6.6681	-1.0534

## FIGURE 5 WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS

WRSO TOWER 3 (OTHERS OPEN)

### GEOMETRY

Wire coordinates in degrees; other dimensions in meters  
Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4  
current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

### ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

### Sources

source	node	sector	magnitude	phase	type
1	21	1	1.	0	voltage

### Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	1	0	4,537.3	0	0	0
2	11	0	14,883.9	0	0	0
3	31	0	4,537.3	0	0	0

### IMPEDANCE

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = .81	1; node 51.04	21, sector 55.237	1, 75.208	47.3	2.8444	-6.3794	-1.1361

## FIGURE 5 WRSO MOMENT SUMMARY FOR INDIVIDUAL TOWERS

WRSO TOWER 4 (OTHERS OPEN)

### GEOMETRY

Wire coordinates in degrees; other dimensions in meters  
Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4  
current nodes = 40

Individual wires	minimum		maximum	
	wire	value	wire	value
segment length	2	9.6	1	9.65
radius	1	.243	1	.243

### ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency		no. of steps	segment length (wavelengths)	
	lowest	step		minimum	maximum
1	.81	0	1	.0266667	.0268056

### Sources

source	node	sector	magnitude	phase	type
1	31	1	1.	0	voltage

### Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	1	0	4,537.3	0	0	0
2	11	0	14,883.9	0	0	0
3	21	0	4,539.1	0	0	0

### IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node .81	50.943	55.333	75.213	47.4	2.8517	-6.3616	-1.1414

**FIGURE 6**  
**WRSO MOMENT MODEL ARRAY SYNTHESIS**  
**(DIRECTIONAL – DAY)**

**APPLICATION FOR LICENSE INFORMATION**  
**EMPLOYING MOMENT METHOD MODELING**  
**WRSO, 810 KHZ, DA-2**  
**ORLOVISTA, FLORIDA**  
**FEBRUARY, 2015**

WRSO DAY

MEDIUM WAVE ARRAY SYNTHESIS FROM FIELD RATIOS

Frequency = .81 MHz

tower	field ratio magnitude	phase (deg)
1	1.	0
2	.931	-99.8
3	.744	-101.
4	.68	-11.3

VOLTAGES AND CURRENTS - rms

source node	voltage magnitude	phase (deg)	current magnitude	phase (deg)
1	666.332	74.8	14.3908	1.4
11	1,131.51	314.2	12.9567	265.5
21	828.243	301.5	10.6227	264.9
31	313.52	69.4	10.012	349.3

Sum of square of source currents = 1,176.11

Total power = 20,000. watts

TOWER ADMITTANCE MATRIX

admittance	real (mhos)	imaginary (mhos)
Y(1, 1)	.00871243	-.00882986
Y(1, 2)	.00496811	.00269084
Y(1, 3)	.00272785	-.00149079
Y(1, 4)	.00332803	-.00202396
Y(2, 1)	.00496807	.00269091
Y(2, 2)	.00865981	-.00902374
Y(2, 3)	.00278277	-.00215183
Y(2, 4)	.0020943	-.00141139
Y(3, 1)	.00272784	-.00149078
Y(3, 2)	.00278277	-.00215185
Y(3, 3)	.00848884	-.00890128
Y(3, 4)	.00491857	.0025569
Y(4, 1)	.00332803	-.00202395
Y(4, 2)	.0020943	-.00141141
Y(4, 3)	.00491857	.0025569
Y(4, 4)	.00852187	-.00877838

TOWER IMPEDANCE MATRIX

impedance	real (ohms)	imaginary (ohms)
Z(1, 1)	51.0064	55.2755
Z(1, 2)	25.7748	-24.7706
Z(1, 3)	-18.1711	-3.06078
Z(1, 4)	-16.5232	-8.91811
Z(2, 1)	25.7744	-24.7709
Z(2, 2)	49.6066	52.1707
Z(2, 3)	-17.189	-5.32849
Z(2, 4)	-17.8057	1.08107

**FIGURE 6**  
**WRSO MOMENT MODEL ARRAY SYNTHESIS**  
**(DIRECTIONAL – DAY)**

Z(3, 1)	-18.171	-3.06079
Z(3, 2)	-17.189	-5.32855
Z(3, 3)	50.7966	55.1332
Z(3, 4)	25.9233	-25.0164
Z(4, 1)	-16.5232	-8.91811
Z(4, 2)	-17.8056	1.081
Z(4, 3)	25.9233	-25.0164
Z(4, 4)	50.7251	55.2564

