



**STATEMENT OF JOHN E. HIDLE, P.E.
IN SUPPORT OF A REQUEST FOR A
SPECIAL TEMPORARY AUTHORIZATION (STA)
TO MAKE TRANSITION USING AN INTERIM ANTENNA
PENDING INSTALLATION OF THE MAIN ANTENNA
WWHO - CHILLICOTHE, OHIO
DTV - CH. 23 - 175.3 kW - 194.4 m HAAT**

Prepared for: MANHAN MEDIA, INC.

I am a Consulting Engineer, an employee in the firm of Carl T. Jones Corporation, with offices located in Springfield, Virginia. My education and experience are a matter of record with the Federal Communications Commission. I am a Licensed Professional Engineer in the Commonwealth of Virginia, No. 7418, and in New York State, No. 63418.

GENERAL

This office has been authorized by MANHAN MEDIA, INC., licensee of WWHO, facility ID number 21158, licensed to Chillicothe, Ohio, to prepare this statement and associated exhibits in support of a request for STA to transition to channel 23 using an interim temporary antenna. WWHO has installed its permanent main transmitter but is not able to secure the installation of its authorized main antenna prior to the phase 8 completion date, March 13, 2020. Therefore, WWHO herein requests authorization to make its transition using a temporary interim operation using an interim antenna. Once the main antenna, as authorized by construction permit, file number 0000094850, is installed and operational WWHO will be ready to license and commence operation on its final post transition broadcast facility.

BLANKETING AND INTERMODULATION INTERFERENCE

Other broadcast and non-broadcast facilities are either co-located with, or located within 10 km of the proposed WWHO site. The applicant does recognize its responsibility to remedy complaints of interference that might result from this proposal in accordance with applicable Rules.

RADIO FREQUENCY IMPACT, SAFETY & STATEMENT OF COMPLIANCE

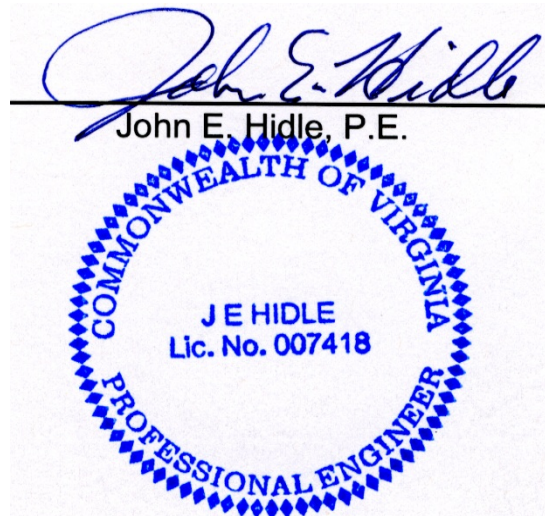
The licensee of WWHO is committed to the protection of station personnel and/or tower contractors working in the vicinity of the WWHO antenna and will reduce power or cease operation, when necessary, to ensure protection to personnel.

As shown in Appendix A the proposed WWHO channel 23 post-transition interim STA facility proposed herein will operate with a maximum ERP of 175.3 kW from an elliptically polarized directional transmitting antenna with a centerline height of 213.4 meters above ground level (AGL). Considering the elevation pattern submitted elsewhere in this application, the vertical plane relative field factor is less than 0.200 at all depression angles greater than 13 degrees. The proposed WWHO STA facility is predicted to produce a worst-case power density at two meters above ground level, at 122.1 meters from the tower base, of $1.226 \mu\text{W}/\text{cm}^2$, which is 0.35% of the FCC guideline value of $351.33 \mu\text{W}/\text{cm}^2$ for an "uncontrolled" environment, and 0.070% of the FCC's guideline value for "controlled" environments. Therefore, pursuant to Section 1.1307(b)(3) of the FCC Rules, because the proposed facility would not exceed 5% of the uncontrolled and controlled exposure limits, the proposal's power density contribution is considered insignificant.

SUMMARY

It is submitted that the instant request for STA for WWHO to make its transition to channel 23 using a temporary interim antenna facility until the authorized permanent main antenna can be installed, as described herein, does comply with the Rules, Regulations and relevant Policies of the Federal Communications Commission. This statement, FCC Form 2100, its technical sections, and the attached exhibits were prepared by me or under my direct supervision and are believed to be true and correct to the best of my knowledge and belief.