**FIGURE 7**  
**WRSO MOMENT MODEL SUMMARY FOR**  
**DIRECTIONAL DAY MODE**

**APPLICATION FOR LICENSE INFORMATION**  
**EMPLOYING MOMENT METHOD MODELING**  
**WRSO, 810 KHZ, DA-2**  
**ORLOVISTA, FLORIDA**  
**FEBRUARY, 2015**

WRSO DAY

GEOMETRY

Wire coordinates in degrees; other dimensions in meters  
 Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4  
 current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency	step	no. of steps	segment length (wavelengths) minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	1	1	942.336	74.8	voltage
2	11	1	1,600.19	314.2	voltage
3	21	1	1,171.31	301.5	voltage
4	31	1	443.384	69.4	voltage

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node 1, sector 1							
.81	13.16	44.393	46.303	73.5	6.9132	-2.5306	-3.5497
source = 2; node 11, sector 1							
.81	57.597	65.643	87.33	48.7	3.2042	-5.6086	-1.3959
source = 3; node 21, sector 1							
.81	62.626	46.445	77.969	36.6	2.3062	-8.0665	-.737
source = 4; node 31, sector 1							
.81	5.3731	30.85	31.314	80.1	12.878	-1.3517	-5.7274

**FIGURE 7**  
**WRSO MOMENT MODEL SUMMARY FOR**  
**DIRECTIONAL DAY MODE**

CURRENT rms  
 Frequency = .81 MHz  
 Input power = 20,000. watts  
 Efficiency = 100. %  
 coordinates in degrees

no.	X	Y	Z	mag (amps)	phase (deg)	real (amps)	imaginary (amps)
GND	0	0	0	14.3908	1.4	14.3868	.340922
2	0	0	9.65	14.7135	.8	14.7121	.202131
3	0	0	19.3	14.5145	.4	14.5141	.10502
4	0	0	28.95	13.8928	.1	13.8927	.0264191
5	0	0	38.6	12.8779	359.8	12.8778	-.0355023
6	0	0	48.25	11.4992	359.6	11.4989	-.0803309
7	0	0	57.9	9.78984	359.4	9.78926	-.107014
8	0	0	67.55	7.78531	359.2	7.78447	-.114348
9	0	0	77.2	5.51781	359.	5.51688	-.101099
10	0	0	86.85	2.9972	358.7	2.99649	-.0656428
END	0	0	96.5	0	0	0	0
GND	13.1475	-89.0345	0	12.9567	265.5	-1.02345	-12.9162
12	13.1475	-89.0345	9.6	13.4673	263.	-1.63043	-13.3682
13	13.1475	-89.0345	19.2	13.4336	261.6	-1.97168	-13.2881
14	13.1475	-89.0345	28.8	12.9755	260.4	-2.15967	-12.7945
15	13.1475	-89.0345	38.4	12.1214	259.5	-2.21057	-11.9181
16	13.1475	-89.0345	48.	10.8978	258.7	-2.13273	-10.6871
17	13.1475	-89.0345	57.6	9.33466	258.	-1.93352	-9.13221
18	13.1475	-89.0345	67.2	7.46468	257.5	-1.62078	-7.28659
19	13.1475	-89.0345	76.8	5.31777	256.9	-1.20195	-5.18015
20	13.1475	-89.0345	86.4	2.90268	256.5	-.6796	-2.822
END	13.1475	-89.0345	96.	0	0	0	0
GND	223.323	-27.4206	0	10.6227	264.9	-.938196	-10.5812
22	223.323	-27.4206	9.65	10.8886	262.3	-1.46813	-10.7892
23	223.323	-27.4206	19.3	10.7693	260.6	-1.76492	-10.6236
24	223.323	-27.4206	28.95	10.3339	259.3	-1.92665	-10.1527
25	223.323	-27.4206	38.6	9.60155	258.2	-1.9675	-9.3978
26	223.323	-27.4206	48.25	8.59224	257.3	-1.89486	-8.3807
27	223.323	-27.4206	57.9	7.32948	256.5	-1.71532	-7.12594
28	223.323	-27.4206	67.55	5.83915	255.8	-1.43594	-5.65983
29	223.323	-27.4206	77.2	4.14509	255.1	-1.06348	-4.00635
30	223.323	-27.4206	86.85	2.25478	254.6	-.60047	-2.17336
END	223.323	-27.4206	96.5	0	0	0	0
GND	199.427	59.4518	0	10.012	349.3	9.83826	-1.85722
32	199.427	59.4518	9.65	10.1324	349.1	9.94864	-1.92081
33	199.427	59.4518	19.3	9.93024	348.9	9.74478	-1.91023
34	199.427	59.4518	28.95	9.45594	348.8	9.27484	-1.84179
35	199.427	59.4518	38.6	8.72779	348.6	8.55677	-1.7193
36	199.427	59.4518	48.25	7.765	348.5	7.60953	-1.54606
37	199.427	59.4518	57.9	6.58971	348.4	6.45499	-1.32568
38	199.427	59.4518	67.55	5.22569	348.3	5.11665	-1.06198
39	199.427	59.4518	77.2	3.6943	348.2	3.61563	-.75833
40	199.427	59.4518	86.85	2.00203	348.	1.95853	-.415087
END	199.427	59.4518	96.5	0	0	0	0

**FIGURE 8**  
**WRSO MOMENT MODEL ARRAY SYNTHESIS**  
**(DIRECTIONAL – NIGHT)**

**APPLICATION FOR LICENSE INFORMATION**  
**EMPLOYING MOMENT METHOD MODELING**  
**WRSO, 810 KHZ, DA-2**  
**ORLOVISTA, FLORIDA**  
**FEBRUARY, 2015**

WRSO NIGHT

MEDIUM WAVE ARRAY SYNTHESIS FROM FIELD RATIOS

Frequency = .81 MHz

tower	field ratio	
	magnitude	phase (deg)
1	1.	0
2	0	0
3	.95	-29.5
4	0	0

VOLTAGES AND CURRENTS - rms

node	source voltage		current	
	magnitude	phase (deg)	magnitude	phase (deg)
1	164.627	63.8	2.37815	3.2
11	48.2653	296.8	.0838396	27.5
21	132.326	21.8	2.32942	334.2
31	93.6368	269.	.167967	358.8

Sum of square of source currents = 22.234

Total power = 400. watts

TOWER ADMITTANCE MATRIX

admittance	real (mhos)	imaginary (mhos)
Y(1, 1)	.00871243	-.00882986
Y(1, 2)	.00496811	.00269084
Y(1, 3)	.00272785	-.00149079
Y(1, 4)	.00332803	-.00202396
Y(2, 1)	.00496807	.00269091
Y(2, 2)	.00865981	-.00902374
Y(2, 3)	.00278277	-.00215183
Y(2, 4)	.0020943	-.00141139
Y(3, 1)	.00272784	-.00149078
Y(3, 2)	.00278277	-.00215185
Y(3, 3)	.00848884	-.00890128
Y(3, 4)	.00491857	.0025569
Y(4, 1)	.00332803	-.00202395
Y(4, 2)	.0020943	-.00141141
Y(4, 3)	.00491857	.0025569
Y(4, 4)	.00852187	-.00877838

TOWER IMPEDANCE MATRIX

impedance	real (ohms)	imaginary (ohms)
Z(1, 1)	51.0064	55.2755
Z(1, 2)	25.7748	-24.7706
Z(1, 3)	-18.1711	-3.06078
Z(1, 4)	-16.5232	-8.91811
Z(2, 1)	25.7744	-24.7709
Z(2, 2)	49.6066	52.1707
Z(2, 3)	-17.189	-5.32849
Z(2, 4)	-17.8057	1.08107
Z(3, 1)	-18.171	-3.06079
Z(3, 2)	-17.189	-5.32855

**FIGURE 8**  
**WRSO MOMENT MODEL ARRAY SYNTHESIS**  
**(DIRECTIONAL – NIGHT)**

Z(3, 3)	50.7966	55.1332
Z(3, 4)	25.9233	-25.0164
Z(4, 1)	-16.5232	-8.91811
Z(4, 2)	-17.8056	1.081
Z(4, 3)	25.9233	-25.0164
Z(4, 4)	50.7251	55.2564

**FIGURE 9**  
**WRSO MOMENT MODEL SUMMARY FOR**  
**DIRECTIONAL NIGHT MODE**

**APPLICATION FOR LICENSE INFORMATION**  
**EMPLOYING MOMENT METHOD MODELING**  
**WRSO, 810 KHZ, DA-2**  
**ORLOVISTA, FLORIDA**  
**FEBRUARY, 2015**