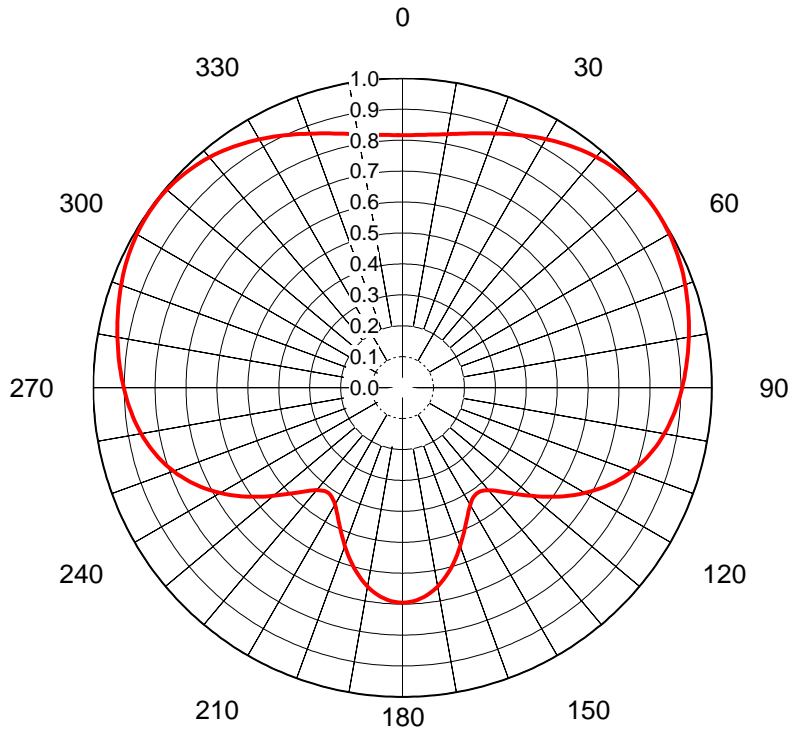
DATED: February 24, 2020



AZIMUTH PATTERN Horizontal Polarization

Proposal No. **WWHO Interim Ch 23**
 Date **21-Feb-20**
 Call Letters **WWHO**
 Channel **23**
 Frequency **527 MHz**
 Antenna Type **TFU-8WB/VP-R C160**
 Gain **1.54 (1.88dB)**
 Calculated