GEOMETRY  
 WRSO NIGHT

GEOMETRY  
 Wire coordinates in degrees; other dimensions in meters  
 Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.243	10
		0	0	96.5		
2	none	90.	81.6	0	.243	10
		90.	81.6	96.		
3	none	225.	7.	0	.243	10
		225.	7.	96.5		
4	none	208.1	343.4	0	.243	10
		208.1	343.4	96.5		

Number of wires = 4  
 current nodes = 40

Individual wires segment length radius	minimum		maximum	
	wire	value	wire	value
	2	9.6	1	9.65
	1	.243	1	.243

ELECTRICAL DESCRIPTION

Frequencies (MHz)

no.	frequency	step	no. of steps	segment length (wavelengths) minimum	maximum
1	.81	0	1	.0266667	.0268056

Sources

source	node	sector	magnitude	phase	type
1	1	1	232.817	63.8	voltage
2	21	1	187.137	21.8	voltage

Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	11	0	575.64	0	0	0
2	31	0	557.47	0	0	0

IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)	react (ohms)	imped (ohms)	phase (deg)	VSWR	S11 dB	S12 dB
source = 1; node 1, sector 1							
.81	33.962	60.298	69.204	60.6	4.0454	-4.385	-1.9677
source = 2; node 21, sector 1							
.81	38.307	41.942	56.803	47.6	2.6061	-7.0254	-.96023

**FIGURE 9**  
**WRSO MOMENT MODEL SUMMARY FOR**  
**DIRECTIONAL NIGHT MODE**

CURRENT rms  
 Frequency = .81 MHz  
 Input power = 400. watts  
 Efficiency = 100. %  
 coordinates in degrees

current				mag	phase	real	imaginary
no.	X	Y	Z	(amps)	(deg)	(amps)	(amps)
GND	0	0	0	2.37861	3.2	2.37493	.132359
2	0	0	9.65	2.46164	1.7	2.4605	.0750189
3	0	0	19.3	2.44764	.8	2.44738	.036138
4	0	0	28.95	2.35775	.1	2.35775	5.86E-03
5	0	0	38.6	2.19733	359.6	2.19726	-.0168924
6	0	0	48.25	1.97135	359.1	1.97108	-.0323633
7	0	0	57.9	1.68539	358.6	1.6849	-.0406187
8	0	0	67.55	1.34544	358.2	1.34479	-.0417169
9	0	0	77.2	.956957	357.9	.95629	-.0357237
10	0	0	86.85	.521547	357.5	.521059	-.0225592
END	0	0	96.5	0	0	0	0
GND	13.1475	-89.0345	0	.0839735	26.8	.074951	.0378669
12	13.1475	-89.0345	9.6	.0462457	26.7	.0412989	.0208101
13	13.1475	-89.0345	19.2	.0212658	26.3	.0190663	9.42E-03
14	13.1475	-89.0345	28.8	2.42E-03	17.1	2.32E-03	7.13E-04
15	13.1475	-89.0345	38.4	.0112656	210.2	-9.73E-03	-5.67E-03
16	13.1475	-89.0345	48.	.0200294	209.5	-.0174351	-9.86E-03
17	13.1475	-89.0345	57.6	.0242098	209.5	-.021067	-.0119289
18	13.1475	-89.0345	67.2	.0241126	209.7	-.020936	-.0119625
19	13.1475	-89.0345	76.8	.0200658	210.	-.0173698	-.0100462
20	13.1475	-89.0345	86.4	.0123212	210.4	-.0106294	-6.23E-03
END	13.1475	-89.0345	96.	0	0	0	0
GND	223.323	-27.4206	0	2.32935	334.2	2.09728	-1.01355
22	223.323	-27.4206	9.65	2.37803	332.6	2.11045	-1.09592
23	223.323	-27.4206	19.3	2.34445	331.5	2.06053	-1.11833
24	223.323	-27.4206	28.95	2.24331	330.7	1.95597	-1.09846
25	223.323	-27.4206	38.6	2.07908	330.	1.80038	-1.03981
26	223.323	-27.4206	48.25	1.85632	329.4	1.59776	-.945034
27	223.323	-27.4206	57.9	1.58028	328.9	1.35275	-.816912
28	223.323	-27.4206	67.55	1.25663	328.4	1.07033	-.658427
29	223.323	-27.4206	77.2	.890562	328.	.755004	-.472303
30	223.323	-27.4206	86.85	.483689	327.6	.408257	-.259387
END	223.323	-27.4206	96.5	0	0	0	0
GND	199.427	59.4518	0	.1679	358.9	.167871	-3.11E-03
32	199.427	59.4518	9.65	.094281	358.9	.0942651	-1.73E-03
33	199.427	59.4518	19.3	.0448671	359.	.0448606	-7.6E-04
34	199.427	59.4518	28.95	6.88E-03	.2	6.88E-03	2.49E-05
35	199.427	59.4518	38.6	.021208	178.3	-.0211983	6.41E-04
36	199.427	59.4518	48.25	.0398862	178.4	-.0398714	1.08E-03
37	199.427	59.4518	57.9	.0494597	178.4	-.0494414	1.34E-03
38	199.427	59.4518	67.55	.0502426	178.4	-.0502228	1.41E-03
39	199.427	59.4518	77.2	.0425701	178.3	-.0425515	1.26E-03
40	199.427	59.4518	86.85	.0266035	178.2	-.02659	8.48E-04
END	199.427	59.4518	96.5	0	0	0	0