Pattern Number **WB-C160-23 Hpol**



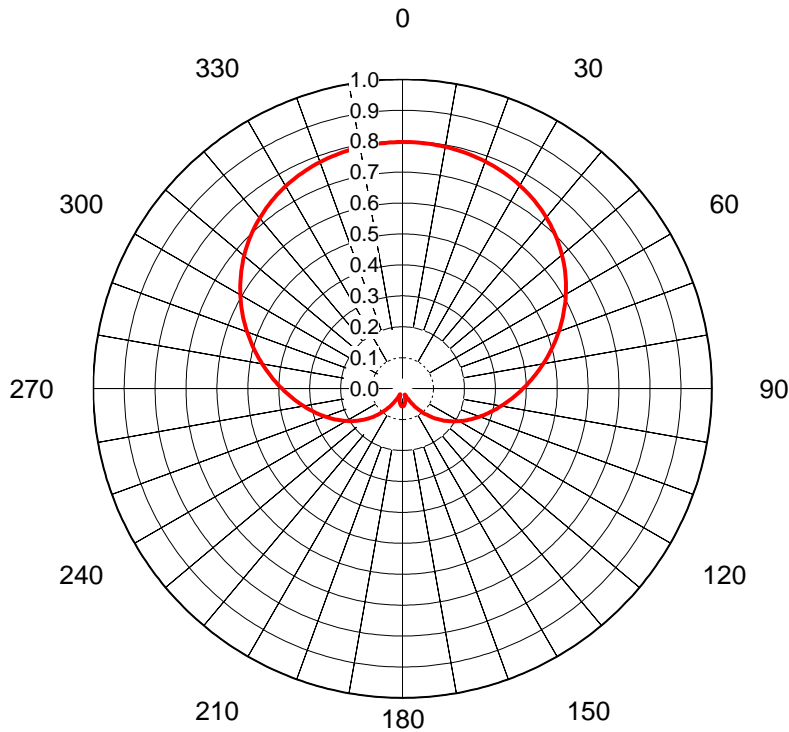
| Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value |
|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|
| 0 | 0.817 | 36 | 0.957 | 72 | 0.966 | 108 | 0.806 | 144 | 0.418 | 180 | 0.695 | 216 | 0.417 | 252 | 0.805 | 288 | 0.962 | 324 | 0.956 |
| 1 | 0.817 | 37 | 0.962 | 73 | 0.963 | 109 | 0.798 | 145 | 0.417 | 181 | 0.695 | 217 | 0.419 | 253 | 0.813 | 289 | 0.965 | 325 | 0.951 |
| 2 | 0.817 | 38 | 0.966 | 74 | 0.960 | 110 | 0.789 | 146 | 0.419 | 182 | 0.693 | 218 | 0.422 | 254 | 0.821 | 290 | 0.968 | 326 | 0.947 |
| 3 | 0.818 | 39 | 0.970 | 75 | 0.957 | 111 | 0.780 | 147 | 0.421 | 183 | 0.691 | 219 | 0.427 | 255 | 0.828 | 291 | 0.971 | 327 | 0.942 |
| 4 | 0.819 | 40 | 0.974 | 76 | 0.954 | 112 | 0.771 | 148 | 0.425 | 184 | 0.688 | 220 | 0.433 | 256 | 0.834 | 292 | 0.974 | 328 | 0.937 |
| 5 | 0.821 | 41 | 0.977 | 77 | 0.950 | 113 | 0.761 | 149 | 0.431 | 185 | 0.684 | 221 | 0.440 | 257 | 0.841 | 293 | 0.977 | 329 | 0.932 |
| 6 | 0.822 | 42 | 0.981 | 78 | 0.947 | 114 | 0.751 | 150 | 0.437 | 186 | 0.680 | 222 | 0.448 | 258 | 0.847 | 294 | 0.980 | 330 | 0.927 |
| 7 | 0.824 | 43 | 0.984 | 79 | 0.943 | 115 | 0.740 | 151 | 0.445 | 187 | 0.674 | 223 | 0.458 | 259 | 0.852 | 295 | 0.982 | 331 | 0.922 |
| 8 | 0.827 | 44 | 0.986 | 80 | 0.940 | 116 | 0.729 | 152 | 0.454 | 188 | 0.668 | 224 | 0.468 | 260 | 0.858 | 296 | 0.984 | 332 | 0.916 |
| 9 | 0.829 | 45 | 0.989 | 81 | 0.937 | 117 | 0.718 | 153 | 0.464 | 189 | 0.661 | 225 | 0.480 | 261 | 0.863 | 297 | 0.986 | 333 | 0.911 |
| 10 | 0.832 | 46 | 0.991 | 82 | 0.933 | 118 | 0.706 | 154 | 0.474 | 190 | 0.653 | 226 | 0.491 | 262 | 0.868 | 298 | 0.988 | 334 | 0.906 |
| 11 | 0.836 | 47 | 0.993 | 83 | 0.930 | 119 | 0.694 | 155 | 0.485 | 191 | 0.644 | 227 | 0.504 | 263 | 0.873 | 299 | 0.990 | 335 | 0.900 |
| 12 | 0.839 | 48 | 0.995 | 84 | 0.926 | 120 | 0.681 | 156 | 0.496 | 192 | 0.635 | 228 | 0.517 | 264 | 0.877 | 300 | 0.992 | 336 | 0.895 |
| 13 | 0.843 | 49 | 0.997 | 85 | 0.923 | 121 | 0.668 | 157 | 0.508 | 193 | 0.625 | 229 | 0.530 | 265 | 0.882 | 301 | 0.993 | 337 | 0.890 |
| 14 | 0.847 | 50 | 0.998 | 86 | 0.919 | 122 | 0.655 | 158 | 0.520 | 194 | 0.615 | 230 | 0.544 | 266 | 0.886 | 302 | 0.994 | 338 | 0.884 |
| 15 | 0.851 | 51 | 0.999 | 87 | 0.915 | 123 | 0.642 | 159 | 0.533 | 195 | 0.604 | 231 | 0.558 | 267 | 0.890 | 303 | 0.995 | 339 | 0.879 |
| 16 | 0.855 | 52 | 0.999 | 88 | 0.912 | 124 | 0.628 | 160 | 0.545 | 196 | 0.593 | 232 | 0.572 | 268 | 0.894 | 304 | 0.996 | 340 | 0.874 |
| 17 | 0.860 | 53 | 1.000 | 89 | 0.908 | 125 | 0.614 | 161 | 0.557 | 197 | 0.581 | 233 | 0.586 | 269 | 0.898 | 305 | 0.997 | 341 | 0.869 |
| 18 | 0.864 | 54 | 1.000 | 90 | 0.904 | 126 | 0.600 | 162 | 0.570 | 198 | 0.569 | 234 | 0.600 | 270 | 0.901 | 306 | 0.997 | 342 | 0.864 |
| 19 | 0.869 | 55 | 1.000 | 91 | 0.900 | 127 | 0.586 | 163 | 0.582 | 199 | 0.557 | 235 | 0.614 | 271 | 0.905 | 307 | 0.997 | 343 | 0.860 |
| 20 | 0.874 | 56 | 0.999 | 92 | 0.896 | 128 | 0.572 | 164 | 0.593 | 200 | 0.545 | 236 | 0.628 | 272 | 0.909 | 308 | 0.997 | 344 | 0.855 |
| 21 | 0.879 | 57 | 0.999 | 93 | 0.892 | 129 | 0.558 | 165 | 0.604 | 201 | 0.532 | 237 | 0.642 | 273 | 0.912 | 309 | 0.996 | 345 | 0.851 |
| 22 | 0.885 | 58 | 0.998 | 94 | 0.888 | 130 | 0.544 | 166 | 0.615 | 202 | 0.520 | 238 | 0.655 | 274 | 0.916 | 310 | 0.995 | 346 | 0.847 |
| 23 | 0.890 | 59 | 0.997 | 95 | 0.884 | 131 | 0.531 | 167 | 0.626 | 203 | 0.508 | 239 | 0.668 | 275 | 0.919 | 311 | 0.994 | 347 | 0.843 |
| 24 | 0.895 | 60 | 0.996 | 96 | 0.879 | 132 | 0.517 | 168 | 0.635 | 204 | 0.496 | 240 | 0.681 | 276 | 0.923 | 312 | 0.993 | 348 | 0.839 |
| 25 | 0.901 | 61 | 0.994 | 97 | 0.875 | 133 | 0.504 | 169 | 0.644 | 205 | 0.485 | 241 | 0.693 | 277 | 0.926 | 313 | 0.991 | 349 | 0.836 |
| 26 | 0.906 | 62 | 0.992 | 98 | 0.870 | 134 | 0.492 | 170 | 0.653 | 206 | 0.474 | 242 | 0.706 | 278 | 0.929 | 314 | 0.989 | 350 | 0.832 |
| 27 | 0.912 | 63 | 0.990 | 99 | 0.865 | 135 | 0.480 | 171 | 0.661 | 207 | 0.463 | 243 | 0.717 | 279 | 0.933 | 315 | 0.987 | 351 | 0.829 |
| 28 | 0.917 | 64 | 0.988 | 100 | 0.859 | 136 | 0.469 | 172 | 0.668 | 208 | 0.454 | 244 | 0.729 | 280 | 0.936 | 316 | 0.984 | 352 | 0.827 |
| 29 | 0.922 | 65 | 0.986 | 101 | 0.854 | 137 | 0.458 | 173 | 0.674 | 209 | 0.445 | 245 | 0.740 | 281 | 0.940 | 317 | 0.982 | 353 | 0.824 |
| 30 | 0.928 | 66 | 0.984 | 102 | 0.848 | 138 | 0.449 | 174 | 0.680 | 210 | 0.437 | 246 | 0.750 | 282 | 0.943 | 318 | 0.979 | 354 | 0.822 |
| 31 | 0.933 | 67 | 0.981 | 103 | 0.842 | 139 | 0.440 | 175 | 0.684 | 211 | 0.430 | 247 | 0.761 | 283 | 0.946 | 319 | 0.975 | 355 | 0.821 |
| 32 | 0.938 | 68 | 0.978 | 104 | 0.835 | 140 | 0.433 | 176 | 0.688 | 212 | 0.425 | 248 | 0.770 | 284 | 0.950 | 320 | 0.972 | 356 | 0.819 |
| 33 | 0.943 | 69 | 0.975 | 105 | 0.828 | 141 | 0.427 | 177 | 0.691 | 213 | 0.421 | 249 | 0.780 | 285 | 0.953 | 321 | 0.968 | 357 | 0.818 |
| 34 | 0.948 | 70 | 0.973 | 106 | 0.821 | 142 | 0.423 | 178 | 0.693 | 214 | 0.418 | 250 | 0.789 | 286 | 0.956 | 322 | 0.964 | 358 | 0.817 |
| 35 | 0.953 | 71 | 0.970 | 107 | 0.814 | 143 | 0.419 | 179 | 0.695 | 215 | 0.417 | 251 | 0.797 | 287 | 0.959 | 323 | 0.960 | 359 | 0.817 |