**FIGURE 10  
DERIVED DIRECTIONAL PARAMETERS**

**APPLICATION FOR LICENSE INFORMATION  
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WRSO, 810 KHZ, DA-2  
ORLOVISTA, FLORIDA  
FEBRUARY, 2015**

**DAY:**

Tower	Theoretical		Base Network Input Current		Normalized TCT	
	Field	Phase	Amplitude	Phase	Amplitude	Phase
1 (SW)	1.000	0.0°	14.62	+1.15°	1.114	+95.9°
2 (SE)	.931	-99.8°	13.12	-94.76°	1.000	0.0°
3 (NE)	.744	-101.0°	10.80	-95.84°	.823	-1.1°
4 (NW)	.680	-11.3°	10.14	-10.79°	.773	+84.0°

**NIGHT:**

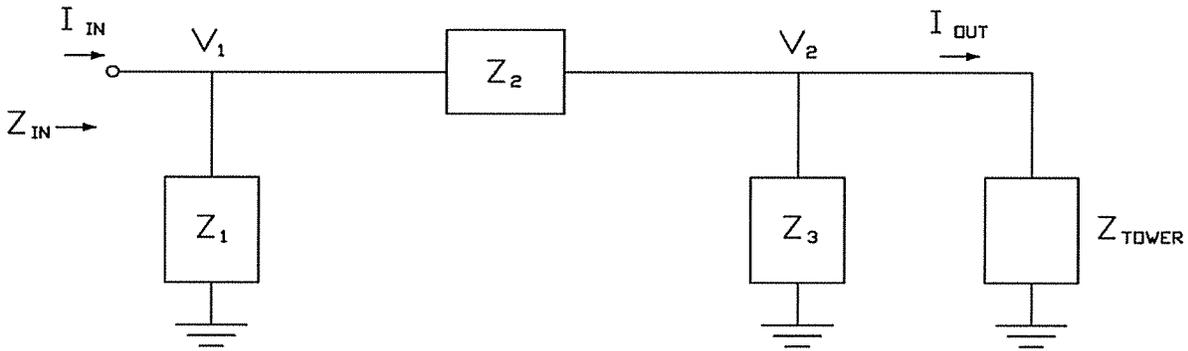
Tower	Theoretical		Base Network Input Current		Normalized TCT	
	Field	Phase	Amplitude	Phase	Amplitude	Phase
1 (SW)	1.000	0.0°	2.42	+2.77°	1.000	0.0°
2 (SE)			DETUNED			
3 (NE)	.950	-29.5°	2.37	-26.27°	.979	-29.0°
4 (NW)			DETUNED			

**FIGURE 11**  
**WRSO TOWER BASE CIRCUIT ANALYSIS DESCRIPTION**

**APPLICATION FOR LICENSE INFORMATION**  
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**WRSO, 810 KHZ, DA-2**  
**ORLOVISTA, FLORIDA**  
**FEBRUARY, 2015**

**CIRCUIT ANALYSIS**

Circuit Analysis was performed on each Tower of the WRSO model. "Phasetek" nodal Circuit Analysis program was used to compute base model Input/Output voltages and currents. For the Directional modes, the calculated Mininec Tower Base Drive Voltage was used to determine the Base Network Input Current. This point is the location of the Sampling TCT. " $Z_1$ " represents the ATU Shunt impedance, " $Z_2$ " represents the Tower Feed impedance, and " $Z_3$ " represents the Tower Base Shunt impedance.