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AZIMUTH PATTERN Vertical Polarization

Proposal No. **WWHO Interim Ch 23**
 Date **21-Feb-20**
 Call Letters **WWHO**
 Channel **23**
 Frequency **527 MHz**
 Antenna Type **TFU-8WB/VP-R C160**
 Gain **2.61 (4.17dB)**
 Calculated

Pattern Number **WB-C160-23 Vpol**



| Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value | Deg | Value |
|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|-----|-------|
| 0 | 0.797 | 36 | 0.739 | 72 | 0.522 | 108 | 0.276 | 144 | 0.077 | 180 | 0.058 | 216 | 0.074 | 252 | 0.277 | 288 | 0.520 | 324 | 0.735 |
| 1 | 0.797 | 37 | 0.735 | 73 | 0.515 | 109 | 0.271 | 145 | 0.072 | 181 | 0.058 | 217 | 0.079 | 253 | 0.283 | 289 | 0.527 | 325 | 0.739 |
| 2 | 0.797 | 38 | 0.731 | 74 | 0.507 | 110 | 0.265 | 146 | 0.066 | 182 | 0.057 | 218 | 0.085 | 254 | 0.288 | 290 | 0.534 | 326 | 0.743 |
| 3 | 0.797 | 39 | 0.727 | 75 | 0.500 | 111 | 0.260 | 147 | 0.061 | 183 | 0.057 | 219 | 0.091 | 255 | 0.294 | 291 | 0.542 | 327 | 0.746 |
| 4 | 0.797 | 40 | 0.723 | 76 | 0.492 | 112 | 0.254 | 148 | 0.056 | 184 | 0.056 | 220 | 0.096 | 256 | 0.300 | 292 | 0.549 | 328 | 0.750 |
| 5 | 0.797 | 41 | 0.719 | 77 | 0.484 | 113 | 0.249 | 149 | 0.051 | 185 | 0.055 | 221 | 0.102 | 257 | 0.306 | 293 | 0.556 | 329 | 0.753 |
| 6 | 0.796 | 42 | 0.714 | 78 | 0.477 | 114 | 0.243 | 150 | 0.046 | 186 | 0.054 | 222 | 0.108 | 258 | 0.312 | 294 | 0.564 | 330 | 0.756 |
| 7 | 0.796 | 43 | 0.710 | 79 | 0.469 | 115 | 0.238 | 151 | 0.041 | 187 | 0.053 | 223 | 0.113 | 259 | 0.318 | 295 | 0.571 | 331 | 0.759 |
| 8 | 0.795 | 44 | 0.705 | 80 | 0.462 | 116 | 0.232 | 152 | 0.037 | 188 | 0.051 | 224 | 0.119 | 260 | 0.325 | 296 | 0.578 | 332 | 0.762 |
| 9 | 0.795 | 45 | 0.700 | 81 | 0.454 | 117 | 0.227 | 153 | 0.033 | 189 | 0.049 | 225 | 0.125 | 261 | 0.331 | 297 | 0.585 | 333 | 0.764 |
| 10 | 0.794 | 46 | 0.695 | 82 | 0.447 | 118 | 0.221 | 154 | 0.029 | 190 | 0.047 | 226 | 0.130 | 262 | 0.337 | 298 | 0.592 | 334 | 0.767 |
| 11 | 0.793 | 47 | 0.689 | 83 | 0.440 | 119 | 0.216 | 155 | 0.026 | 191 | 0.045 | 227 | 0.136 | 263 | 0.343 | 299 | 0.599 | 335 | 0.769 |
| 12 | 0.792 | 48 | 0.684 | 84 | 0.432 | 120 | 0.211 | 156 | 0.023 | 192 | 0.043 | 228 | 0.142 | 264 | 0.350 | 300 | 0.606 | 336 | 0.772 |
| 13 | 0.791 | 49 | 0.679 | 85 | 0.425 | 121 | 0.205 | 157 | 0.021 | 193 | 0.040 | 229 | 0.147 | 265 | 0.356 | 301 | 0.612 | 337 | 0.774 |
| 14 | 0.790 | 50 | 0.673 | 86 | 0.418 | 122 | 0.200 | 158 | 0.021 | 194 | 0.038 | 230 | 0.153 | 266 | 0.363 | 302 | 0.619 | 338 | 0.776 |
| 15 | 0.789 | 51 | 0.667 | 87 | 0.411 | 123 | 0.194 | 159 | 0.021 | 195 | 0.035 | 231 | 0.159 | 267 | 0.370 | 303 | 0.626 | 339 | 0.778 |
| 16 | 0.788 | 52 | 0.661 | 88 | 0.404 | 124 | 0.189 | 160 | 0.022 | 196 | 0.032 | 232 | 0.164 | 268 | 0.376 | 304 | 0.632 | 340 | 0.780 |
| 17 | 0.786 | 53 | 0.655 | 89 | 0.397 | 125 | 0.183 | 161 | 0.024 | 197 | 0.030 | 233 | 0.170 | 269 | 0.383 | 305 | 0.638 | 341 | 0.781 |
| 18 | 0.785 | 54 | 0.649 | 90 | 0.390 | 126 | 0.178 | 162 | 0.026 | 198 | 0.027 | 234 | 0.176 | 270 | 0.390 | 306 | 0.645 | 342 | 0.783 |
| 19 | 0.783 | 55 | 0.643 | 91 | 0.383 | 127 | 0.172 | 163 | 0.029 | 199 | 0.025 | 235 | 0.181 | 271 | 0.397 | 307 | 0.651 | 343 | 0.785 |
| 20 | 0.782 | 56 | 0.636 | 92 | 0.376 | 128 | 0.167 | 164 | 0.031 | 200 | 0.022 | 236 | 0.187 | 272 | 0.404 | 308 | 0.657 | 344 | 0.786 |
| 21 | 0.780 | 57 | 0.630 | 93 | 0.369 | 129 | 0.161 | 165 | 0.034 | 201 | 0.021 | 237 | 0.192 | 273 | 0.411 | 309 | 0.663 | 345 | 0.788 |
| 22 | 0.778 | 58 | 0.623 | 94 | 0.362 | 130 | 0.156 | 166 | 0.037 | 202 | 0.020 | 238 | 0.198 | 274 | 0.418 | 310 | 0.668 | 346 | 0.789 |
| 23 | 0.776 | 59 | 0.616 | 95 | 0.356 | 131 | 0.150 | 167 | 0.039 | 203 | 0.020 | 239 | 0.204 | 275 | 0.425 | 311 | 0.674 | 347 | 0.790 |
| 24 | 0.774 | 60 | 0.610 | 96 | 0.349 | 132 | 0.145 | 168 | 0.042 | 204 | 0.021 | 240 | 0.209 | 276 | 0.432 | 312 | 0.680 | 348 | 0.791 |
| 25 | 0.772 | 61 | 0.603 | 97 | 0.343 | 133 | 0.139 | 169 | 0.044 | 205 | 0.023 | 241 | 0.215 | 277 | 0.439 | 313 | 0.685 | 349 | 0.792 |
| 26 | 0.769 | 62 | 0.596 | 98 | 0.336 | 134 | 0.133 | 170 | 0.046 | 206 | 0.026 | 242 | 0.220 | 278 | 0.446 | 314 | 0.690 | 350 | 0.793 |
| 27 | 0.767 | 63 | 0.589 | 99 | 0.330 | 135 | 0.128 | 171 | 0.048 | 207 | 0.030 | 243 | 0.226 | 279 | 0.453 | 315 | 0.695 | 351 | 0.794 |
| 28 | 0.764 | 64 | 0.581 | 100 | 0.324 | 136 | 0.122 | 172 | 0.050 | 208 | 0.034 | 244 | 0.231 | 280 | 0.461 | 316 | 0.700 | 352 | 0.794 |
| 29 | 0.762 | 65 | 0.574 | 101 | 0.318 | 137 | 0.116 | 173 | 0.052 | 209 | 0.038 | 245 | 0.237 | 281 | 0.468 | 317 | 0.705 | 353 | 0.795 |
| 30 | 0.759 | 66 | 0.567 | 102 | 0.312 | 138 | 0.111 | 174 | 0.053 | 210 | 0.043 | 246 | 0.243 | 282 | 0.475 | 318 | 0.710 | 354 | 0.796 |
| 31 | 0.756 | 67 | 0.560 | 103 | 0.306 | 139 | 0.105 | 175 | 0.055 | 211 | 0.048 | 247 | 0.248 | 283 | 0.483 | 319 | 0.715 | 355 | 0.796 |
| 32 | 0.753 | 68 | 0.552 | 104 | 0.300 | 140 | 0.099 | 176 | 0.056 | 212 | 0.053 | 248 | 0.254 | 284 | 0.490 | 320 | 0.719 | 356 | 0.797 |
| 33 | 0.750 | 69 | 0.545 | 105 | 0.294 | 141 | 0.094 | 177 | 0.057 | 213 | 0.058 | 249 | 0.259 | 285 | 0.498 | 321 | 0.723 | 357 | 0.797 |
| 34 | 0.746 | 70 | 0.537 | 106 | 0.288 | 142 | 0.088 | 178 | 0.057 | 214 | 0.063 | 250 | 0.265 | 286 | 0.505 | 322 | 0.727 | 358 | 0.797 |
| 35 | 0.743 | 71 | 0.530 | 107 | 0.282 | 143 | 0.083 | 179 | 0.058 | 215 | 0.068 | 251 | 0.271 | 287 | 0.512 | 323 | 0.731 | 359 | 0.797 |

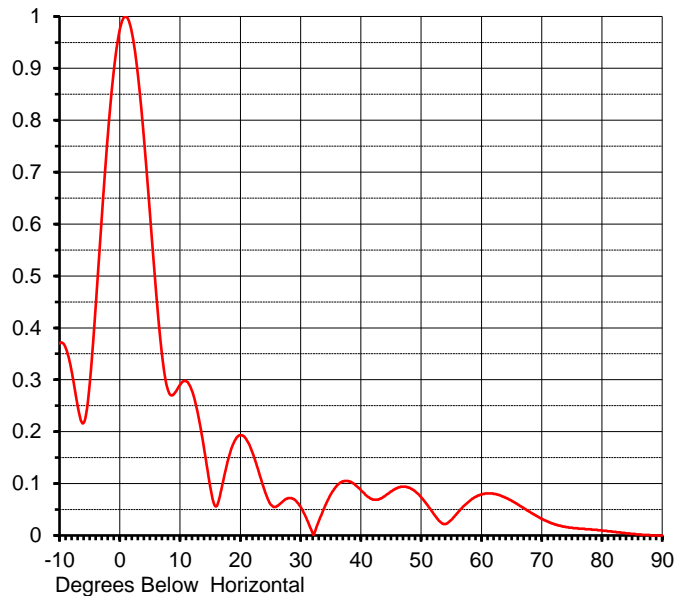
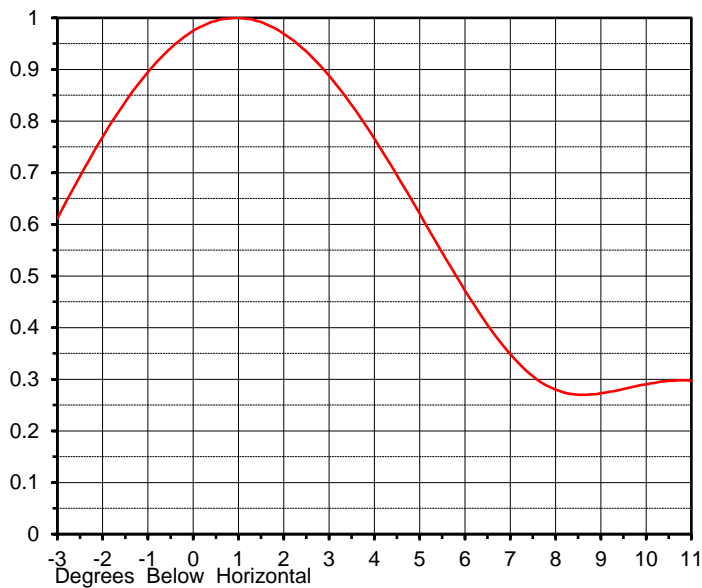
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ELEVATION PATTERN