**FIGURE 12**  
**WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 1 (OTHERS OPEN)

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 51.00, 55.39 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.43	55.42
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	82.82	-8.57

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	49.18	74.50	89.27	56.57
INPUT CURRENT (AMPS) :	0.62	-0.93	1.12	-56.57
OUTPUT CURRENT (AMPS) :	0.62	-0.91	1.10	-55.93

INPUT/OUTPUT CURRENT RATIO = 1.0183  
 INPUT/OUTPUT PHASE = -0.64 DEGREES

**FIGURE 12**  
**WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 2 (OTHERS OPEN)

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 26.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -4366.40 OHMS  
 TOWER IMPEDANCE (R,X) : 49.85, 52.31 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.06	52.36
1		2	0.00	26.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	78.19	-11.19

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	48.74	77.29	91.38	57.76
INPUT CURRENT (AMPS) :	0.58	-0.93	1.09	-57.76
OUTPUT CURRENT (AMPS) :	0.58	-0.91	1.08	-57.57

INPUT/OUTPUT CURRENT RATIO = 1.0113  
 INPUT/OUTPUT PHASE = -0.19 DEGREES

**FIGURE 12**  
**WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 3 (OTHERS OPEN)

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 21.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 51.04, 55.24 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.47	55.27
1		2	0.00	21.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	82.08	-8.95

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	49.20	75.31	89.95	56.85
INPUT CURRENT (AMPS) :	0.61	-0.93	1.11	-56.85
OUTPUT CURRENT (AMPS) :	0.61	-0.91	1.09	-56.21

INPUT/OUTPUT CURRENT RATIO = 1.0186  
 INPUT/OUTPUT PHASE = -0.64 DEGREES

**FIGURE 12**  
**WRSO CIRCUIT ANALYSIS FOR INDIVIDUAL TOWERS**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 4 (OTHERS OPEN)

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 50.94, 55.33 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	51.38	55.37
1	1	2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	100.00	0.00
2	82.81	-8.58

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	49.13	74.45	89.20	56.58
INPUT CURRENT (AMPS) :	0.62	-0.94	1.12	-56.58
OUTPUT CURRENT (AMPS) :	0.62	-0.91	1.10	-55.94

INPUT/OUTPUT CURRENT RATIO = 1.0183  
 INPUT/OUTPUT PHASE = -0.64 DEGREES

**FIGURE 13**  
**WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 1 DAY

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 13.16, 44.39 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	13.25	44.53
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	944.81	79.77
2	666.33	74.80

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	12.75	63.36	64.63	78.62
INPUT CURRENT (AMPS) :	14.62	0.29	14.62	1.15
OUTPUT CURRENT (AMPS) :	14.39	0.33	14.39	1.31

INPUT/OUTPUT CURRENT RATIO = 1.0158  
 INPUT/OUTPUT PHASE = -0.16 DEGREES

**FIGURE 13**  
**WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 2 DAY

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 26.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -4366.40 OHMS  
 TOWER IMPEDANCE (R,X) : 57.60, 65.64 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	59.36	65.85
1		2	0.00	26.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	1395.79	-36.64
2	1131.51	314.20

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	56.22	90.37	106.43	58.12
INPUT CURRENT (AMPS) :	-1.09	-13.07	13.12	-94.76
OUTPUT CURRENT (AMPS) :	-1.02	-12.92	12.96	-94.54

INPUT/OUTPUT CURRENT RATIO = 1.0122  
 INPUT/OUTPUT PHASE = -0.22 DEGREES

**FIGURE 13**  
**WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 3 DAY

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 21.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 62.63, 46.44 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	63.07	46.31
1		2	0.00	21.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	976.38	-47.93
2	828.24	301.50

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	60.59	67.10	90.41	47.92
INPUT CURRENT (AMPS) :	-1.10	-10.74	10.80	-95.84
OUTPUT CURRENT (AMPS) :	-0.94	-10.58	10.62	-95.06

INPUT/OUTPUT CURRENT RATIO = 1.0167  
 INPUT/OUTPUT PHASE = -0.78 DEGREES

**FIGURE 13**  
**WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL DAY MODE**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 4 DAY

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 5.37, 30.85 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	5.40	30.92
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	511.47	73.25
2	313.52	69.40