Proposal No. **WWHO Interim Ch 23**
 Date **21-Feb-20**
 Call Letters **WWHO**
 Channel **23**
 Frequency **527 MHz**
 Antenna Type **TFU-8WB/VP-R C160**

RMS Directivity at Main Lobe **7.8 (8.94 dB)**
 RMS Directivity at Horizontal **7.5 (8.75 dB)**
Calculated

Beam Tilt **1.05 deg**
 Pattern Number **08W078105-23**



| Angle | Field | Angle | Field | Angle | Field | Angle | Field | Angle | Field |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| -10.0 | 0.370 | 10.0 | 0.290 | 30.0 | 0.055 | 50.0 | 0.074 | 70.0 | 0.032 |
| -9.0 | 0.362 | 11.0 | 0.297 | 31.0 | 0.032 | 51.0 | 0.059 | 71.0 | 0.027 |
| -8.0 | 0.317 | 12.0 | 0.278 | 32.0 | 0.004 | 52.0 | 0.043 | 72.0 | 0.022 |
| -7.0 | 0.250 | 13.0 | 0.232 | 33.0 | 0.027 | 53.0 | 0.028 | 73.0 | 0.019 |
| -6.0 | 0.217 | 14.0 | 0.166 | 34.0 | 0.055 | 54.0 | 0.022 | 74.0 | 0.016 |
| -5.0 | 0.291 | 15.0 | 0.094 | 35.0 | 0.079 | 55.0 | 0.030 | 75.0 | 0.015 |
| -4.0 | 0.441 | 16.0 | 0.056 | 36.0 | 0.096 | 56.0 | 0.043 | 76.0 | 0.014 |
| -3.0 | 0.611 | 17.0 | 0.097 | 37.0 | 0.104 | 57.0 | 0.056 | 77.0 | 0.013 |
| -2.0 | 0.769 | 18.0 | 0.147 | 38.0 | 0.104 | 58.0 | 0.066 | 78.0 | 0.012 |
| -1.0 | 0.895 | 19.0 | 0.181 | 39.0 | 0.098 | 59.0 | 0.074 | 79.0 | 0.011 |
| 0.0 | 0.975 | 20.0 | 0.193 | 40.0 | 0.087 | 60.0 | 0.079 | 80.0 | 0.010 |
| 1.0 | 1.000 | 21.0 | 0.185 | 41.0 | 0.076 | 61.0 | 0.081 | 81.0 | 0.008 |
| 2.0 | 0.969 | 22.0 | 0.160 | 42.0 | 0.069 | 62.0 | 0.080 | 82.0 | 0.007 |
| 3.0 | 0.888 | 23.0 | 0.125 | 43.0 | 0.070 | 63.0 | 0.078 | 83.0 | 0.006 |
| 4.0 | 0.766 | 24.0 | 0.088 | 44.0 | 0.076 | 64.0 | 0.073 | 84.0 | 0.004 |
| 5.0 | 0.621 | 25.0 | 0.060 | 45.0 | 0.085 | 65.0 | 0.067 | 85.0 | 0.003 |
| 6.0 | 0.472 | 26.0 | 0.056 | 46.0 | 0.091 | 66.0 | 0.060 | 86.0 | 0.002 |
| 7.0 | 0.349 | 27.0 | 0.065 | 47.0 | 0.094 | 67.0 | 0.053 | 87.0 | 0.001 |
| 8.0 | 0.280 | 28.0 | 0.072 | 48.0 | 0.092 | 68.0 | 0.046 | 88.0 | 0.000 |
| 9.0 | 0.273 | 29.0 | 0.069 | 49.0 | 0.085 | 69.0 | 0.039 | 89.0 | 0.000 |
| | | | | | | | | 90.0 | 0.000 |

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RADIO FREQUENCY IMPACT, SAFETY & STATEMENT OF COMPLIANCE

The licensee of WWHO is committed to the protection of station personnel and/or tower contractors working in the vicinity of the WWHO antenna and will reduce power or cease operation, when necessary, to ensure protection to personnel.

As shown in Appendix A the proposed WWHO channel 23 post-transition interim STA facility proposed herein will operate with a maximum ERP of 175.3 kW from an elliptically polarized directional transmitting antenna with a centerline height of 213.4 meters above ground level (AGL). Considering the elevation pattern submitted elsewhere in this application, the vertical plane relative field factor is less than 0.200 at all depression angles greater than 13 degrees. The proposed WWHO STA facility is predicted to produce a worst-case power density at two meters above ground level, at 122.1 meters from the tower base, of $1.226 \mu\text{W}/\text{cm}^2$, which is 0.35% of the FCC guideline value of $351.33 \mu\text{W}/\text{cm}^2$ for an "uncontrolled" environment, and 0.070% of the FCC's guideline value for "controlled" environments. Therefore, pursuant to Section 1.1307(b)(3) of the FCC Rules, because the proposed facility would not exceed 5% of the uncontrolled and controlled exposure limits, the proposal's power density contribution is considered insignificant.

Further, the applicant will continue to cooperate and coordinate with other any other site users and reduce power or cease operation during times of service or maintenance of the transmission systems as necessary to avoid potentially harmful exposure to personnel. In light of the above, the proposed facility should be categorically excluded from RF environmental processing under Section 1.1307(b) of the Commission's Rules.

WWHO
Channel 23 - Chillicothe, Ohio
ERP = 175300.00 WATTS

APPENDIX A

Maximum ERP 175.3 kW

Polarization ----- 2 Circular
 Antenna Height Above Ground - 213.4 meters 700.1 feet
 FCC Uncontrolled RFR Limit ---- 351.33 $\mu\text{W}/\text{cm}^2$

Maximum Computed Power Density 1.226 $\mu\text{W}/\text{cm}^2$
 0.35% of limit

| Angle Below Horizontal (degrees) | <Point X> Horiz Distance from tower to 2 m AGL (meters) | Slant Distance from antenna to Point X (meters) | Vertical Pattern (REL. FIELD) | WWHO ERP (kW) | WWHO Calculated Power Density $\mu\text{W}/\text{cm}^2$ | Percent Limit | Limit Exceeded? |
|---|---|--|-------------------------------------|---------------------|---|------------------|--------------------|
| 1 | | | 1.000 | 175.3000 | | | |
| 5 | 2416.3 | 2425.5 | 0.621 | 67.6029 | 0.768 | 0.22% | No |
| 10 | 1198.9 | 1217.4 | 0.290 | 14.7427 | 0.664 | 0.19% | No |
| 15 | 789.0 | 816.8 | 0.094 | 1.5490 | 0.155 | 0.04% | No |
| 20 | 580.8 | 618.1 | 0.193 | 6.5297 | 1.142 | 0.32% | No |
| 25 | 453.3 | 500.2 | 0.060 | 0.6311 | 0.168 | 0.05% | No |
| 30 | 366.2 | 422.8 | 0.055 | 0.5303 | 0.198 | 0.06% | No |
| 35 | 301.9 | 368.6 | 0.079 | 1.0940 | 0.538 | 0.15% | No |
| 40 | 251.9 | 328.9 | 0.087 | 1.3268 | 0.819 | 0.23% | No |
| 45 | 211.4 | 299.0 | 0.085 | 1.2665 | 0.947 | 0.27% | No |
| 50 | 177.4 | 276.0 | 0.074 | 0.9599 | 0.842 | 0.24% | No |
| 55 | 148.0 | 258.1 | 0.030 | 0.1578 | 0.158 | 0.05% | No |
| 60 | 122.1 | 244.1 | 0.079 | 1.0940 | 1.226 | 0.35% | No |
| 65 | 98.6 | 233.3 | 0.067 | 0.7869 | 0.966 | 0.28% | No |
| 70 | 76.9 | 225.0 | 0.032 | 0.1795 | 0.237 | 0.07% | No |
| 75 | 56.6 | 218.9 | 0.015 | 0.0394 | 0.055 | 0.02% | No |
| 80 | 37.3 | 214.7 | 0.010 | 0.0175 | 0.025 | 0.01% | No |
| 85 | 18.5 | 212.2 | 0.003 | 0.0016 | 0.002 | 0.00% | No |
| 90 | 0.0 | 211.4 | 0.000 | 0.0000 | 0.000 | 0.00% | No |