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	5.24	50.17	50.44	84.04
INPUT CURRENT (AMPS) :	9.96	-1.90	10.14	-10.79
OUTPUT CURRENT (AMPS) :	9.84	-1.86	10.01	-10.72

INPUT/OUTPUT CURRENT RATIO = 1.0128  
 INPUT/OUTPUT PHASE = -0.07 DEGREES

**FIGURE 14**  
**WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL NIGHT MODE**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 1 NIGHT

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 20.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00, -13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 33.96, 60.30 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	34.28	60.49
1		2	0.00	20.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	207.15	70.27
2	164.63	63.80

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	32.68	78.93	85.43	67.51
INPUT CURRENT (AMPS) :	2.42	0.12	2.42	2.77
OUTPUT CURRENT (AMPS) :	2.38	0.13	2.38	3.19

INPUT/OUTPUT CURRENT RATIO = 1.0194  
 INPUT/OUTPUT PHASE = -0.42 DEGREES

**FIGURE 14**  
**WRSO CIRCUIT ANALYSIS FOR DIRECTIONAL NIGHT MODE**

CUSTOMER : WRSO  
 NETWORK ID : TOWER 3 NIGHT

FREQUENCY : 810.00 kHz  
 ATU SHUNT IMPEDANCE (R,X) : 0.00, 3350.00 OHMS  
 TOWER FEED IMPEDANCE (R,X) : 0.00, 21.00 OHMS  
 TOWER SHUNT IMPEDANCE (R,X) : 0.00,-13099.20 OHMS  
 TOWER IMPEDANCE (R,X) : 38.31, 41.94 OHMS

NODE	TO	NODE	IMPEDANCE (OHMS)	
			R	X
1		GROUND	0.00	3350.00
2		GROUND	38.55	41.96
1		2	0.00	21.00

NODE	VOLTAGE	
	MAGNITUDE	PHASE
1	171.44	32.90
2	132.33	21.80

	REAL	IMAGINARY	MAGNITUDE	PHASE
INPUT IMPEDANCE (OHMS) :	37.14	62.22	72.46	59.17
INPUT CURRENT (AMPS) :	2.12	-1.05	2.37	-26.27
OUTPUT CURRENT (AMPS) :	2.10	-1.01	2.33	-25.79

INPUT/OUTPUT CURRENT RATIO = 1.0156  
 INPUT/OUTPUT PHASE = -0.48 DEGREES

## FIGURE 15

WRSO REFERENCE POINTS -- DA-D

1/3/2015

<u>Radial</u>	<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>		
				<u>deg</u>	<u>min</u>	<u>sec</u>			
<b>N 10 E</b>	1	1.52	1003	160.0	N	28	35	6.4	Mercy Drive at Unisource entrance
					W	81	25	52.5	
	2	4.91	1020	35.0	N	28	36	54.4	Parking lot of #6401 Edgewater Drive
					W	81	25	31.7	
	3	5.45	1025	33.0	N	28	37	11.9	Driveway 3531 Dr. Love Road
					W	81	25	27.9	
<b>N 72 E</b>	1	1.84	1040	1310.0	N	28	34	36.2	John Young Pkwy. --south end of Wawa parking lot
					W	81	24	57.4	
	2	2.40	1048	1080.0	N	28	34	41.9	Regent Ave. 100' north of Silver Star Rd.
					W	81	24	37.9	
	3	2.74	1053	1100.0	N	28	34	45.5	Orange Blossom Trail opposite gate
					W	81	24	26.2	
<b>N 127.5 E</b>	1	2.22	1126	138.0	N	28	33	35.3	100' west of int. John Young Pkwy + WD Judge Road
					W	81	24	56.8	
	2	3.67	1105	81.0	N	28	33	5.9	Arlington St + Vern Dr -- southwest corner
					W	81	24	14.6	
	3	3.54	1114	105.0	N	28	33	8.5	W Colonial Dr -- east edge of Citgo parking lot
					W	81	24	19.1	

## FIGURE 15 CONTINUED

WRSO REFERENCE POINTS -- DA-D cont. 1/3/2015

<u>Radial</u>	<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>
				<u>deg</u>	<u>min</u>	<u>sec</u>	
<b>N 230 E</b>	1	2.48	1048	7.6	N 28 33 26.6	26.6	San Domingo Rd near Balboa -- drwy opp spd lim 25
					W 81 27 12.1		
	2	2.93	1032	22.0	N 28 33 16.7	16.7	Mailbox 810 Governors Ave
					W 81 27 24.4		
	3	3.24	1027	18.3	N 28 33 10.6	10.6	Hastings St -- St Andrew Church lot drwy
					W 81 27 33.6		
<b>N 269.5 E</b>	1	1.45	1055	43.0	N 28 34 17.0	17.0	Drwy 2117 Beecher St
					W 81 26 55.2		
	2	1.94	1105	20.5	N 28 34 16.9	16.9	Casa Vida Apts. @ curve south of Building N -- on road
					W 81 27 13.6		
	3	2.27	1112	22.2	N 28 34 15.6	15.6	Golf Club Pkwy + Silver Spruce @ fire hydrant
					W 81 27 25.4		
<b>N 322.5 E</b>	1	2.60	1122	24.2	N 28 35 24.5	24.5	White Heron Dr + Donovan St -- west side
					W 81 27 0.8		
	2	2.89	1128	27.8	N 28 35 31.5	31.5	Grandview off Pine Hills Rd @ spd lim 25
					W 81 27 7.9		
	3	3.50	1133	23.1	N 28 35 47.0	47.0	Mailbox 4403 Robbins Ave
					W 81 27 22.0		

## FIGURE 15 CONTINUED

WRSO REFERENCE POINTS -- DA-N

1/3/2015

<u>Radial</u>		<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>
					<u>deg</u>	<u>min</u>	<u>sec</u>	
<b>N 28.5 E</b>	1	1.24	1338	14.1	N 28	34	58.6	Road to industrial building -- @ fence
					W 81	25	41.3	
	2	2.16	1353	7.7	N 28	35	18.8	Int of Bay Lake Road + Eunice Ave
					W 81	25	22.7	
	3	3.73	1403	5.6	N 28	36	3.2	Trotters Park lot by fire hydrant + stop sign
					W 81	24	55.2	
<b>N 89.5 E</b>	1	2.31	1428	135.0	N 28	34	18.5	Lynx Lane @ bus stop
					W 81	24	37.1	
	2	2.71	1413	91.0	N 28	34	19.3	Orange Blossom Trl W side -- Pr'ton Commerce Ctr.
					W 81	24	22.1	
	3	3.11	1421	72.0	N 28	34	19.1	1503 W Smith St -- parking lot
					W 81	24	7.5	
<b>N 139 E</b>	1	3.05	1453	8.0	N 28	33	3.8	John Young Pkwy W side -- center of mall parking lot
					W 81	24	47.8	
	2	4.04	1448	1.95	N 28	32	39.1	int Lakeland Ave + Washington St
					W 81	24	25.1	
	3	4.68	1439	2.8	N 28	32	23.7	Church St opp stadium box office
					W 81	24	9.0	

## FIGURE 15 CONTINUED

WRSO REFERENCE POINTS -- DA-N cont.

1/3/2015

<u>Radial</u>	<u>Dist</u> <u>km</u>	<u>Time</u>	<u>mV/m</u>	<u>CO-ORD NAD27</u>			<u>Description</u>
				<u>deg</u>	<u>min</u>	<u>sec</u>	
<b>N 235 E</b>	1	1.76	1343	7.0	N 28 33 45.2		Mailbox 4913 Cortez Dr
					W 81 26 55.0		
	2	2.09	1350	4.5	N 28 33 39.1		Drwy 1109 Santa Anita St
					W 81 27 4.8		
	3	2.46	1356	9.6	N 28 33 31.8		Mailbox 1006 Emeraldalda Rd
					W 81 27 15.9		
<b>N 284.5 E</b>	1	1.70	1406	120.0	N 28 34 31.3		Queensway Rd + Kipp @ street sign
					W 81 27 2.6		
	2	2.30	1413	96.0	N 28 34 37.1		Drwy 5800 Golf Club Pkwy
					W 81 27 23.7		
	3	3.02	1419	71.0	N 28 34 42.1		Mailbox 2609 Pioneer Rd
					W 81 27 49.7		
<b>N 345.5 E</b>	1	1.14	1432	20.4	N 28 34 53.5		Seaboard Rd north side @ C+S -- on drain
					W 81 26 13.0		
	2	1.67	1441	13.7	N 28 35 10.1		Shader Rd W of Daltile plant + rail -- S side @ drain
					W 81 26 17.6		
	3	4.45	1458	3.0	N 28 36 37.3		opp drwy 5426 Lee Ann Dr
					W 81 26 43.6		